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1 REDOX-FLOW BATTERY DESIGN FOR A METHANE-PRODUCING

2 **BIOELECTROCHEMICAL SYSTEM**

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- 11 Keywords: Bioelectrochemical power-to-gas, Reactor design, Methane, Biocathode,
- 12 Methanogenic archaea

13 ABSTRACT

14 Methane production at biocathodes is an innovative approach of storing renewable electrical 15 energy in chemical energy via the biological conversion of carbon dioxide. Methane-producing microorganisms use electricity to catalyze the conversion of carbon dioxide into methane; a 16 form of carbon-neutral natural gas. However, the rates of methane production remain too low 17 for practical application. To improve performance, high area-to-volume ratio with good mass 18 19 transfer is required. In this study, we used the design of redox flow-batteries with a high areato-volume ratio of 2.0 cm⁻¹ and an external capillary manifold for flow distribution . Current 20 21 densities up to 35 A/m² were applied, resulting in volumetric methane production rates of up 22 to 12.5 L CH₄/L/d, 3 times higher than rates reported so far. The highest energy efficiency of 30% was obtained at 25 A/m². Even with a low relative abundance of methanogens in the 23 microbial community (20%), dense biofilm growth was observed on the outer surface of the 24 biocathode. Flow-battery cell design shows promising performance for application of 25 methane-producing biocathodes. 26

27 **1.** INTRODUCTION

The increasing global energy demand not only results in a faster depletion of fossil fuels but also in an increased emission of carbon dioxide [1]. Hence, it is necessary to shift from nuclear and fossil energy sources towards renewable energy sources. However, the generation of renewable electricity is depending on intermittent energy sources like wind and sun. Due to the natural fluctuations of these energy sources, it is required to develop energy storage technologies [2].

Power-to-gas is a storage technology in which electrical energy is converted into chemical energy in the form of methane [3]. Recently, methane-producing bioelectrochemical systems (BESs) have emerged as a novel biological power-to-gas technology [4]. In such systems, water is typically oxidized at the anode, and hence functions as electron donor [5], while methane is generated via microorganisms located on or in the vicinity of the cathode from direct (via electrons) and/or indirect (via hydrogen) conversion of carbon dioxide[6].

The reported methane production rates are still low, ranging between 0.13-30 L $CH_4/m^2/day$ [4]. Recently, it was demonstrated that by controlling the current (galvanostatic operation) at 35 A/m², methane production rates were increased up to 60 L $CH_4/m^2/day$ [7]. To increase methane production rates further, it is crucial to design reactors with low distance between anode and cathode, and with good flow distribution to minimize mass transfer limitations.

45 The aim of this study was to improve the performance of methane-producing 46 bioelectrochemical system by adapting a reactor design typical for redox-flow batteries [8], 47 with electrodes positioned close to each other (0.5 cm compartment thickness). Moreover, external manifolds for liquid recirculation were used to ensure good mass transfer, according 48 to [9]. Experiments were conducted in galvanostatic mode at current densities up to 35 A/m². 49 50 For each tested current density, the performances in terms of methane production rate, current-to-methane efficiency as well as the energy efficiency were assessed. Finally, the 51 52 biofilm development and the microbial community have been analyzed via scanning electron 53 microscopy (SEM) and DNA sequencing.

54 2. MATERIALS AND METHODOLOGY

55 2.1 Experimental Set-Up

A redox-flow battery design reactor was used, containing an anode and cathode chamber. 56 Each chamber had a volume of 85 cm³ (13.0 cm length \times 13.0 cm width \times 0.5 cm thickness). 57 The chambers were separated via a cation exchange membrane with an effective surface area 58 59 of 169 cm² (Nafion 117, Dupont, USA). The electrolyte was supplied to and collected from each compartment via external manifolds with eleven capillaries, each with an inner diameter of 60 3.0 mm. These capillaries were wielded into holes located on two opposite sides of both 61 electrolyte frames [9] (Figure 1). An iridium-oxide coated titanium mesh (Typ G, mesh: 4.0 x 62 63 $2.0 \times 0.5 \times 0.5 \text{ mm}$, 12 g Ir/m^2 , Metakem GmbH, Germany) was used as anode. The anode was placed directly on the (untreated) membrane. The remaining space in the anode compartment 64 was filled with three layers of spacer cloth material (Vileda 1174 2-phase haze filter, Vileda, 65 Gemany). The cathode consisted of two layers of 4.6 mm thick graphite felt (specific surface 66 67 area: 0.4 m²/g; GFD 4.6, SGL Carbon Group, USA), compressed to fill the cathode chamber. The graphite felts were heat-treated for 4 h at 390 °C in an air circulation oven before use, in 68 69 order to increase hydrophilicity of the material. A bipolar plate (Sigracet TF6, SGL Carbon Group, USA) was used in connection to a nickel coated copper plate, functioning as current 70 collector, to prevent release of nickel or copper ions into the catholyte. Two reference 71 electrodes (3M KCl Ag/AgCl, QIS, Oosterhout, the Netherlands, +0.205 V vs standard hydrogen 72 73 electrode) were installed. The anodic reference electrode was installed in proximity of the 74 anode chamber, while the cathodic reference electrode was directly inserted into the cathode 75 compartment. The catholyte (total volume of 3.0 L) was recirculated via a liquid-gas separation bottle and a catholyte recirculation bottle. The anolyte was also recirculated via a 76 77 3.0 L anolyte recirculation bottle. The recirculation speed of both anolyte and catholyte was 85 mL/min. 78



Figure1.Exploded view of the redox flow battery design, used as reactor. An external capillary manifold
 was attached to the electrode chamber frame to improve electrolyte distribution. Remaining space in
 the anode compartment was filled with three layers of spacer material (not shown in this figure).

83 2.2 Electrolytes and Inoculum

The base medium for both catholyte and anolyte was a 40 mM phosphate buffer (2.72 g/L KH₂PO₄ and 3.55 g/L Na₂HPO₄·2H₂O). The catholyte additionally contained macronutrients (0.28 g/L NH₄Cl, 0.0076 g/L CaCl₂·2H₂O, 0.01 g/L MgSO₄·7H₂O, and 0.09 g/L MgCl₂·6H₂O), 1 mL/L of a micronutrient solution as described in [10] and 1 mL/L of a vitamin solution as described in [11]. As carbon source, sodium bicarbonate was added to the catholyte in a concentration of 5.0 g/L.

The catholyte was inoculated with 250 mL of a non-enriched consortium of microorganisms ($20.5 \pm 1.2 \text{ g/L}$ of volatile suspended solids (VSS)) from the Loick Bioenergie GmbH biogas plant after sieving (mesh size: 1 mm).

93 2.3 Operational Conditions

The biocathode was galvanostatically controlled (fixed current) by a potentiostat (PP201, ZAHNER-elektrik GmbH & Co. KG, Germany) and cathode potentials were recorded every minute. Catholyte temperature was controlled at 30.0 °C and catholyte pH was controlled at 7.0 via a pH controller (modified device; Liquisys, Endress+Hauser, Germany).

Before inoculation, the reactor was characterized abiotically at a current density of 5 A/m², normalized to cathode projected surface area. After inoculation, the same current density of 5 A/m^2 was used for the biocathode start-up period, which lasted until performance was stable (27 days). Then, the current density was increased to 10, 15, 25, and 35 A/m². The cathode was operated in fed-batch mode. The duration depended on the applied current density and ranged from 7 days to less than a day at 35 A/m², due to a faster depletion of carbon dioxide. After each current density, 2 L of the catholyte was exchanged with fresh medium under nitrogen flushing to prevent depletion of nutrients and bicarbonate.

106 **2.4 Chemical Analysis Methods and Calculations**

107 Methane production rate, current-to-methane efficiency and energy efficiency were analyzed. 108 Gas samples were collected in a gas sampling bag (GSB-P/10, Dr.-Ing.Ritter Apparatebau 109 GmbH & Co.KG, Germany). The volume of gas production inside the gas sampling bag was 110 quantified by syringe and analyzed for the concentrations of methane and carbon dioxide 111 online via a biogas analyzer (BenchOne, BlueSens, Germany); content of hydrogen, oxygen 112 and nitrogen were analyzed via gas chromatography (for details on these measurements see 113 SI).

114 Current, methane, and hydrogen production rates were normalized to the projected cathode 115 surface area (169 cm²) and/or to the volume of the cathode chamber (84.5 cm³). Current-to-116 methane efficiency and energy efficiency were calculated according to [4].

117 **2.5 Polarization Curves**

Polarization curves were recorded at the end of each batch by measuring the current at every
10s when decreasing the cathode potential from -0.2 to -0.9 V vs. SHE with a step width of
0.05 V and a step duration of 300 s. The last 10 data points (100 s) at each cathode potential
were averaged.

122 **2.6 Scanning Electron Microscopy**

Electrode samples were cut from the biocathode immediately after opening the reactor and 123 124 directly fixed for 2 h in 2.5 % glutaraldehyde in phosphate-buffered-saline (PBS) solution consisting of 8.00 g/L NaCl, 0.20 g/L KCl, 1.78 g/L Na₂HPO₄·2H₂O and 0.27 g/L KH₂PO₄ (pH 7.4). 125 126 Each sample was washed with PBS buffer for three times with each washing step lasting for 127 15 min, before dehydrating the samples in an ascending ethanol dilution series (10, 25, 50, 75, 128 and 90% (v/v), 20 min each, and finally in 100% (v/v) ethanol for 30 min. The samples were 129 treated for 20 min with bis(trimethylsilyl)amine (hexamethyldisilazane, HMDS) and dried in a 130 desiccator overnight. After sputter coating the samples with a 5.0 nm thin gold layer, they were placed at high vacuum with a Tescan Vega3 scanning electron microscope at 20 kVaccelerating voltage.

133 2.7 Microbial Community Analysis

Biofilm samples (0.1 g wet weight) of the graphite felts facing the membrane and the current collector were collected for microbial community analysis. DNA samples from the biofilm samples were extracted by using the PowerSoil DNA Isolation Kit (MO BIO Laboratories, Carlsbad, CA, USA). Bacterial and archaeal 16S rDNA gene fragments were amplified and analyzed according to [12].

139 **3. RESULTS AND DISCUSSION**

140 **3.1 Effect of Current Density on Methane production rates**

With increasing current densities from 5 A/m² to 35 A/m², the volumetric methane production rates increased almost linearly from 1.0 L CH₄/L/d to 13.0 L CH₄/L/d (Figure 2A). Current-tomethane efficiencies increased from about 35% at 5 A/m² to about 65% at 15 A/m², and remained at 60-65% at higher current densities (Figure 2B). Hydrogen production increased with increasing current densities, which is likely the result of limited methanogenic activity in relation to the supplied current. The energy efficiency ranged between 19 and 30%; the highest energy efficiency of 30% was obtained at 25 A/m².



Figure 2. A: Production rates of methane (blue) and hydrogen (red) at the different applied current
 densities. B: Current-to-product efficiencies of methane (blue) and hydrogen (red) and energy
 efficiencies (black dots, second y-axis) at different applied current densities.

The cathode potential during galvanostatic operation was approximately -0.75 V vs. SHE at the 151 lower applied current densities of 5 to 15 A/m², decreased to -0.85 V vs SHE at 25 A/m² and 152 finally to -1.1 V vs SHE at 35 A/m² (Figure 3A). Polarization curves showed that the biocathode 153 performance initially increased between 5 and 15 A/m², but then decreased with time at 154 current densities higher than 15 A/m^2 (Figure 3B). A possible cause for this decline in 155 156 performance is that methanogenic activity was not sufficiently high to convert all current into 157 methane (as also reflected in the higher hydrogen production rate). Therefore, hydrogen evolution occurred and higher hydrogen partial pressure in turn elevated cathodic 158 159 overpotential for hydrogen evolution reaction [13].



Figure 3. Cathode potentials (A) and Polarization curves (B) for each applied current density.
 Polarization curves were recorded at each cathode potential. From the polarization curves, initially
 an improvement was seen during which the applied current density was increased from 5 to 15 A/m²,
 while after increasing the applied current density to 25 and even 35 A/m², cathode performance
 deteriorated. This is also reflected in the sharp decrease in cathode potential at 25 and 35 A/m².

165

166 **3.2 Biofilm and Microbial Community Analysis**

167 SEM pictures were taken from the felt at different locations to analyze the distribution of 168 microorganisms (see Supporting Information). Almost no biofilm was observed on the inner part of the felts (Figure S1A), which is in line with observations in other studies [14]. A dense biofilm was observed across the graphite felt biocathode, at the electrode surface facing the membrane and the bipolar plate/current collector assembly (Figure S1B and S1C). Mostly rodshaped microorganisms with sizes around 1 µm were observed on the graphite felt facing the membrane (Figure S1D).

174 The results of microbial community analysis showed a 20% abundance of Archaea, with the other 80% being Bacteria (Figure 4). Different communities were found on the membrane side 175 176 and the current collector side of the electrode. At the current collector side, high relative 177 abundances of both Methanobacteriaceae and Methanomicrobia were found. Both are 178 hydrogenotrophic methanogens and have been observed at methane-producing biocathodes in many previous studies [4, 6, 7]. The presence of members of Firmicutes, such as 179 180 *Clostridium* sp., supported the hypothesis that hydrogen was an active intermediate [15]. At the membrane side, besides the dominant Methanobacteriaceae, Proteobacteria were 181 detected as the most dominant bacteria (81% of bacterial community). Especially, 182 Epsilonproteobacteria, which generate energy by oxidizing hydrogen using oxygen as electron 183 184 acceptor [16], was the most abundant bacterial genus in this location (49% of microbial 185 community) and likely had a role as oxygen scavenger near the membrane.



Figure 4. Taxonomic distribution of the biofilm on the graphite felt facing the membrane and the current collector. The abundance of methanogens was low, around 20%, while the rest of the microbial populations consisted of bacteria. Differences between membrane and current collector side are likely related to the availability of oxygen.

192 3.3 Outlook

193 An overview of the performances of methane producing biocathodes is shown in Table 1. 194 Compared to other studies, high methane production rates were achieved with the redox-195 flow battery design, especially when these rates are normalized to cathode volume. This is related to the high area to volume ratio (2.0 cm²/cm³) compared to other studies (all lower 196 than 0.9 cm²/cm³). Moreover, other studies, which also achieved high methane production 197 rates [7] often have small projected surface areas compared to the reactor design used herein, 198 whereas the performance in studies using reactors with larger projected surface areas [5] had 199 low methane production rates. The fact that larger reactors achieve lower rates may be 200 201 related to the fact that the medium distribution in large reactors has not always been 202 optimized, leading to a non-even distribution of reactor solution and mass transfer limitations. 203 Hence, the manifold design with several in- and outlets in this study is believed to be directly 204 related to the results obtained in this study. The mixing of the catholyte via the external manifold has been demonstrated for redox-flow battery application [17] shown to result in 205 homogeneously distributed reactor solutions. 206

- 208 **Table1.** Key parameters of this study in comparison to data of other mixed culture methane-producing
- 209 bioelectrochemical systems using water oxidation at the anode. Values have been normalized to
- 210 cathode projected surface area and cathode chamber volume, at standard temperature and pressure
- 211 (STP, 298.15 K and 1 bar).

Cathode potential [V vs. SHE]	Electrode material	Current density		Methane production rate		Curront	Projecte	Catho de surfac	
		[A/m²]	[kA/m³]	[L _{CH4} / m²/d]	[L _{CH4} /L/d]	to- methane efficienc y [%]	d cathode surface area [cm ²]	e area- to- volum e ratio [SA/V, cm ⁻¹]	Ref.
-0.32	Activated carbon granules	10.0	0.7	14.8	1.0	54	22	0.7	[7]
-0.38	Activated carbon granules	35.0	2.5	63.9	4.2	67	22	0.7	[7]
-0.50	Carbon cloth	0.2	2*10 ⁻⁴	1.6	0.1	93	80	0.2	[18]
-0.55	Graphite felt	0.2	0.1	0.1	0.01	23	250	0.9	[5]
-0.70	Graphite felt	2.9	1.0	5.1	0.5	73	250	0.9	[5]
-0.70	Graphite granules	10.0	0.7	15.0	1.0	52	22	0.7	[7]
-0.75	Carbon felt	3.4	0.1	7.4	0.1	89	98	0.2	[19]
-0.76	Graphite felt	10.0	2.0	15.7	3.1	56	169	2.0	This study
-0.85	Graphite granules	35.0	2.3	62.0	4.1	67	22	0.7	[7]
-1.08	Graphite felt	35.0	7.0	62.5	12.5	64	169	2.0	This study

213 Anode overpotentials were close to 0.3 V, independent of current density, a value typical for

noble metal catalysts [20]. The main irreversible voltage losses occurred at the biocathode.

At biological standard conditions (298.15 K and 1 bar, pH=7), the cathode potential for CO₂

- reduction to methane is about -0.24 V [4]. Based on our results (Fig. 3), the cathode
- overpotential was 0.52 V at 10 A/m², and increased to 0.84 V at 35A/m². These high

overpotentials at the cathode could be the result of limited cathodic microbial coverage and

219 activity [21]. Modifying the cathode surface in order to improve microbial adhesion could be

one solution to overcome this limitation [22]. Another strategy is the use of other cathode

221 materials, for example granular activated carbon (GAC), as it was recently reported that

222 methane-production biocathodes using GAC at 10 A/m² had cathode overpotentials of only

223 0.06 V [7].

224 The redox flow battery design offers opportunities for improving the performance of methane

225 producing BESs, especially when energy losses (overpotentials) at the cathode can be further

reduced, for example via modified electrodes or use of different electrode materials.

227

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231

232 **References**

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1 SUPPORTING INFORMATION

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3 REDOX-FLOW BATTERY DESIGN FOR A METHANE-PRODUCING

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- 14 systems, Biocathode, Methanogenic Archaea

16 Gas Chromatography

All gas samples were analyzed as doublets (each 250 μ L) for their concentrations of 17 methane, hydrogen, carbon dioxide, oxygen and nitrogen in a gas chromatograph of the 18 19 type Agilent Technologies 6890N. This gas chromatograph, which was equipped with an 20 HP-Plot column (30m x 0.53 mm x 40 μ m), an HP-Al₂O₃ column (30m x 0.53 mm x 15 μ m), 21 and an HP-Molsieve column (30m x 0.53 mm x 25 µm), analyzed the gas components via a flame ionization detector (FID) and a thermal conductivity detector (TCD). Helium was used 22 as carrier gas (flow rate HP-Al₂O₃: 5 mL/min; HP-Molsieve: 10 mL/min). Processing started 23 24 with keeping the gas samples at a temperature of 50 °C for 5 min, before raising the

- temperature by 10 °C/min until the final temperature of 120 °C was reached and held for 3
- 26 min.

27





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FigureS2. Scanning electron microscopy pictures of the biofilms. A: Low biofilm growth on inner part

of graphite felt. B: Dense biofilm on top of the graphite felt in contact with the membrane. C: Dense

biofilm on graphite felt fibers near the current collector. D: Close-up of biofilm on graphite felt near

36 the membrane.