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This is a "Post-Print" accepted manuscript, which has been Published in "Bioinspiration & amp; biomimetics"

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Please cite this publication as follows:

Langowski, J. K. A., Rummenie, A., Pieters, R. P. M., Kovalev, A., Gorb, S. N., & van Leeuwen, J. L. (2019). Estimating the maximum attachment performance of tree frogs on rough substrates. Bioinspiration & biomimetics, 14(2). https://doi.org/10.1088/1748-3190/aafc37

You can download the published version at:

https://doi.org/10.1088/1748-3190/aafc37

1	Estimating the maximum attachment performance of tree frogs
2	on rough substrates
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# 8 Abstract

9 Tree frogs can attach to smooth and rough substrates using their adhesive toe pads. We present 10 the results of an experimental investigation of tree frog attachment to rough substrates, and of 11 the role of mechanical interlocking between superficial toe pad structures and substrate asperi-12 ties in the tree frog species *Litoria caerulea* and *Hyla cinerea*. Using a rotation platform setup, 13 we quantified the adhesive and frictional attachment performance of whole frogs clinging to 14 smooth, micro-, and macrorough substrates. The transparent substrates enabled quantification 15 of the instantaneous contact area during detachment by using frustrated total internal reflection. 16 A linear mixed-effects model shows that the adhesive performance of the pads does not differ 17 significantly with roughness (for nominal roughness levels of  $0-15 \,\mu\text{m}$ ) in both species. This 18 indicates that mechanical interlocking does not contribute to the attachment of whole animals. 19 Our results show that the adhesion performance of tree frogs is higher than reported previously, 20 emphasising the biomimetic potential of tree frog attachment. Overall, our findings contribute 21 to a better understanding of the complex interplay of attachment mechanisms in the toe pads of 22 tree frogs, which may promote future designs of tree-frog-inspired adhesives.

Keywords: Bioadhesion, biomimetics, bioinspired adhesive, *Litoria caerulea*, *Hyla cinerea*,
surface roughness, mechanical interlocking.

# 25 **1 Introduction**

Strong, reversible, and repeatable attachment to a variety of substrates with different geometrical, mechanical, and chemical properties is a basic requirement both for climbing animals and for next-generation technological adhesives [1]. This overlap in functional demands has led to a considerable transfer of knowledge between the fields of biological and technical adhesion
(e.g. [2–7]), and to the design of a large number of biomimetic and bioinspired adhesives [3,8–
10].

32 Geckos and tree frogs are the most prominent vertebrate models for the design of biomimetic adhesives [11–15]. The toes of geckos are 'hairy' structures covered by numerous micro-33 34 scopic setae ending in nanoscopic spatulae and can conform to minute asperities of the substrate, hence facilitating the generation of 'dry' intermolecular van der Waals (vdW) forces 35 36 between toe and substrate [16–19]. The ventral epidermis on the toe pads of tree frogs is relatively smooth compared to that of the gecko, but it also forms a surface pattern consisting of 37 38 microscopic prismatic cells that are covered with nanoscopic cellular protrusions ('nanopillars') 39 and separated by channels [20,21]. In contrast to geckos, tree frogs rely on a wet environment, 40 and their permeable skin is inherently moist [22–24]. Accordingly, their toe pads stand out as a 41 model system for attachment in wet conditions. The toe pads have been proposed to give rise 42 to 'wet adhesion' [25-30], which comprises capillary and hydrodynamic attachment forces 43 ([31,32]; e.g. Stefan adhesion). VdW forces [25,33] and mechanical interlocking [25,34–36] 44 have also been discussed to contribute to the adhesion (i.e. the attachment force normal to the 45 substrate surface) and friction (i.e. the attachment force parallel to the substrate surface) of tree 46 frogs.

47 Studying the fundamental mechanisms of tree frog attachment contributes not only to the 48 understanding of the ecology [37,38] and evolution [39,40] of these animals, but also promotes 49 the technical development of biomimetic adhesives for operation in a wet environment, for 50 example in surgery [41] or robotics [42]. Measuring adhesion, friction, and the respective con-51 tact-area-normalised contact stresses as a function of substrate properties such as free surface 52 energy, stiffness, or roughness is a common approach to elucidate the fundamental mechanisms 53 of an attachment apparatus [43–46]. For example, insect claws can only interlock mechanically 54 with substrate asperities above a critical roughness [47,48]. Analogously, mechanical interlock-55 ing of the superficial structures on a tree frogs' toe pad with substrate asperities should be-if present at all—maximal when the nominal roughness R of the substrate (defined, unless men-56 57 tioned otherwise, as the characteristic size of the substrate asperities) is similar or larger in size than the pad surface structures (i.e.  $\approx 300$  nm for the nanopillars [21] and  $\approx 10 \,\mu\text{m}$  for the epi-58 59 dermal cells [20]). The attachment forces generated by the other proposed attachment mecha-60 nisms might also be critically attenuated with increasing substrate roughness, for example by 61 reducing the effective contact area [49] or by meniscus cavitation [34,50].

Traditionally, the attachment performance of a whole tree frog is quantified by measuring 62 63 the angles at which a frog begins to slide on (sliding angle  $\alpha_{\parallel}$ ) and finally falls off (falling angle 64  $\alpha_{\perp}$ ) from a substrate rotating around a horizontal axis (referred to as 'rotation platform'; [25,50,51]). These angles are proxies for the whole-animal (static) friction and adhesion, re-65 66 spectively. Previous work shows slight variations of falling and sliding angle with increasing 67 roughness up to ca. 15 µm [34,43,50,52]. At higher roughness levels, adhesive [34,50] as well 68 as frictional [34] performance decline. For computation of the contact-area-normalised whole-69 animal adhesion (i.e. tenacity), previous studies exclusively used the maximum total contact 70 area of all toe pads and neglected inertial loads acting on the pads. Measurements of the whole-71 animal attachment performance on nano- to microrough substrates under control of substrate 72 surface energy, and under consideration of the instantaneous contact area (i.e. the actual contact 73 area just before falling) and of dynamic loads are largely missing, which may have led to an 74 underestimation of the attachment performance of tree frogs.

Here, we present a study of the whole-animal attachment performance of tree frogs as a function of substrate roughness on smooth (i.e. a nominal roughness  $R = 0 \,\mu\text{m}$ ), micro- $(R = 0.1 \,\mu\text{m}, 0.5 \,\mu\text{m}, 6 \,\mu\text{m}, \text{and } 15 \,\mu\text{m})$ , and macrorough ( $R = 200 \,\mu\text{m}$ ) substrates in the species *Litoria caerulea* and *Hyla cinerea*, which are among the most intensively studied tree frog 79 species [20,21,25,33,35,41,42,53,54]. Most previous studies included smooth and macrorough 80 substrates, distinguishing these roughness levels as reference cases. Using a custom-built rota-81 tion platform, which allows the dynamic measurement of the instantaneous contact area, we 82 aim to (i) characterise the whole-animal attachment performance on rough substrates, (ii) test whether mechanical interlocking contributes to the adhesion of the toe pads, and (iii) provide 83 84 an estimate for the maximum adhesion performance of tree frogs' toe pads. As tree frogs fre-85 quently encounter substrates with very diverse properties [55], we expect that adhesion and 86 friction are insensitive towards a large range of substrate roughness levels. If mechanical inter-87 locking is present as proposed previously, we expect an increase in attachment performance 88 with increasing roughness. In particular, the attachment performance should increase stepwise 89 when the substrate roughness gets larger than the nanopillars (i.e. switching from 0.1 nm to 90  $0.5 \,\mu\text{m}$ ) or the epidermal cells (i.e. switching from  $6 \,\mu\text{m}$  to  $15 \,\mu\text{m}$ ). A stepwise decrease in 91 attachment performance may be expected at an even higher roughness (i.e. 200 µm), when the 92 substrate asperities become too large to allow interlocking with the micro- to nanoscopic pad 93 surface structures. As the animal-substrate contact area in friction measurements is dominated 94 by the belly [28,29,52,56,57], we can only analyse the whole-animal performance with respect to friction. 95

- 96 2 Materials and methods
- 97 2.1 Ethical statement

All animals used in this study were bought from legal vendors. All procedures described were
approved by the Animal Ethics Committee of Wageningen University & Research (WUR; permit number 2014126.d).

101 2.2 Experimental animals

Experiments were performed with adult individuals of *Litoria caerulea* (number n = 6, body mass  $m = 46.8 \pm 13.4$  g, snout-vent-length  $\ell_{SV} = 79.2 \pm 5.6$  mm; unless mentioned otherwise, 104 we report mean  $\pm$  standard deviation throughout this study) and Hyla cinerea (n = 6,  $m = 8.7 \pm 1.7$  g,  $\ell_{SV} = 48.7 \pm 1.6$  mm). The animals were housed, separated by species, in 105  $0.6 \cdot 0.6 \cdot 1.2 \text{ m}^3$  (width  $\cdot$  length  $\cdot$  height) large terraria, with six frogs per terrarium, at the CA-106 107 RUS research facility at WUR. The terraria were enriched with plants (Ficus spec.) and scaf-108 folds of polypropylene-pipes. Temperature and relative air humidity were kept at 24-26 °C and 109 45–85%, using heating mats and a semi-automatised sprinkler system spraying demineralised 110 water (Bitter Watertreatment, Netherlands), respectively. The frogs were kept at a 12 h : 12 h 111 dark-light-cycle and fed 2-3 times per week with 3-5 live crickets enriched with vitamin/min-112 eral powder (Dendrocare, AmVirep, Netherlands) per individual; water was supplied ad libi-113 tum. The room air was filtered for pathogens with an air purifier (WINIX U300, Winix, USA). 114 The frogs were monitored daily for their wellbeing.

## 115 **2.3 Test substrates**

Transparent, stiff substrates with a defined roughness and a surface area of  $290 \cdot 210 \text{ mm}^2$  were 116 117 produced in a two-stage-casting-process (similar to [58,59]). To create substrates with nominal 118 roughness levels of 0 µm (smooth), 0.1 µm, 0.5 µm, 6 µm, 15 µm, and 200 µm (macrorough), 119 a thin sheet of plexiglas, diamond lapping film (661X, 3M, USA), or conventional sandpaper 120 (grit size 80, KWB, Germany) with the according particle size was glued into an aluminium 121 mould (Figure 1A). Polydimethylsiloxane (PDMS; Sylgard 184, Dow Corning, USA) was pre-122 pared at a base:curing-agent ratio of 10:1, degassed in a vacuum-oven, and filled into the mould 123 to create a negative of the rough surface (Figure 1B). Before casting, the mould was slightly 124 tilted to avoid bubble formation. After curing, the PDMS-negative was removed (Figure 1C) 125 and filled with vacuum-degassed epoxy resin prepared at a base:curing-agent ratio of 1:0.9 126 (Crystal Clear 200, Smooth-On, USA; Shore hardness = 80 D, Elastic modulus  $\approx$  400 MPa; 127 Figure 1D), which resulted in a positive cast of the rough surface (Figure 1E).



128

129 Figure 1. Generation of the transparent and stiff test substrates with defined roughness.

130 Surface roughness was characterised and spatial homogeneity of the surface profiles of the 131 test substrates was ensured using a VR-3100 3D measuring macroscope (Keyence, Japan) and 132 a New View 6000 white light interferometer (Zygo, USA). Conventional roughness parameters of the substrates are shown in Table 1, a more elaborate roughness analysis can be found in 133 134 section SI.2.1. With an OCAH 200 contact angle measuring system (DataPhysics Instruments, 135 Germany) and the sessile drop method, we computed for the hydrophilic substrate material (water contact angle  $71.92 \pm 2.07^{\circ}$ ) a free surface energy  $\gamma$  of 39.2 mJ m<sup>-2</sup> (dispersive compo-136 nent  $\gamma_d = 30 \text{ mJ m}^{-2}$ , polar component  $\gamma_p = 9.2 \text{ mJ m}^{-2}$ ) with the Owens, Wendt, Rabel, and 137 138 Kaelble (OWRK) method ([60–62]; see section SI.2.2).

<sup>139</sup>**Table 1.** Conventional roughness parameters  $R_a$  (arithmetic average roughness) and *RMS* (root mean squared140roughness) of the used substrates in  $\mu$ m (mean  $\pm$  standard deviation, n = 10). For the smooth to 15  $\mu$ m substrates,141roughness was measured by white light interferometry, for the macrorough substrate with profilometry (120×142magnification).

	Magni- fication	Smooth	0.1 µm	0.5 µm	6 µm	15 µm	Macrorough
Ra	$5 \times$	$0.024 \pm 0.007$	$0.438 \pm 0.022$	$0.476 \pm 0.017$	$0.405 \pm 0.025$	$0.441 \pm 0.046$	<u> 99 214 - 11 902</u>
	$50 \times$	$0.005 \pm 0.002$	$0.425 \pm 0.023$	$0.474 \pm 0.032$	$0.410 \pm 0.072$	$0.484 \pm 0.122$	00.214±11.095
DMC	$5 \times$	$0.053 \pm 0.014$	$0.591 \pm 0.030$	$0.628 \pm 0.055$	$0.684 \pm 0.029$	$0.965 \pm 0.076$	NT/A
KMS	$50 \times$	$0.006 \pm 0.002$	$0.534 \pm 0.028$	$0.579 \pm 0.034$	$0.667 \pm 0.096$	$0.961 \pm 0.141$	1N/A

143

## 144 **2.4 Experimental setup and protocol**

A custom-built rotation platform was used to quantify the whole-animal attachment performance of the studied frog species (Figure 2A). The test substrates were rotated around a horizontal axis at an angular speed of ca.  $3.6^{\circ}$  s<sup>-1</sup>, driven by a RS Pro brushed DC geared motor (RS Components, Netherlands) via a pulley-timing-belt-system (27-T5; Mädler, Germany). A custom-programmed Arduino (Arduino Uno revision 3, Arduino) read out the platform angle from an angle sensor (981 HE special, Vishay Spectrol, USA; linearity  $\pm$  0.5%).







Four LED-strips (LS-OO06-STWH-SD111; Intelligent LED Solutions, UK) were attached 155 156 to the sides of the transparent substrate such that the emitted light was reflected internally. This 157 allowed us to visualise the instantaneous pad-substrate contact area by frustrated total internal 158 reflection (FTIR; [63]), which utilises the frustration of the internal reflection at locations of 159 animal-substrate contact, causing local light scattering (inset in Figure 2A). The contact area 160 was recorded ventrally with a HC-VX980 camcorder rotating with the substrate (Panasonic, Japan;  $3840 \cdot 2160$  pixels, effective pixel size  $\approx 90 \cdot 90 \,\mu\text{m}^2$ ) at 30 frames per second, resulting 161 162 in an angular step size of 0.12° per frame. The video recordings and angle measurements were 163 synchronised using a sound signal (duration < 5 ms) at regular time intervals ( $\Delta t \approx 2.14$  s). The 164 animals were filmed laterally with a C930e webcam (Logitech, Switzerland; 1920 · 1080 pix-165 els, 30 frames per second) to inspect general body positing and movements.

Prior to each trial, the animals were rinsed carefully with demineralised water to remove contaminations that could influence attachment performance, and subsequently put on a smooth

168 polymer sheet to standardise the amount of liquid covering the ventral body surface. Six indi-169 viduals each of L. caerulea and H. cinerea were tested for the six substrates with different 170 roughness levels in a randomised order. To compensate for the variation in the measurements 171 due to behavioural variation in the animals, we repeated each individual-roughness-combina-172 tion 10 times (i.e. a trial), leading to a total of 720 trials (60 per species and roughness). In each 173 trial, individual animals were placed head upwards on the substrate and rotated from a horizon-174 tal  $(0^{\circ})$  into a vertical  $(90^{\circ})$  and finally an overhanging position (> 90^{\circ}). Belly-substrate contact 175 was impaired by gently prodding the animals with a soft object. Trials were excluded when the 176 frogs jumped off the substrate, moved outside the substrate area with specified roughness, or 177 made extensive contact with body parts other than the toe pads before falling (in adhesion meas-178 urements), leading to 133 and 72 trials of L. caerulea, and 106 and 70 trials of H. cinerea for 179 further analysis of their adhesion and friction performance, respectively. These trials include 180 cases with only a few toes in contact.

#### 181

#### **2.5** Data analysis and statistics

182 Data analysis was performed with a custom-made MATLAB routine (Version R2015a, The 183 Mathworks, USA). From the videos, the angles at which the frogs started sliding  $(\alpha_{ll})$  and lost 184 contact to the substrate  $(\alpha_{\perp})$  with all four limbs were identified. For the determination of the instantaneous contact area A just before falling, we measured the contact area of all toes in 185 186 contact at the last recorded moment before detachment, at which the number of toes in contact 187 was constant and the contact area of individual toes was not yet decreasing (i.e. static contact; 188 see also Figure SI.6). The instantaneous contact area was quantified with ImageJ (Version 189 1.51g, National Institutes of Health, USA). This was not possible for the macrorough substrate 190 because of too strong scattering of the totally internally reflected light.

Before each trial, snout-vent-length  $\ell_{SV}$  was recorded by a calibrated dorsal photograph made with a Nikon 5500 camera using a Nikon AF-NIKKOR 24 mm f/2.8 D lens

8

193 (6000  $\cdot$  4000 pixels, effective pixel size 47  $\cdot$  47  $\mu$ m<sup>2</sup>); immediately after each trial, body mass 194 *m*, environmental temperature *T*, and relative air humidity *H* were recorded using an OHAUS 195 Scout Pro balance (Parsippany, USA; resolution: 0.01 g) and a testo 608-H1 hygrometer (Testo 196 Ltd, UK; resolution: 0.1 °C, 0.1%), respectively.

197 From the sliding and falling angle ( $\alpha_{\parallel}$  and  $\alpha_{\perp}$ ), body mass *m*, and instantaneous contact area 198 *A*, we computed adhesion  $F_{\perp}$ , static friction  $F_{\parallel}$ , and the adhesive contact stress (i.e. tenacity  $\sigma_{\perp}$ ) 199 as follows (Figure 2B, [51]):

$$F_{\perp} = mg\cos(180 - \alpha_{\perp}) = -mg\cos\alpha_{\perp} \qquad \qquad 90^{\circ} < \alpha_{\perp} < 180^{\circ} \qquad (1)$$

$$F_{\parallel} = mg \sin \alpha_{\parallel} \qquad \qquad 0^{\circ} < \alpha_{\parallel} < 90^{\circ} \qquad (2)$$

$$\sigma_{\perp} = \frac{F_{\perp}}{A} \tag{3}$$

200 In these equations, we assume an equal distribution of load over all limbs and toes, and 201 neglect inertial effects. The potential effects of substrate roughness on the attachment perfor-202 mance of tree frogs were analysed by fitting the falling angle  $\alpha_{\perp}$  and sliding angle  $\alpha_{\parallel}$  as a func-203 tion of substrate, species, and body mass in a linear mixed-effect model in MATLAB (signifi-204 cance level  $\alpha = 0.05$ ). Based on the Akaike information criterion adjusted for small sample sizes 205 (AICc; [64]), snout-vent-length, temperature, and relative humidity were excluded as fixed ef-206 fects. Individual identity was fitted as random intercept to correct for interindividual variation 207 that is not accounted by the fixed effects. Measurement date was fitted as additional random 208 intercept to correct for variation between measurement days. Moreover, the interaction between 209 individual identity and substrate, as well as between individual identity and repetition number 210 were fitted as random intercepts to correct for pseudo-replication and to quantify the variation 211 of an individual within a given substrate and repetition number, respectively. For the model 212 diagnostics see section SI.4.

## 213 **3 Results**

214 Tree frogs are able to generate adhesion and friction on substrates with different roughness 215 levels. Over the course of measurements, temperature and relative air humidity were 23.3-216 26.3 °C and 39.8–69.0%, respectively. During single trials, the animals regularly moved across 217 the rotating platform, requiring prodding with the hands of the experimenter to keep the frogs 218 on the platform (Figure 3). Typical changes in body posture were observed, with frogs taking a 219 splayed body posture with increasing substrate inclination, as discussed in detail elsewhere 220 [52,65]. Over the course of one trial, large changes in the number of contact points and in the 221 size of the instantaneous contact area were observed, ranging from—in addition to the toes— 222 full belly contact to the contact of only a few toes of two limbs (Figure 3).



223

Figure 3. Rotation platform trial for an individual of *L. caerulea* on a smooth substrate. At platform angles  $\leq 100^{\circ}$ , the belly contributes to the overall contact area. Just before detachment (angles  $\geq 123^{\circ}$ ), quick limb movements are visible, which result in time and space dependent variations of the ensemble of pad-substrate contact areas.

Interestingly, we observed several instances where frogs clinging to the substrate at an angle of approximately 120–130° were able to remain attached although temporarily the forelimbs completely detached from the substrate and the animals swung back- and forwards (Figure 4).





Figure 4. Attachment dynamics of *L. caerulea* clinging to a rotating, overhanging, smooth substrate. After detachment of the forelimbs, the body swings backwards by more than 90°. During the swinging phase, inertial loads are likely to act on the attachment interface in addition to the static body weight. Insets show the body posture in lateral view. To improve clarity, the images were filtered by outlier-removal (ImageJ).

In the following sections, we describe the adhesion performance of the toe pads and the

237 friction performance of whole animals for the studied frog species.

## 238 **3.1** Adhesion performance

For *L. caerulea*, the falling angle  $\alpha_{\perp}$  ranges from 93.0 ± 13.4° (macrorough substrate) to 129.1 ± 11.2° (0.1 µm substrate; Figure 5). The falling angles on the 0.1 µm, 0.5 µm (118.1 ± 24.4°), 6 µm (128.2 ± 12.6°), and the 15 µm substrate (128.8 ± 14.7°) do not differ significantly from  $\alpha_{\perp}$  on the smooth substrate (119.4 ± 18.2°), whereas falling angles on the macrorough substrate are significantly lower by 36.1 ± 4.9° than on the smooth substrate (estimate ± 95% confidence interval [*CI*]; see Table 2 for the linear mixed-effect model statistics). The falling angle scales negatively with body mass *m* (slope = -0.34 ± 0.28° g<sup>-1</sup>, estimate ±

246 95% *CI*; *t* = -2.337, *DF* = 231, *p* = 0.020).



247

248 **Figure 5.** (A<sub>I</sub>) Falling angle  $\alpha_{\perp}$ , (A<sub>II</sub>) adhesion  $F_{\perp}$ , and (A<sub>III</sub>) tenacity  $\sigma_{\perp}$ , as well as (B<sub>I</sub>) sliding angle  $\alpha_{\parallel}$  and (B<sub>II</sub>) 249 (static) friction  $F_{\parallel}$  as a function of (nominal) substrate roughness R for Litoria caerulea (blue) and Hyla cinerea 250 (green). For sliding angles  $\alpha_{\parallel} > 90^{\circ}$ , the friction  $F_{\parallel}$  was computed with  $\alpha_{\parallel} = 90^{\circ}$ . Boxes indicate median, and 25<sup>th</sup> 251 and 75<sup>th</sup> percentiles of the measured values. Values that are a located more than 1.5 times the interquartile range 252 above or below the boxes are shown as outliers. For the falling and sliding angle, black dots and whiskers denote 253 the mean values and the 95% confidence intervals predicted from the linear mixed-effects models. Strong scatter-254 ing of the internally reflected light prevented the measurement of the contact area and thus of the tenacity on the 255 macrorough substrate.

The adhesion  $F_{\perp}$  of *L. caerulea* ranges between  $192.8 \pm 85.7$  mN and  $282.1 \pm 88.5$  mN for roughness levels between smooth and 15 µm. On the macrorough substrate,  $F_{\perp}$  drops by 81%

to  $50.2 \pm 63.5$  mN, if compared to the smooth substrate; adhesion on the macrorough substrate

is significantly different from the other roughness levels according to one-way ANOVA with

Bonferroni correction (F[5,100] = 29.98, p < 0.001). The adhesive tenacity  $\sigma_{\perp}$  ranges from 2.1 ± 0.8 mN mm<sup>-2</sup> (smooth substrate) to 2.8 ± 0.9 mN mm<sup>-2</sup> (15 µm substrate). The tenacity measures are not significantly different, as determined by one-way ANOVA with Bonferroni correction (F[4,88] = 1.46, p = 0.220). Tenacity could not be quantified for the macrorough substrate because of too strong scattering of the internally reflected light. Peak tenacities of 8.8 mN mm<sup>-2</sup> were measured.

Table 2. Fixed-effects coefficient estimates of the linear mixed-effects model for the falling angles of tree frogs
 on substrates with different roughnesses. *SE* standard error, *DF* degrees of freedom, *t* t-statistic, *p* p-value.

	Estimate	SE	DF	t	р
Intercept <sup>a</sup>	142.73	7.26	231	19.665	< 0.001
Hyla cinerea	-11.60	6.07	231	-1.912	0.057
0.1 µm	0.60	2.36	231	0.254	0.799
0.5 µm	-1.78	2.69	231	0.287	0.774
6 µm	0.71	2.48	231	0.419	0.676
15 µm	1.02	2.42	231	-0.661	0.510
Macrorough	-36.12	2.47	231	-14.619	<.001
Body mass	-0.34	0.14	231	-2.337	0.020
<sup>a</sup> i.e. <i>Litoria caerulea</i> on the smooth substrate.					

<sup>268</sup> 

269 Similar trends were observed for the adhesion performance of *H. cinerea*, and the linear 270 mixed-effects model does not show significant differences between the two species (t = -1.912, DF = 231, p = 0.057). Falling angles range from  $126.9 \pm 8.2^{\circ}$  to  $130.1 \pm 9.2^{\circ}$  for roughness lev-271 272 els between smooth and 15 µm, and the falling angle decreases significantly on the macrorough substrate, if compared to the other roughness levels. Compared to L. caerulea, H. cinerea gen-273 274 erates much lower adhesion of  $46.9 \pm 15.1$  mN to  $54.5 \pm 16.0$  mN for roughness levels between 275 15 µm. On the macrorough substrate, *H. cinerea* barely adheres smooth and  $(F_{\perp} = 2.0 \pm 14.2 \text{ mN})$ . The tenacity varies between 1.5  $\pm$  0.7 mN mm<sup>-2</sup> and 2.8  $\pm$  1.1 mN mm<sup>-2</sup> 276 277 on the five less rough substrates, mostly without significant differences; only on the 0.1 µm 278 (p = 0.003) and the 15  $\mu$ m (p = 0.003) substrate, the frogs generated significantly higher tenac-279 ities compared to the smooth substrate, as found in a multiple comparison using Bonferroni 280 correction.

#### 281 **3.2 Friction performance**

The sliding angle  $\alpha_{\parallel}$  of *L. caerulea* ranges between  $79.4 \pm 18.6^{\circ}$  (smooth) and  $81.1 \pm 9.5^{\circ}$ (macrorough). Compared to the smooth substrate,  $\alpha_{\parallel}$  is significantly higher by 8.4–13.6° (estimates) on the 0.1 µm, the 6 µm, and the 15 µm substrate (Table 3). For the macrorough substrate, lower sliding angles were measured than on the smooth substrate (difference =  $-7.6 \pm 8.5^{\circ}$ , estimate  $\pm 95\%$  *CI*), but this difference is just not statistically significant (p = 0.081). In contrast to the falling angle, the scaling of sliding angle with body mass *m* is not significant (slope =  $-0.14 \pm 0.29^{\circ}$  g<sup>-1</sup>; t = -0.923, DF = 134, p = 0.358).

Table 3. Fixed-effects coefficient estimates of the linear mixed-effects model for the sliding angles of tree frogs
 on substrates with different roughnesses. Symbols as in Table 2.

	Estimate	SE	DF	t	р
Intercept <sup>a</sup>	87.94	7.75	134	11.352	< 0.001
Hyla cinerea	11.73	6.33	134	1.855	0.066
0.1 µm	8.35	4.21	134	1.984	0.049
0.5 µm	6.22	4.21	134	1.478	0.142
6 µm	8.98	4.21	134	2.135	0.035
15 µm	13.64	4.21	134	3.242	0.002
Macrorough	-7.58	4.31	134	-1.760	0.081
Body mass	-0.14	0.15	134	-0.923	0.358
<sup>a</sup> i.e. <i>Litoria caerulea</i> on the smooth substrate					

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The maximum friction force  $F_{\parallel}$  generated by *L. caerulea* ranges between 435.4 ± 135.3 mN (smooth) and 458.0 ± 131.6 mN (0.1 µm). Differences between the roughness levels are not significant, as determined by one-way ANOVA with Bonferroni correction (*F*[5,64] = 0.08, *p* = 0.995).

*H. cinerea* shows sliding angles  $\alpha_{||}$  between  $85.2 \pm 5.6^{\circ}$  (macrorough) and  $112.3 \pm 10.5^{\circ}$ (15 µm). The sliding angle was not significantly different between *L. caerulea* and *H. cinerea* (t = 1.855, DF = 134, p = 0.066). The friction  $F_{||}$  of *H. cinerea* ranges between  $83.4 \pm 18.4$  mN ( $0.1 \mu$ m) and  $86.3 \pm 18.5$  mN ( $0.5 \mu$ m). An one-way ANOVA with Bonferroni correction does not show significant differences in the friction generated on the different substrates (F[5,66] = 0.05, p = 0.998).

# 302 4 Discussion

## 303 4.1 Effects of substrate roughness on attachment performance

304 Figure 6 provides an overview of the effect of substrate roughness variations on the adhesive 305 performance of L. caerulea and H. cinerea studied here as well as of various tree frog species 306 studied in previous research [34,43,50,52]. The adhesion performance of L. caerulea and H. ci-307 *nerea*, approximated by the falling angle  $\alpha_{\perp}$ , is approximately constant up to a roughness of 308 15 µm, showing that tree frogs are well able to adhere to substrates with a wide range of rough-309 ness. Also the adhesion  $F_{\perp}$  and tenacity  $\sigma_{\perp}$  barely differ on all tested substrates except the 310 macrorough one. Such an insensitivity of adhesion towards substrate roughness is beneficial, 311 as tree frogs encounter various roughness levels in their natural habitat, ranging from smooth 312 to microrough leaves (e.g.  $R_a \approx 0.5-100 \,\mu\text{m}$  [55]) to macrorough tree bark. In the following, we 313 discuss the adhesion performance of the toe pads for the different roughness levels, from 314 smooth over micro- to macrorough substrates. As the friction data are largely confounded by 315 the contact of belly and other body portions, we discuss these only where helpful.



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**Figure 6.** Adhesion performance of tree frogs as a function of (nominal) substrate roughness, indicated by the falling angles measured in this study (circles; means and 95% confidence intervals predicted from a linear mixedeffects model, *Litoria caerulea* [blue], *Hyla cinerea* [green]) and reported in literature (asterisks from Fig. 5 in [50], *Hyla microcephala*; crosses from Fig. 8a in [43], *Colostethus trinitatis*; diamonds from Fig. 3b in [52], *Rhacophorus pardalis*; squares from Fig. 1B in [34], *Litoria caerulea*). For smooth substrates, R = 10 nm is assumed. Falling angles below 90° (dashed line) indicate full adhesive failure. Due to only small interspecific differences, the blue and green circles are almost overlapping.

324 The falling angles of L. caerulea and H. cinerea measured on the smooth substrate fall within the range of 100–180° reported in literature (Figure 6). This large range arises from 325 326 several causes. Most importantly, the attachment performance of tree frogs scales intra- and 327 interspecifically with body size: As reported in this study and elsewhere [50,66,67], falling 328 angles scale negatively with body mass. The correction for body mass in the linear mixed-329 effects model removes this size effect, resulting in  $\alpha_{\perp} \approx 127.5^{\circ}$ . Whereas the superficial mor-330 phology of the adhesive pad does not seem to differ between the two species (see Figure SI.9; 331 [51,52]), interspecific differences in animal behaviour, in the chemistry of the secreted mucus, 332 or in the internal morphology of the toe pads [68] may explain the interspecific differences in 333 attachment performance. Also, differences in substrate properties other than roughness should 334 be considered. In this study, a hydrophilic epoxy resin with—compared to glass—relatively 335 low free surface energy was used. We are not aware of extensive experimental studies on the 336 effects of variations of free surface energy on tree frog attachment [69], and differences in free 337 surface energy and hence in adhesion performance between the different studies (e.g. glass and 338 aluminium oxide polishing paper in [34]) cannot be excluded.

On microrough substrates (i.e.  $0.1 \,\mu m < R < 15 \,\mu m$ ), the adhesion performance does not 339 340 differ compared to the smooth substrate, as shown by the linear mixed-effects model for falling 341 angles, and by the transformation of falling angles to adhesion forces or tenacities. Only for 342 H. cinerea, tenacities are significantly higher on the 0.1 µm and the 15 µm substrate compared 343 to the smooth one. These results are only partially in line with the findings of Crawford et al. 344 [34], who described for single pads of L. caerulea significantly higher tenacities for R = 0.3-345  $16 \,\mu\text{m}$ , if compared to a smooth substrate. Presumably, this disagreement between rotation plat-346 form experiments and single pad studies arises from differences in pad loading. Normal as well 347 as shear loading have been shown to be important factors in determining the attachment performance of tree frog toe pads [26,70], which is discussed in more detail in Section 4.3. 348

349 In general, adhesion performance changes only little with an increasing substrate roughness 350 from smooth to ca. 40 µm (Figure 6). Neither does adhesion performance increase abruptly with 351 increasing roughness, as expected for biological attachment systems using mechanical inter-352 locking (e.g. the claws of the beetles Gastrophysa viridula [44] and Pachnoda marginata [47], 353 or of the may fly larva *Epeorus assimilis* [48]), nor does it drop suddenly, as hypothesised when 354 the substrate asperities become too large to allow mechanical interlocking with the nano- to 355 microscopic features of the ventral pad surface [53]. Importantly, the toe pads of tree frogs are 356 very soft (with an effective elastic modulus of ca. 20–50 kPa; [41,71,72]), potentially allowing 357 a close conformation to a rough substrate, an increase in the effective contact area, and as a 358 result enhanced van der Waals forces (e.g. [73]). Therefore, one cannot exclude that at different 359 roughness levels the effects of mechanical interlocking and other possibly involved attachment 360 mechanisms cancel each other, leading to a constant attachment performance with increasing 361 roughness. For further studies of the pad conformability, we suggest the visualisation of the 362 pad-substrate contact for varying roughness levels. A detailed interpretation of the effects of 363 variations in the complex phenomenon roughness [74] on tree frog attachment is challenging, 364 also because of the presence of mucus in the contact area. Based on a discussion of the rough-365 ness parameters computed from the bearing area curves of the used substrates (see Section 366 SI.2.1), one can conclude that the adhesion performance of tree frogs does not change despite 367 a continuous increase in total roughness height  $S_{tot}$  up to ca. 4 µm and in reduced peak height 368  $S_{pk}$  up to almost 3 µm between the smooth and the 15 µm substrate. As asperities are a primary 369 prerequisite for mechanical interlocking, this speaks against an appreciable contribution of me-370 chanical interlocking to tree frog attachment.

A comparison with the attachment performance of other bioadhesive systems from various clades on rough substrates helps to further explore the fundamentals of tree frog attachment. For example, the hairy toe pads of insects (e.g. *G. viridula*, [44]; *Leptinotarsa decemlineata*,

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374 [75]), arachnids (Philodromus dispar, [76]), and geckos (Gekko gecko, [77]) perform worse on 375 microrough substrates (typically in a range of 0.3–1.0 µm) than on smooth ones, which is gen-376 erally explained by a loss of effective contact area for dry adhesion. Similar observations were 377 made for the smooth adhesive pads of insects (Cydia pomonella, [78]) and arachnids (Ixodes 378 *ricinus*, [79]). Such a decline in attachment performance is clearly not observed for tree frogs 379 in the microrough regime. This may be explained by the high pad conformability, which pre-380 sumably facilitates a close pad-substrate contact and vdW force generation (Figure SI.10) on 381 microrough substrates, as proposed by [34]. Independence of the attachment performance on 382 roughness variations in between 0 µm and 12 µm has also been reported for the hairy adhesive 383 pads on the prey-capture apparatus of beetles in the genus Stenus [80]. The authors related this 384 independence partially to the small tip diameter  $(0.17-0.24 \,\mu\text{m})$  of the hairy structures, which 385 may widen the range of substrate roughness which the pads can conform to. The nanopillars on 386 tree frogs' toe pads have a similar size (diameter  $\approx 0.3 \,\mu$ m, [21]), possibly indicating a func-387 tional analogy. Alternatively, the compensatory action of capillary adhesion may explain these 388 findings, as suggested by the increase in tree frog adhesion on rough substrates when adding 389 liquid [43,50,52].

390 On macrorough substrates (i.e.  $R > 40 \,\mu\text{m}$ ), adhesion decreases gradually from  $R \approx 40 \,\mu\text{m}$ 391 to a local minimum at  $R \approx 200 \,\mu\text{m}$ , suggesting a gradually progressing failure of the involved 392 attachment mechanism(s) with increasing roughness. Such failure could be the cavitation of the 393 liquid meniscus and hence the loss of capillary adhesion [34,43,50]. Alternatively, a gradual 394 loss of effective contact area and of vdW forces with increasing roughness may lead to adhesive 395 failure, as aforementioned at lower roughness levels for the pads of lizards, insects, and arach-396 nids. For  $R > 200 \,\mu\text{m}$ , adhesion seemingly increases again. This may indicate mechanical in-397 terlocking of the whole toe pad with macroscopic surface asperities [43]. Here, the distal phal-398 anx, which in many species is pointy (with a tip diameter of ca. 60 µm in *H. cinerea* [68]) and extends distally into the subepidermal pad space [81], may act as 'internal claw'. Also, Huber et al. [77] suggested for geckos that individual attachment units (i.e. setae) can conform to the tops or sides of macroscopic substrate asperities. A similar mechanism could apply to the individual epidermal cells on tree frogs' toe pads (Figure SI.10).

403 Further work is required for a full explanation of the attachment performance of tree frogs 404 on rough substrates. In order to test for the potential role of vdW forces, we suggest the direct 405 quantification of the conformability of tree frog toe pads to micro- to macrorough substrates. 406 Furthermore, a detailed analysis of the meniscus geometry for different roughness levels is 407 needed to illuminate the role of capillary adhesion in tree frog attachment on rough substrates. 408 Little is known about the substrates and roughness levels which tree frogs experience in their 409 natural habitats [39]. As increasingly emerging in the field of gecko adhesion [82,83], we propose ecomorphological analyses of tree frogs' toe pads in order to explore correlations between 410 411 parameters of pad morphology (e.g. of the superficial epidermal cells [67]), ecology and natural 412 substrate properties, and attachment performance.

## 413 **4.2 Maximum attachment performance of tree frogs**

414 Using whole-animal rotation platform experiments, we measured mean tenacities of approximately 2.5 mN mm<sup>-2</sup> and a peak tenacity of 8.8 mN mm<sup>-2</sup>. These values are considerably 415 higher than the tenacities of around 1 mN mm<sup>-2</sup> measured in previous rotation platform studies 416 [25,26,51,66,67]. However, our results agree well with peak tenacities of up to ca. 8 mN mm<sup>-2</sup> 417 418 that were recently reported for single pads adhering to a microrough substrate [34]. The devia-419 tion in tenacity from earlier studies presumably relates to several factors. Most importantly, we 420 measured the instantaneous contact area before detachment of only the toe pads in contact, 421 which is smaller than the total surface area of all pads considered in previous studies. For ex-422 ample, we found that tree frogs can generate sufficient adhesion with only two limbs in contact, 423 approximately doubling the tenacity compared to a situation where all limbs are in contact. Moreover, the falling angle measured here exceeds the values reported in most other studies (Figure 6). This deviation may relate to the used setup, substrates, and the experimental animals. We specifically designed a stiff rotation platform to reduce vibrations, the induction of stress, and hence the chance of 'premature detachment' because of jumping of the animals. Moreover, we used frogs from a laboratory population that were accustomed to handling and the setup in pilot trials. Other studies [51,66,67] relied on wild-caught animals, which possibly are more susceptible towards stress during experimental handling.

431 Moreover, the frogs sometimes swing backwards upon detachment of the forelimbs (Figure 432 4), which results in inertial forces acting in addition to the static body weight on the pad-sub-433 strate interface. To estimate the magnitude of these inertial forces, the backwards swinging frog 434 may be simplified as an oscillating pendulum. The maximum tension acting in the string of a 435 pendulum is three times its static weight [84]. Assuming the swinging frog as pendulum, we estimate that the toe pads can withstand a maximum load of around 26 mN mm<sup>-2</sup>, which lies 436 close to the peak tenacity of 22 mN mm<sup>-2</sup> measured by Endlein et al. [70]. Assuming free fall 437 438 of the animals, inertial forces may be even higher, as indicated by peak forces of 130 mN (Os-439 teopilus septentrionalis, [26]) and 1270 mN (estimated from landing kinematics in Trachyceph-440 alus resinifictrix, [85]) generated by single pads and limbs during dynamic events.

441 In order to determine the 'true' maximum attachment performance of tree frogs in whole-442 animal measurements, an accurate quantification of the inertial loads acting on the toes during 443 dynamic events by a full inverse dynamics analysis is required. Moreover, rather than studying 444 the average attachment performance—as done here and in previous work—we suggest for fu-445 ture studies a focus on an in-depth analysis of peak performance situations (e.g. the peak per-446 formance for each individual on each substrate), which was not possible here due to a too low 447 sample number (n = 4). In combination with whole-animal studies, we suggest the execution of 448 single pad force measurements under specified dynamic loading conditions, as done in [70].

449 Overall, the results of this study indicate that the attachment performance of tree frogs may 450 be at least one order of magnitude higher than reported in earlier works. This makes tree frogs 451 an interesting model system for the development of biomimetic high-performance adhesives in 452 a wet environment. However, several questions remain unanswered: What is the real maximum 453 attachment performance of tree frogs? Which mechanisms do explain the generation of the high 454 attachment forces? Addressing these questions is relevant for the future design of biomimetic 455 adhesives inspired by tree frog toe pads. For example, Drotlef et al. [13] measured for a tree-456 frog-inspired PDMS surface covered with hexagonal micropillars tenacities of around 2-4 mN mm<sup>-2</sup>. Such technical adhesives may benefit significantly from a better understanding of 457 458 the mechanisms determining the maximum attachment performance of tree frogs.

## 459 **4.3 Problems and perspectives**

In this study, we used the rotation platform approach, which allows the collection of relatively
large data sets. Also, attachment can be studied for a relatively natural body posture, because
the artificial fixation of body parts performed in single pad studies [33,34,70] is not required.
However, rotation platform experiments also have drawbacks, which we discuss below.

464 Friction and adhesion are computed from the angles of falling and sliding (see equations 1 465 and 2), respectively. This approach allows a quick and easy quantification of whole-animal 466 adhesion and friction. However, the two forces are inherently coupled due to the performed 467 vector composition of the body weight. Hence, the normal load pulling the animal off the sub-468 strate (which equals adhesion at the moment of detachment) cannot be controlled independently 469 of the parallel load dragging the frog along the substrate (which equals static friction at the 470 onset of sliding; Figure 7), and vice versa. For example, sliding occurred at a range of angles, 471 for which the normal load was compressive as well as tensile, and at angles just before falling 472 parallel loads varied by approximately 50% of the body weight (Figure 7). In tree frogs, adhe-473 sion depends on the amount of the shear load before detachment [42,70], and—although to our knowledge not substantiated by measurements—friction also depends on normal loading (e.g.
in Coulomb friction [86] or in lubricated systems [87]). Therefore, the interdependency of normal and shear loading in rotation platform experiments presumably leads to an artificially increased variation of the measured forces.



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**Figure 7.** Interdependency of body-weight-normalised loads acting on a toe pad normal and parallel to the substrate in rotation platform experiments for the sliding ( $\alpha_{\parallel}$ , green circles) and falling ( $\alpha_{\perp}$ , red crosses) angles measured in this study.

482 For evaluation of the adhesive whole-animal performance of tree frogs, we measured the 483 instantaneous contact area of only the toe pads making contact with the substrate just before 484 detachment. In previous works [26,50,66,67], it was assumed that the contact area is formed by 485 the ventral surface areas of all toes of an individual, which presumably has led to an underesti-486 mation of the tenacity of tree frogs. Therefore, this study is an important step towards a more 487 accurate quantification of the attachment performance, and an understanding of the fundamen-488 tal attachment mechanisms of these animals. Such an understanding requires a detailed analysis 489 of the fractions of the overall contact area, which are effective in the generation of wet and dry 490 contact forces, respectively, and of the effective contact area on rough substrates. Such an anal-491 ysis cannot be achieved with the FTIR technique used here. In future studies, optical methods 492 (e.g. interference reflection microscopy [33,34]) or mechano-sensitive substrate coatings [88] 493 could be used to measure the detailed characteristics of the contact area.

494 The quantification of the frictional performance of tree frog toe pads is confounded by 495 several factors. During sliding, large fractions of the contact area are formed by the belly and 496 other body portions, which has also been shown elsewhere [52,70]. As the belly and other body 497 portions can contribute considerably to the attachment of tree frogs [52], the rotation platform 498 is inappropriate for the analysis of the frictional performance of tree frogs' toe pads. Also, when 499 analysing sliding at angles of around 90°, it seemed that individuals of *H. cinerea* started sliding 500 with their frontlimbs but could still resist sliding with their hindlimbs. This observation indi-501 cates that the assumption of equal loading of all toes is not fulfilled, as to be expected for the 502 required moment balance during steady attachment [68]. Such an unequal load distribution may 503 also occur at the angle of falling, reducing the effective measured adhesion. Differences in the 504 sliding of single toes may also explain the larger variation in sliding angles compared to the 505 measured falling angles. Lastly, it is difficult—if not impossible—to quantify the willingness 506 of a tree frog to attach to a substrate. We found a relatively large variation of the falling angles 507 per substrate and species, and of the number of successful trials per individual. In future rotation 508 platform experiments, such behavioural differences among individuals may be considered, for 509 example by including individual variability as random effect in the statistical model, as done in 510 this study.

511 Statistical models such as the linear mixed-effects model used here may help to cope with 512 the large variation in rotation platform studies. Temperature and relative air humidity should be 513 controlled to test for the effects of variations of these parameters on tree frog attachment. Com-514 plementarily, single pad measurements with controlled shear loads in adhesion measurements 515 and vice versa, as in [42,70], will help to deepen the understanding of tree frog attachment.

# 516 **5 Conclusions**

517 What is the maximum attachment performance of tree frogs on rough substrates? We address 518 this question by measuring the whole-animal attachment performance of the tree frog species 519 Litoria caerulea and Hyla cinerea on smooth, micro-, and macrorough substrates using a rota-520 tion platform setup. The adhesive performance of the toe pads of tree frogs is insensitive to-521 wards variations in substrate roughness up to a nominal roughness of ca. 40 µm. At higher 522 roughness levels up to  $R \approx 200 \,\mu\text{m}$ , adhesion decreases significantly compared to lower rough-523 ness levels. The absence of a sudden increase in attachment performance when increasing the 524 roughness from smooth to microrough, and the absence of a stepwise decline in attachment 525 performance when further increasing the roughness negate a contribution of mechanical inter-526 locking to tree frog attachment. Further work is required to elucidate if variations in substrate 527 roughness affect attachment force generation by capillary adhesion or by van der Waals inter-528 actions (or by both mechanisms). Tree frogs were able to remain attached with only two limbs 529 in contact with an overhanging substrate. In agreement with recent studies, the tenacity of the toe pads reaches peak values of up to 8.8 mN mm<sup>-2</sup>, which is almost one order of magnitude 530 531 higher than reported previously. Inertial forces have to be considered in the quantification of 532 the maximum attachment performance, and we estimate that the maximum tenacity of tree frogs' toe pads may be as much as  $26 \text{ mN mm}^{-2}$ . 533

## 534 Acknowledgements

535 This work is part of the research programme 'Secure and gentle grip of delicate biological tis-536 sues' with project number 13353, which is financed by the Netherlands Organisation for Scien-537 tific Research (NWO). We thank the following people for their valuable contributions. D. van 538 de Pol, S. van Woudenberg, S. Visser, and M. ter Veld from the CARUS research facility at 539 Wageningen University & Research (WUR), Wageningen, The Netherlands, set up and took 540 care of the populations of frogs used in this research. J. Belgraver and H. Meijer from the Tech-541 nical Development Studio, WUR, assisted with designing and manufacturing the experimental 542 setup. A. Hagmayer and C. Voesenek, Experimental Zoology Group, WUR, helped with statis-543 tical analysis and with MATLAB scripting, respectively. W.J.P. Barnes, Institute of Molecular,

- 544 Cell and Systems Biology, University of Glasgow, UK, provided helpful feedback on the ex-
- 545 perimental setup and animal housing. E.-J. Bakker, Biometris, WUR, provided advice on the
- 546 statistical analysis, and R. Morssinkhof advised us on the housing of amphibians.

# 547 Author contributions

- 548 Conception of the study: JKAL, AR, JLvL; Development and testing of experimental setup:
- 549 JKAL, RP, AR; Data collection: AR, JKAL; Data analysis: JKAL, AR; Data interpretation:
- 550 JKAL, AR, JLvL; Drafting of the manuscript and figures: JKAL; Literature analysis: JKAL,
- 551 SNG; Substrate preparation and characterisation methodology, and equipment: SNG, AK; Crit-
- 552 ical revision and approval: all authors.

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