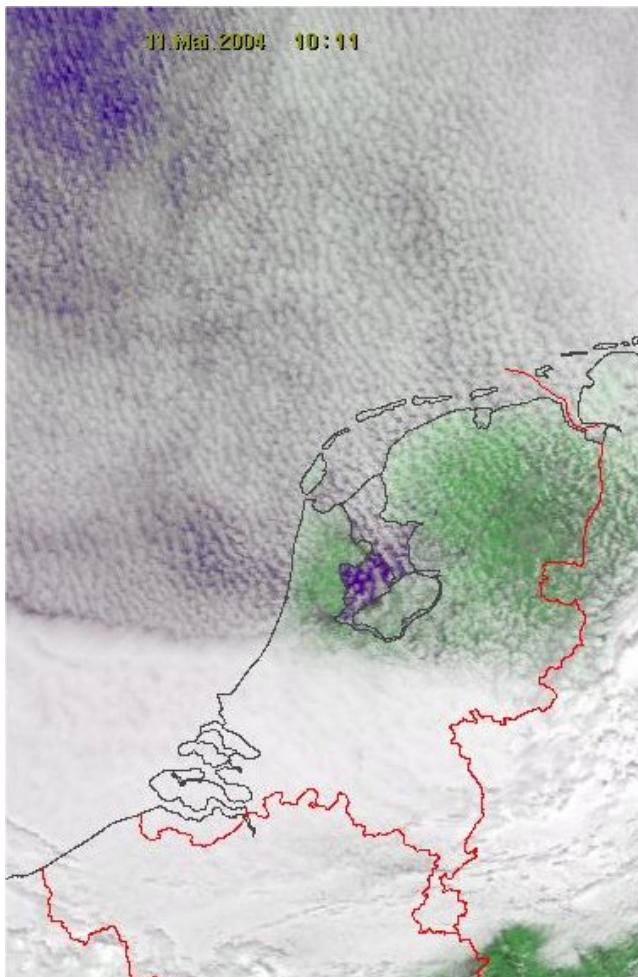


Entrainment rates in stratocumulus computed from a 1D TKE model



Stephan de Roode

KNMI

Turbulent mixing and entrainment in simple closure models

Computation of the flux

$$\overline{w' \psi} = -K_\psi \frac{\partial \bar{\psi}}{\partial z}$$

Representation of entrainment rate w_e

1. K-profile $K = w_e \Delta z$, w_e from parametrization
2. TKE model $K(z) = TKE(z)^{1/2} l(z)$, w_e implicit

Question

Does w_e from a TKE model compare well to w_e from parametrizations?

Entrainment parameterizations designed from LES of stratocumulus (*Stevens 2002*)

- Nicholls and Turton (1986)

$$w_e = \frac{2.5 A W_{NE}}{\Delta\theta_{v,NT} + 2.5 A (T_2 \Delta\theta_{v,dry} + T_4 \Delta\theta_{v,sat})}$$

- Lilly (2002)

$$w_e = \frac{A_{DL} W_{NE,DL}}{\Delta\theta_{v,DL} + A_{DL} (L_2 \Delta\theta_{v,dry} + L_4 \Delta\theta_{v,sat})}$$

- Stage and Businger (1981)
Lewellen and Lewellen (1998)
VanZanten et al. (1999)

$$w_e = \frac{A W_{NE}}{T_2 \Delta\theta_{v,dry} + T_4 \Delta\theta_{v,sat}}$$

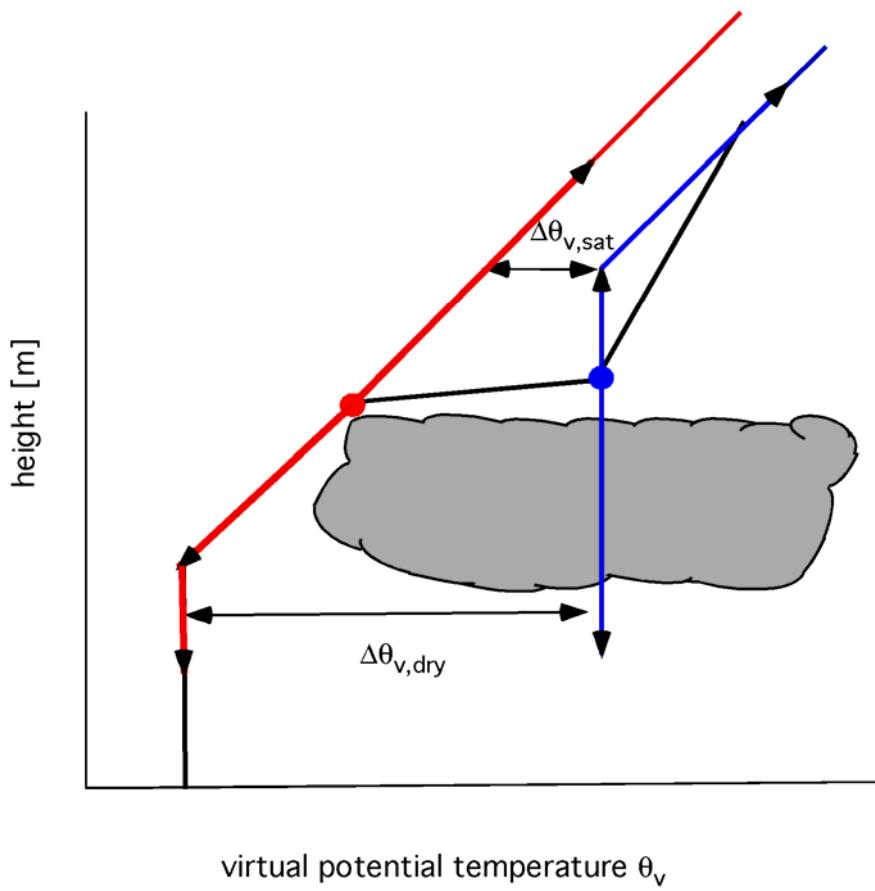
- Lock (1998)

$$w_e = \frac{2 A_{AL} W_{NE} + \alpha_t A_W \Delta F_L / (\rho c_p)}{\Delta\theta_v}$$

- Moeng (2000)

$$w_e = \frac{A_M \overline{w' \theta_l'} + \Delta F_L (3 - e^{-\sqrt{b_m L}}) / (\rho c_p)}{\Delta\theta_l}$$

Stability jumps



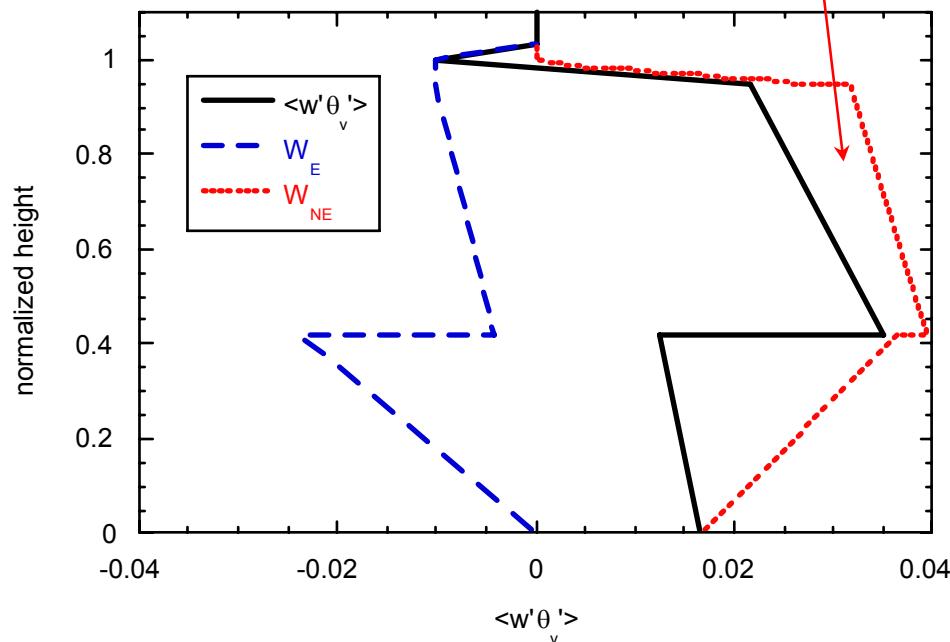
$\Delta\theta_{v,sat} = \Delta_2$ (the CTEI criterion, Randall 1980, Deardorff 1980)

Solve entrainment rate for a stratocumulus-topped boundary layer

$$w_e = A \frac{w_*^3}{g H \Delta \theta_v}$$

solve for
entrainment rate
 \Rightarrow

$$w_e = \frac{2.5 A W_{NE}}{\Delta \theta_v + 2.5 A (T_2 \Delta \theta_{v,dry} + T_4 \Delta \theta_{v,sat})}$$

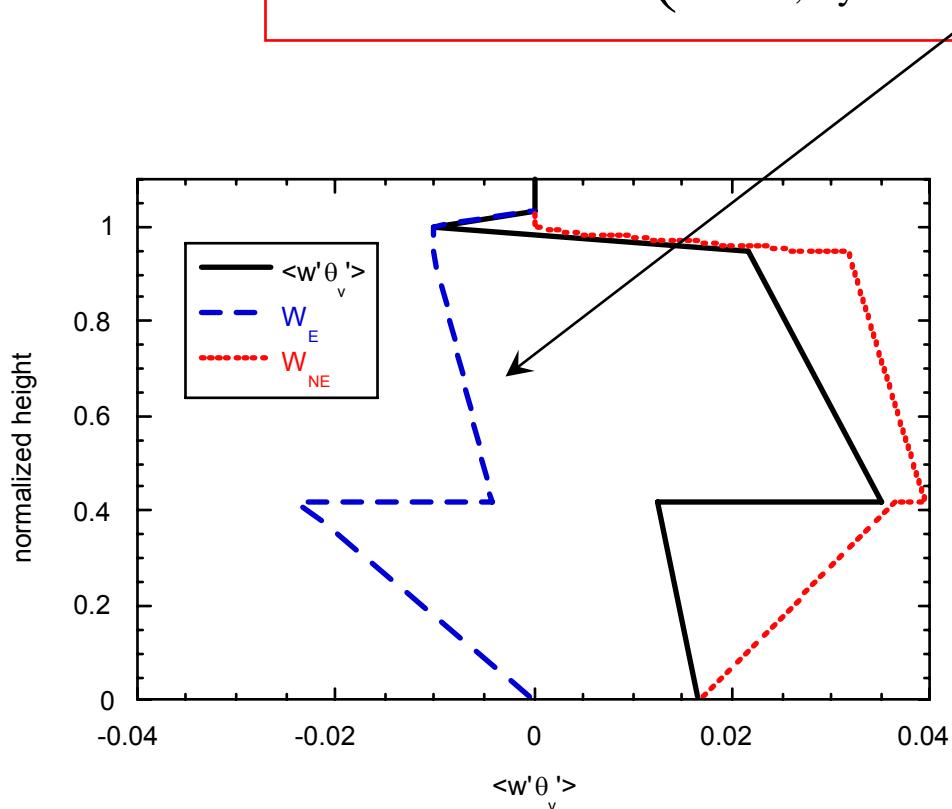


Solve entrainment rate for a stratocumulus-topped boundary layer

$$w_e = A \frac{w_*^3}{g H \Delta \theta_v}$$

solve for
entrainment rate
 \Rightarrow

$$w_e = \frac{2.5 A W_{NE}}{\Delta \theta_v + 2.5 A (T_2 \Delta \theta_{v,dry} + T_4 \Delta \theta_{v,sat})}$$

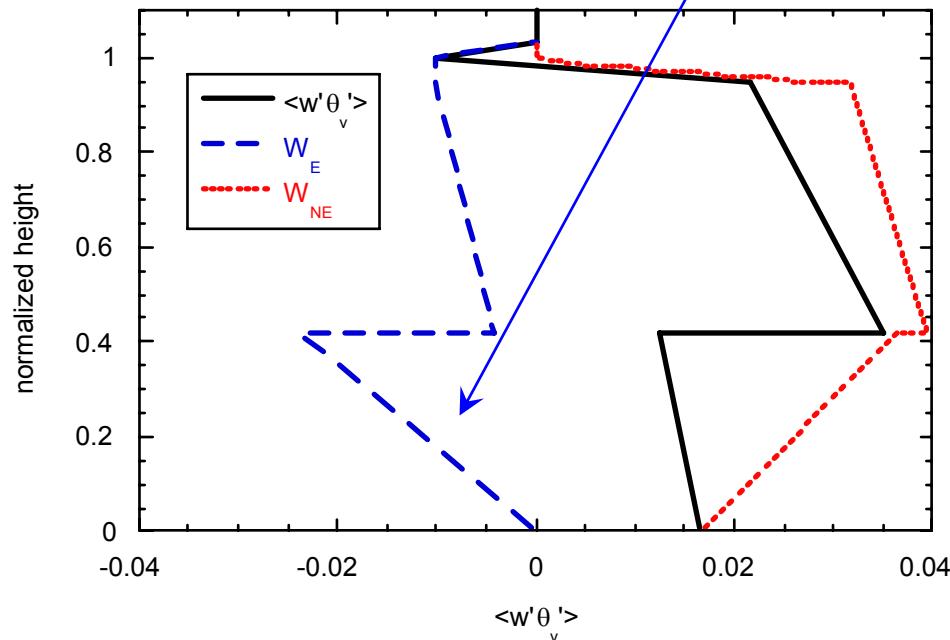


Solve entrainment rate for a stratocumulus-topped boundary layer

$$w_e = A \frac{w_*^3}{g H \Delta \theta_v}$$

solve for
entrainment rate
 \Rightarrow

$$w_e = \frac{2.5 A W_{NE}}{\Delta \theta_v + 2.5 A (T_2 \Delta \theta_{v,dry} + T_4 \Delta \theta_{v,sat})}$$



Entrainment parameterizations designed from LES of stratocumulus (*Stevens 2002*)

- Nicholls and Turton (1986)

$$w_e = \frac{2.5 A W_{NE}}{\Delta\theta_{v,NT} + 2.5 A (T_2 \Delta\theta_{v,dry} + T_4 \Delta\theta_{v,sat})}$$

- Lilly (2002)

$$w_e = \frac{A_{DL} W_{NE,DL}}{\Delta\theta_{v,DL} + A_{DL} (L_2 \Delta\theta_{v,dry} + L_4 \Delta\theta_{v,sat})}$$

- Stage and Businger (1981)
Lewellen and Lewellen (1998)
VanZanten et al. (1999)

$$w_e = \frac{A W_{NE}}{T_2 \Delta\theta_{v,dry} + T_4 \Delta\theta_{v,sat}}$$

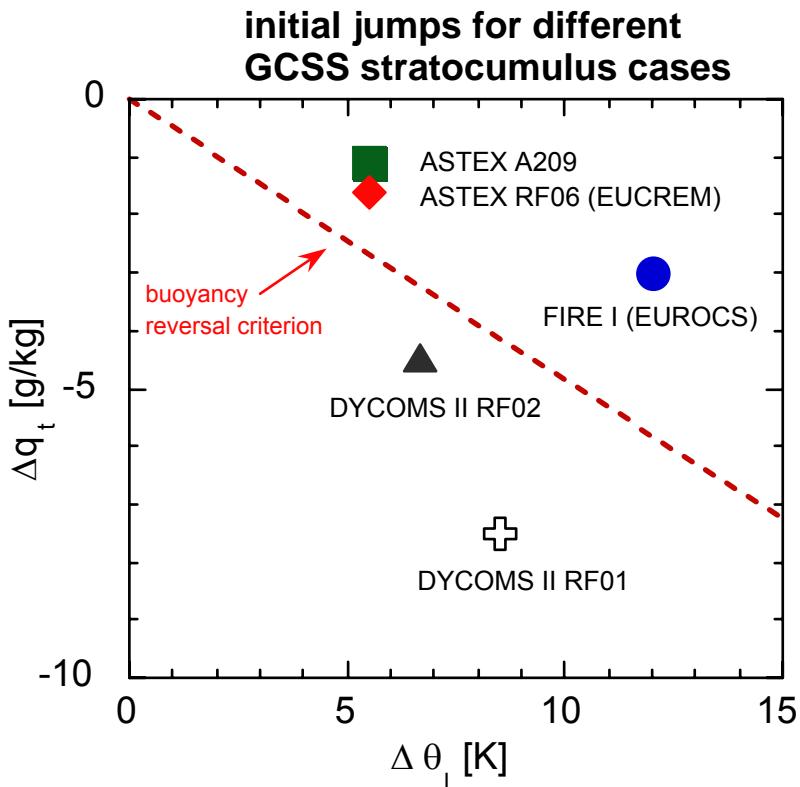
- Lock (1998)

$$w_e = \frac{2 A_{AL} W_{NE} + \alpha_t A_W \Delta F_L / (\rho c_p)}{\Delta\theta_v}$$

- Moeng (2000)

$$w_e = \frac{A_M \overline{w' \theta_l'} + \Delta F_L (3 - e^{-\sqrt{b_m L}}) / (\rho c_p)}{\Delta\theta_l}$$

GCSS stratocumulus cases

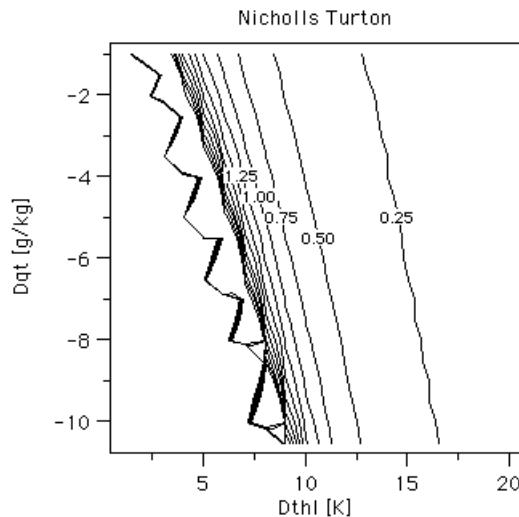
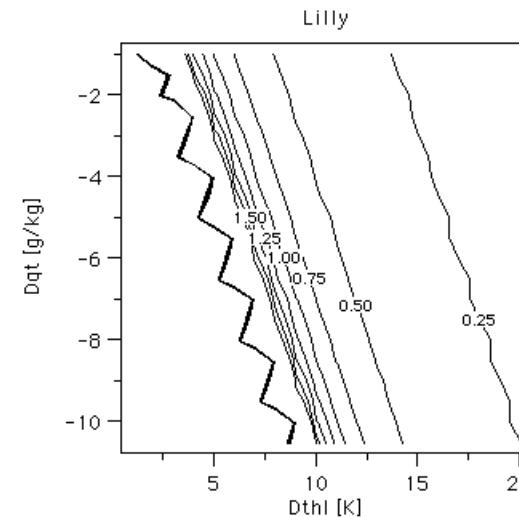
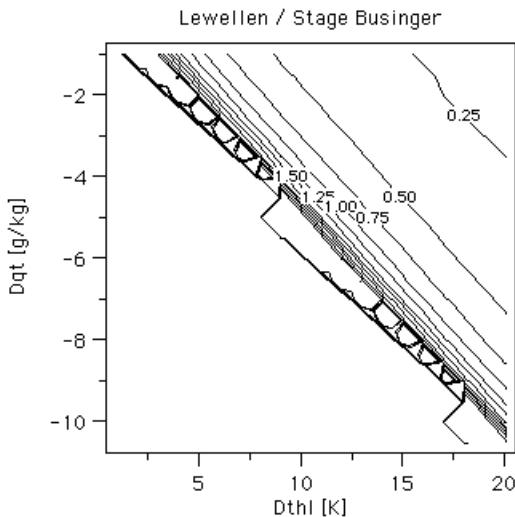
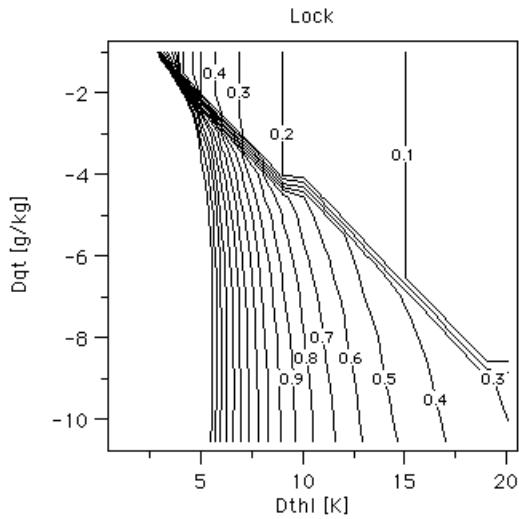
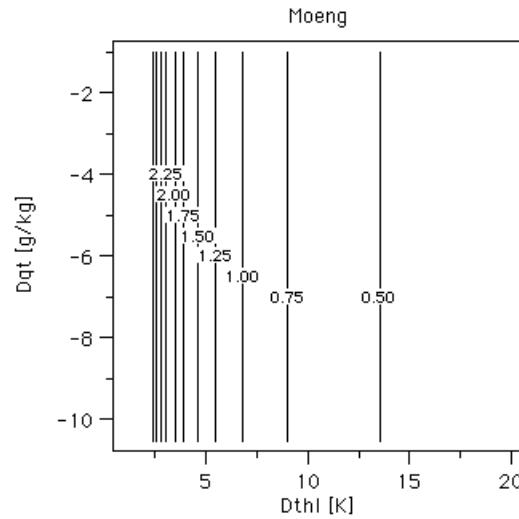
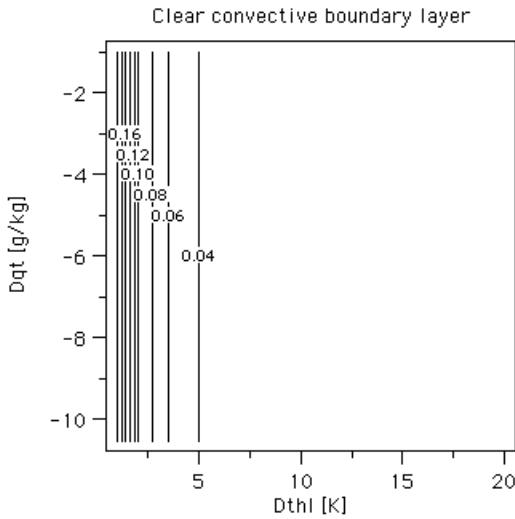


ASTEX A209 boundary conditions

cloud base height	= 240 m
cloud top height	= 755 m
sensible heat flux	= 10 W/m ²
latent heat flux	= 30 W/m ²
longwave flux jump	= 70 W/m ²
max liq. water content	= 0.5 g/kg
LWP	= 100 g/m ²
Δθ _l	= 5.5 K
Δq _t	= -1.1 g/kg

fill in these values in parameterizations,
but vary the inversion jumps $\Delta\theta_l$ and Δq_t

Entrainment rate [cm/s] sensitivity to inversion jumps - Boundary conditions as for ASTEX A209



Some details of the TKE model simulation

- TKE equation

$$\frac{\partial \bar{E}}{\partial t} = \frac{g}{\theta_v} \bar{w' \theta_v'} - \bar{u' w'} \frac{\partial U}{\partial z} - \bar{v' w'} \frac{\partial V}{\partial z} - \frac{\partial}{\partial z} \left(\bar{w' E'} + \frac{\bar{w' p'}}{\rho} \right) - \varepsilon$$

- Flux

$$\bar{w' \psi'} = -c_\psi \sqrt{TKE} \ell \frac{\partial \bar{\psi}}{\partial z}$$

- 'integral' length scale

$$\frac{1}{\ell} = \frac{1}{\ell_u} + \frac{1}{\ell_d}$$

(Lenderink & Holtslag 2004)

- buoyancy flux weighed with cloud fraction

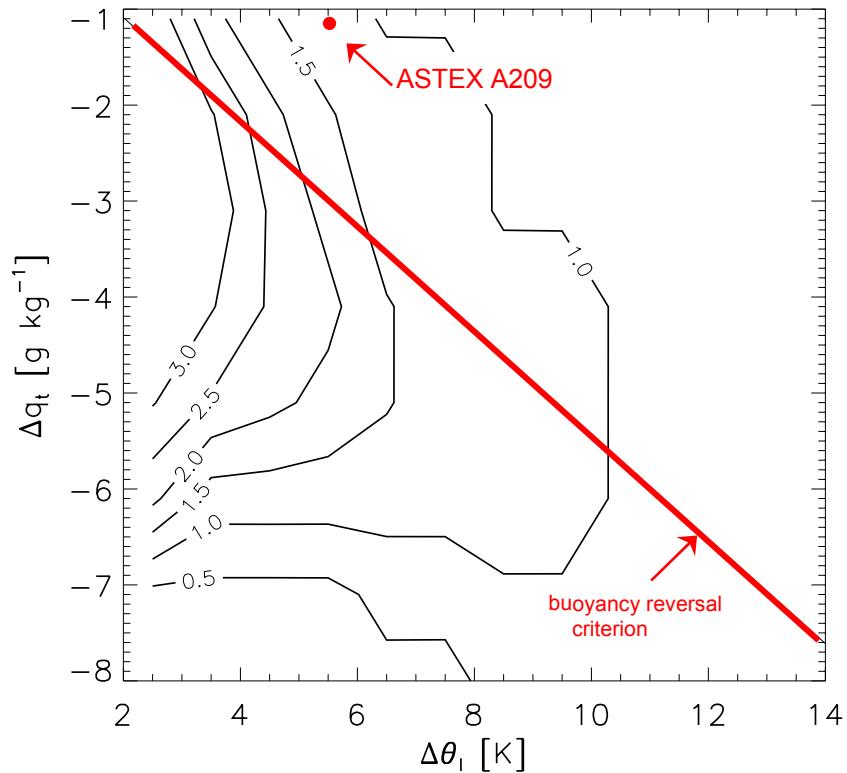
$$\bar{w' \theta_v'} = -c_H \sqrt{\bar{E}} \ell \left[\sigma \left(A_w \frac{\partial \bar{\theta}_1}{\partial z} + B_w \frac{\partial \bar{q}_t}{\partial z} \right) + (1 - \sigma) \left(A_d \frac{\partial \bar{\theta}_1}{\partial z} + B_d \frac{\partial \bar{q}_t}{\partial z} \right) \right]$$

- ASTEX A209 forcing and initialization

- $\Delta t = 60$ s , $\Delta z = 5$ m

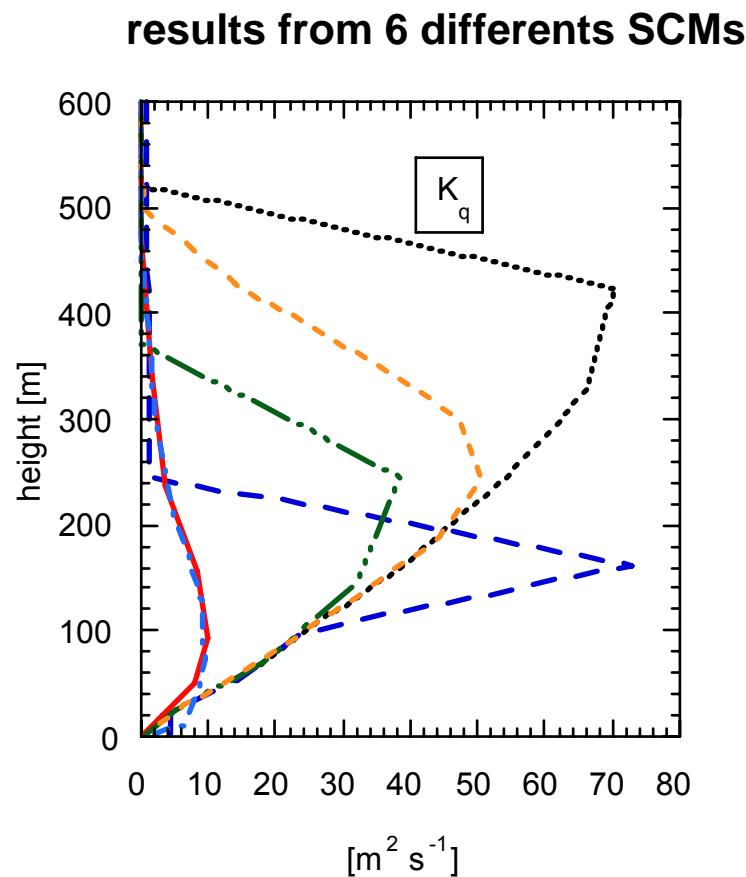
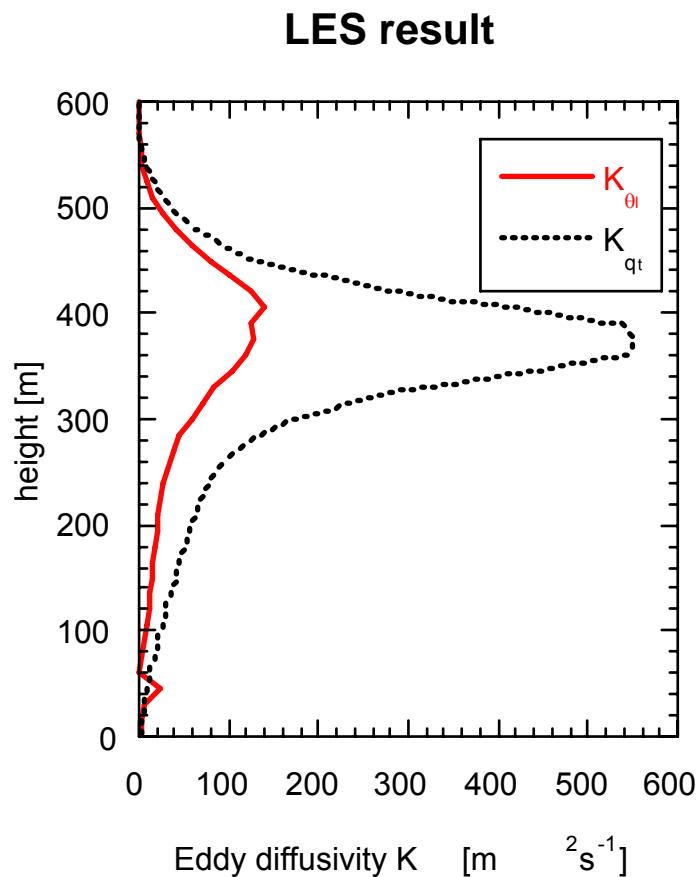
- Mass flux scheme turned off, no precipitation

Entrainment sensitivity to inversion jumps from a TKE model



- Moisture jump sensitivity
- No buoyancy reversal: entrainment rates slightly larger than parameterizations
- Buoyancy reversal: entrainment rates decrease

Eddy diffusivities in K-closure models - Results from the EUROCS stratocumulus case



- LES: Eddy diffusivities for heat and moisture differ (like CBL, Wyngaard and Brost 1980)
- SCM: typically smaller values than LES

Should we care about eddy diffusivity profiles in SCMs?

Simple experiment

1. Prescribe surface latent and sensible heat flux

2. Prescribe entrainment rate

⇒ Given jumps of θ_l and q_t , fluxes at BL top are fixed

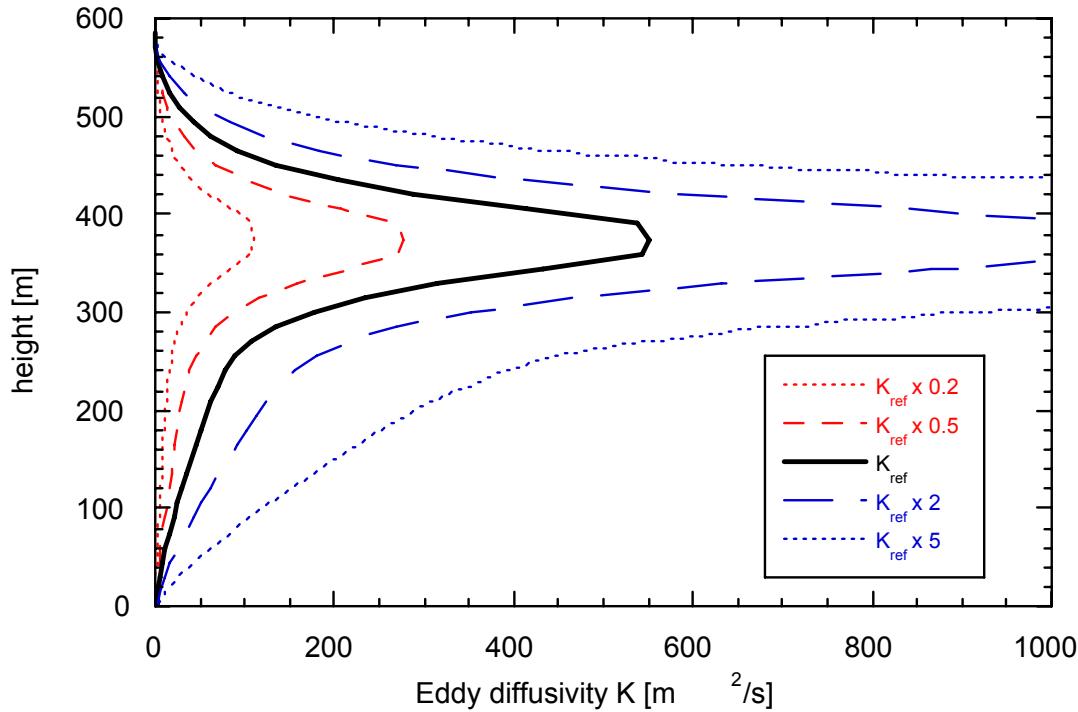
3. Consider quasi-steady state solutions

⇒ fluxes linear function of height

Consider mean state solutions from

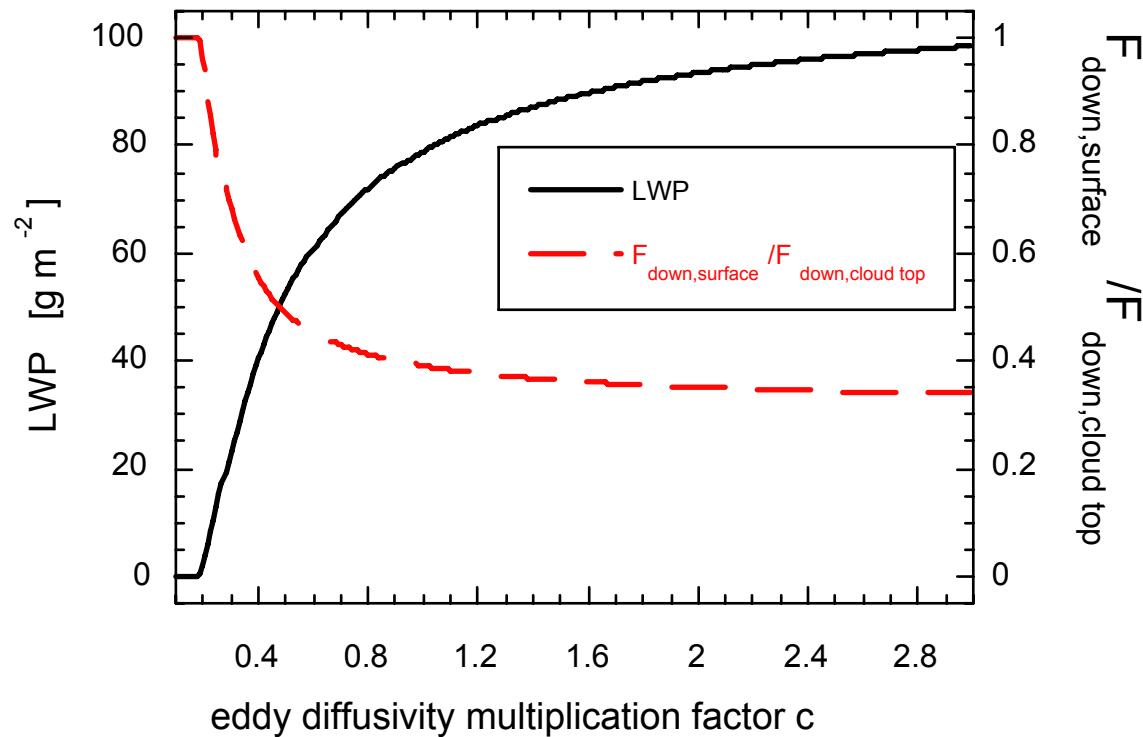
$$\bar{\psi}(z) = \psi_0 - \int_{z'=0}^{z'=z} \frac{\overline{w' \psi'}(z')}{K_\psi(z')} dz'$$

Vary eddy diffusivity profiles with a constant factor

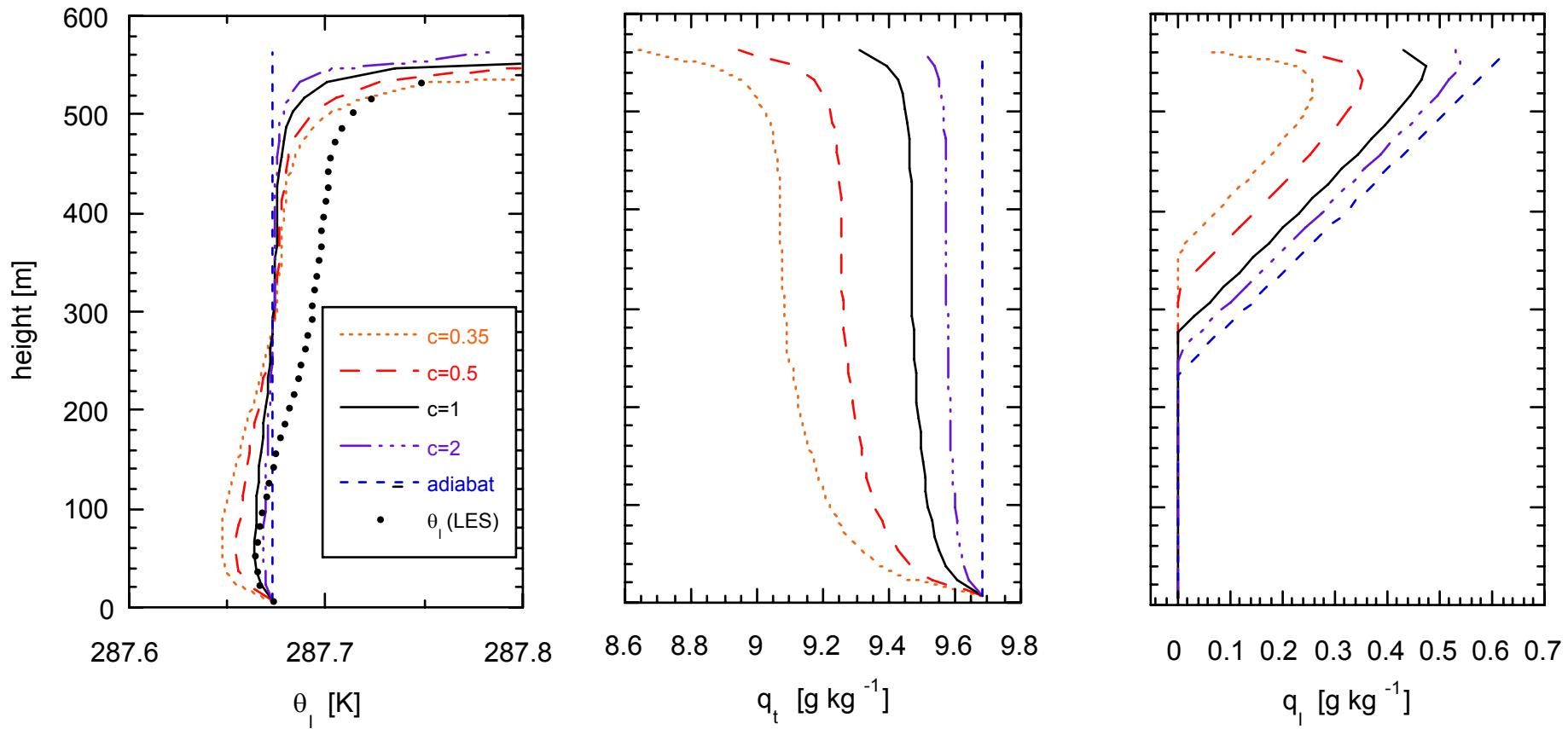


- K_{ref} is identical to K_{qt} from LES
- $0.2 \times K_{ref}$ is very close to K_{ql} from LES

LWP and shortwave radiation (normalized) solutions as a function of the eddy-diffusivity multiplication factor c



Mean state solutions



Similar K profiles for heat and moisture - Interpretation

Gradient ratio:

$$\frac{\overline{\partial \theta_1} / \partial z}{\overline{\partial q_t} / \partial z} = \frac{\overline{w' \theta_1'} / K}{\overline{w' q_t'} / K} = \frac{H}{LE} \frac{L_v}{c_p} \quad (K \text{ drops out})$$

Typical flux values near the surface for marine stratocumulus:

$$H=10 \text{ W/m}^2 \text{ and } LE = 100 \text{ W/m}^2$$

Then a 0.1 K decrease in θ_1 corresponds to a change of 0.4 g/kg in q_t

The larger the latent heat flux LE, the larger the vertical gradient in q_t will be!

Conclusions

TKE model

- appears to be capable to represent realistic entrainment rates

Eddy diffusivity experiments

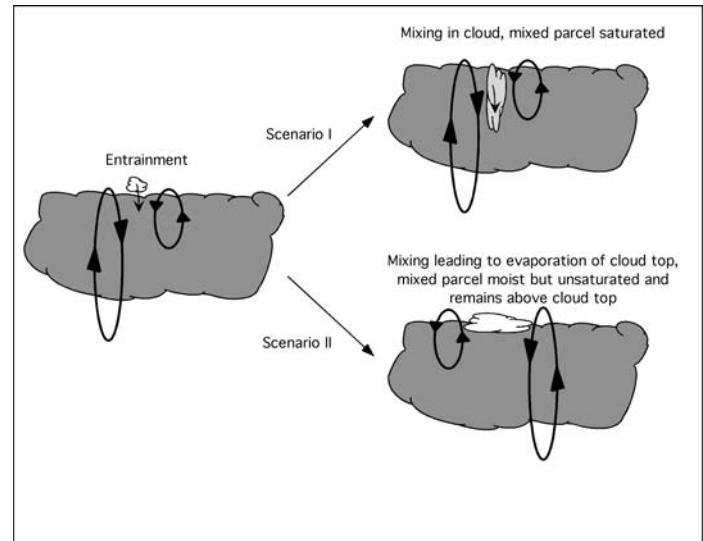
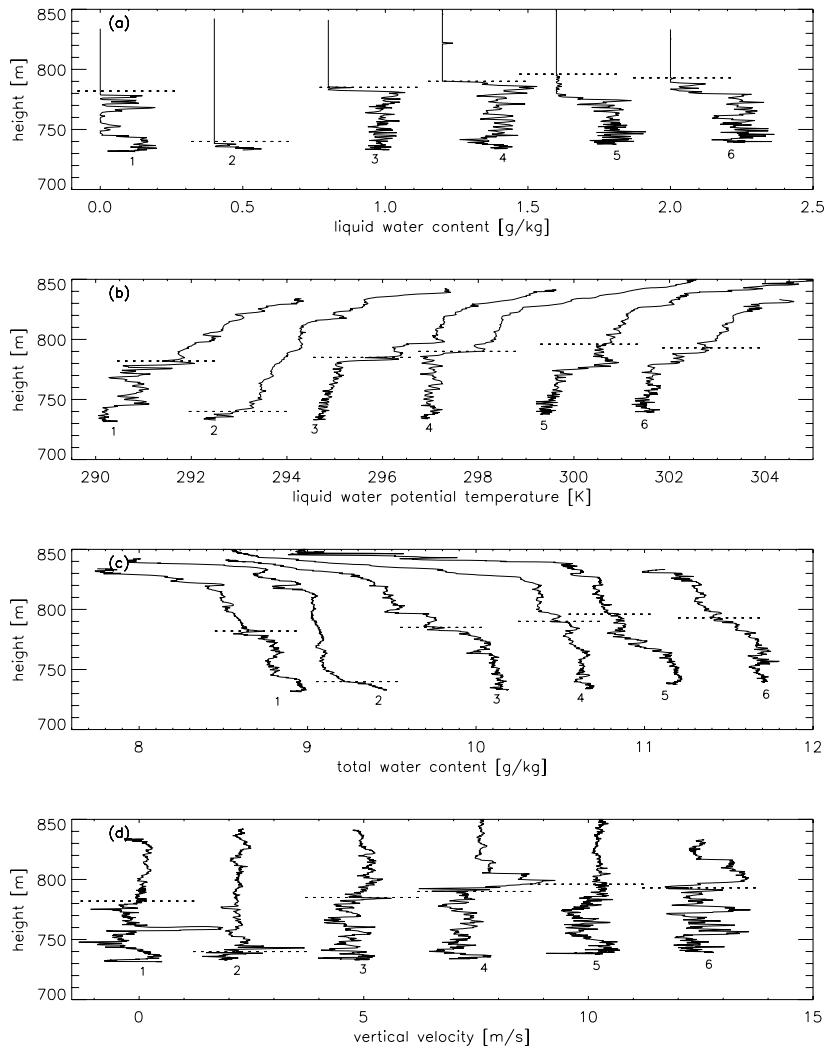
- stratocumulus may disappear by incorrect BL internal structure, even for 'perfect' entrainment rate
- observations often show adiabatic LWP (Albrecht et al. 1990, Bretherton et al. 2004), suggesting large values for K_{qt}

Recommendation

- pay more attention to K-profiles from LES

<http://www.knmi.nl/~roode/publications.html>

FIRE I stratocumulus observations of the stratocumulus inversion structure



de Roode and Wang : Do stratocumulus clouds detraining? FIRE I data revisited. BLM, in press