

NN31545.1500

BIBLIOTHEEK
STARINGENBOUW

NOTA 1500 ^I

JANUARI 1984

Instituut voor Cultuurtechniek en Waterhuishouding
Wageningen

COMPUTER PROGRAM "CAPSEV" TO CALCULATE:

I. SOIL HYDRAULIC CONDUCTIVITY FROM GRAIN SIZE DISTRIBUTION

II. STEADY STATE WATER FLOW IN LAYERED SOIL PROFILES

Ir. J.G.Wesseling, Ing. G.W.Bloemen and Ing. W.A.J.M. Kroonen

Nota's van het Instituut zijn in principe interne communicatie-
middelen, dus geen officiële publikaties.

Hun inhoud varieert sterk en kan zowel betrekking hebben op een
eenvoudige weergave van cijferreeksen, als op een concluderende
discussie van onderzoeksresultaten. In de meeste gevallen zullen
de conclusies echter van voorlopige aard zijn omdat het onderzoek
nog niet is afgesloten.

Bepaalde nota's komen niet voor verspreiding buiten het Instituut
in aanmerking.

CENTRALE LANDBOUWCATALOGUS



0000 0125 3976

USN 204603-02

CONTENTS

INTRODUCTION

1. Calculation of $K(h)$ relationship from texture and organic matter content	1
2. Steady state soil water flow	9
3. Alternative functions to describe the $K(h)$ relationship	11
4. The program	15
5. Examples	20

REFERENCES

Listing of the program CAPSEV

INTRODUCTION

Program "CAPSEV" calculates soil hydraulic conductivity from soil texture and organic matter content according to the method described by BLOEMEN(1980a).

Knowing the hydraulic conductivity the program calculates steady state water flow in a heterogeneous soil in which the groundwater table is present. The flow may be in either upward direction, capillary rise, or in downward direction, infiltration.

In addition to the hydraulic conductivity function of BLOEMEN(1980a) some alternative functions to describe the hydraulic conductivity can be applied in the program.

The program "CAPSEV" is a fully interactive program. Examples of input and output are given.

1. CALCULATION OF K(h) RELATIONSHIP FROM TEXTURE AND ORGANIC MATTER CONTENT

1.1. Hydraulic conductivity relationship

BLOEMEN (1980a: Fig.9, eq.17) modified the Brooks and Corey expression in order to account for hysteresis. He obtained the following hydraulic conductivity scanning function (see Fig.1, line s):

$$K = K_e \quad \text{for} \quad h \geq h_w \quad (1)$$

$$K = K_e \left[\frac{h_w}{h} \right]^n \quad \text{for} \quad h < h_w \quad (2)$$

where $K =$ hydraulic conductivity [cm.day⁻¹]

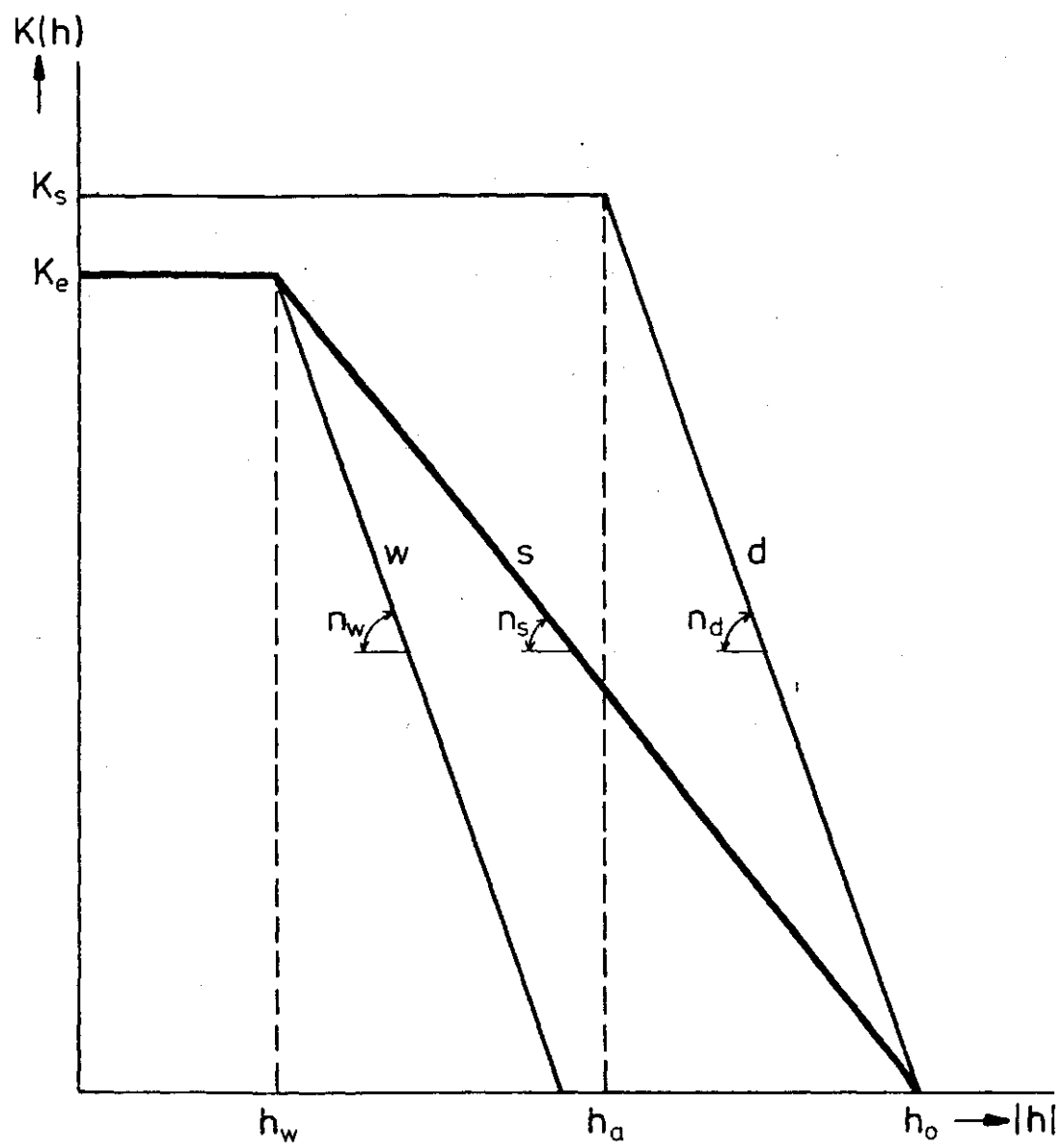


Fig. 1. $K(h)$ description according to Bloemen(1980a).

K_e = effective conductivity [cm.day^{-1}] attained after rewetting, assuming $K_e = 0.5 K_s$, where K_s is the saturated conductivity
 h_a = pressure head [cm]
 h_w = pressure head [cm] at which K_e is attained after rewetting
 n_s = slope of the average scanning curve between wetting and desorption

According to BLOEMEN (1980a) the eqs. (1) and (2) can in terms of the desorption curve (fig. 1, line d) be rewritten as:

$$K_e = 0.5 K_s \quad \text{for} \quad h \geq h_a \quad (3)$$

$$K_e = 0.5 K_s \left[\frac{h/r_a}{h} \right]^{n_s} \quad \text{for} \quad h < h_a \quad (4)$$

in which

K_s = saturated conductivity [cm.day^{-1}]
 h_a = pressure head [cm] at air entry point
 r = factor to convert h_a into h_w , depending on type of soil,
 i.e. $r = h_w / h_a$
 n_s = slope of the scanning curve (Fig.1, line s)

The expression for n_s is (BLOEMEN, 1980a, eq. 22):

$$n = \frac{\log_{10} \left[\frac{2 \left[\frac{h}{a} \right] \left[\frac{h}{0} \right]}{\left[\frac{h/r}{a} \right] \left[\frac{h}{0} \right]} \right]}{s} \quad (5)$$

where

- h = pressure head [cm] at which K becomes negligibly small
- 0 (see Fig. 1)
- n = slope of the desorption curve, Fig.1, line d
- d

It will now be explained how the parameters K , h , r , h and n can be found.

1.2 Computation of parameters of the hydraulic conductivity function from grain size distribution and organic matter content

BLOEMEN(1980a), BLOEMEN and VAN GILS(1982) described a method to calculate hydraulic conductivity as a function of the soil texture (grain size distribution) and organic matter content.

For applying the method three categories of soils are distinguished:

- Mineral soils: grain size distribution and organic matter content are required.
- Fen peat: only bulk density is required.
- High bog peat: only bulk density is required.

Grain size distribution data, are given either as percentages or fractions of the total amount of grains. For an example see Table 1.

Table 1. Example of the grain size distribution and humus content of a marine clay soil consisting of five different layers.

Description	Thick. (CM)	Hum. %	S - values in microns							
			2.	16.	50.	75.	105.	150.	210.	
Sandy clay	15.0	5.4	19.2	11.3	43.8	12.6	9.4	2.6	1.2	
Heavy clay	35.0	3.7	50.0	23.9	21.5	2.3	1.3	0.5	0.5	
Peat	25.0		FEN PEAT, BULK DENSITY= 0.24 G . CM**3							
Clayey sand	75.0	0.8	6.6	2.7	13.9	38.1	34.9	3.7	0.1	
Sand	150.0	0.6	3.3	2.6	11.9	19.8	27.7	27.4	6.7	

The grain size distribution index, f , is defined as:

$$f = \frac{\sum_{i=2}^n \left(\frac{P_i - P_{i-1}}{S_i - S_{i-1}} \right)}{\sum_{i=2}^n (P_i - P_{i-1})} \quad (6)$$

where

$$f = \frac{\sum_{i=2}^n (P_i - P_{i-1}) \frac{\log(P_i / P_{i-1})}{\log(S_i / S_{i-1})}}{\sum_{i=2}^n (P_i - P_{i-1})} \quad (7)$$

in which

P_i = cumulative weight percentage

S_i = size interval limit [μ]

The saturated conductivity, K_s , can be found from the following equations:

for mineral soils:

$$K_s = 0.02 M_d^{1.93} f^{-0.74} \quad [\text{cm.day}^{-1}] \quad (8)$$

for fen peat:

$$K_s = 0.00266 g_b^{-3.625} \quad [\text{cm.day}^{-1}] \quad (9)$$

for high bog peat:

$$K_s = 0.0036 g_b^{-2.83} \quad [\text{cm.day}^{-1}] \quad (10)$$

where M_d is the median grain size [μ], (Note: M_d differs from M_{50})

g_b is the dry bulk density [g.cm^{-3}]

The value of h_a is calculated according to:

for mineral soils:

$$h_a = -2914 M_d^{-0.96} f^{0.79} \quad [\text{cm}] \quad (11)$$

for fen peat:

$$h_a = -416 g_b^{1.12} \quad [\text{cm}] \quad (12)$$

for high bog peat:

$$h = \frac{-794}{a} \frac{g}{b} \quad [cm] \quad (13)$$

The value of the reduction factor r is depending only on the type of soil:

$$\begin{aligned} r &= 4.5 && \text{for sandy soils with } M_d > 50 \\ r &= 2.9 && \text{for clayey soils with } M_d \leq 50 \\ r &= 3.1 && \text{for fen peat} \\ r &= 1.9 && \text{for high bog peat with } g_b < 0.1 \text{ g.cm}^{-3} \\ r &= 3.4 && \text{for high bog peat with } g_b \geq 0.1 \text{ g.cm}^{-3} \end{aligned}$$

The value of h_0 can be found from the grain size distribution factor f_0 and the median grain size M_d . To find a general relation between h_0 , f_0 and M_d , a large amount of soil profiles from the archives of the Soil Survey Institute in Wageningen was investigated. On the base of an iterative method, starting from initially assumed values of h_0 (BLOEMEN and VAN GILS, 1982, section 2.10), relationships between h_0 , f_0 and M_d were found. The results of these calculations are presented in fig. 2.

The slope n_d of the desorption curve can be calculated according to:

for mineral soils:

$$n_d = 1.41 + 4.536 \left(e^{0.3 f_0} - 1 \right) - 0.75 f_0^{1.6} \log H \quad (14)$$

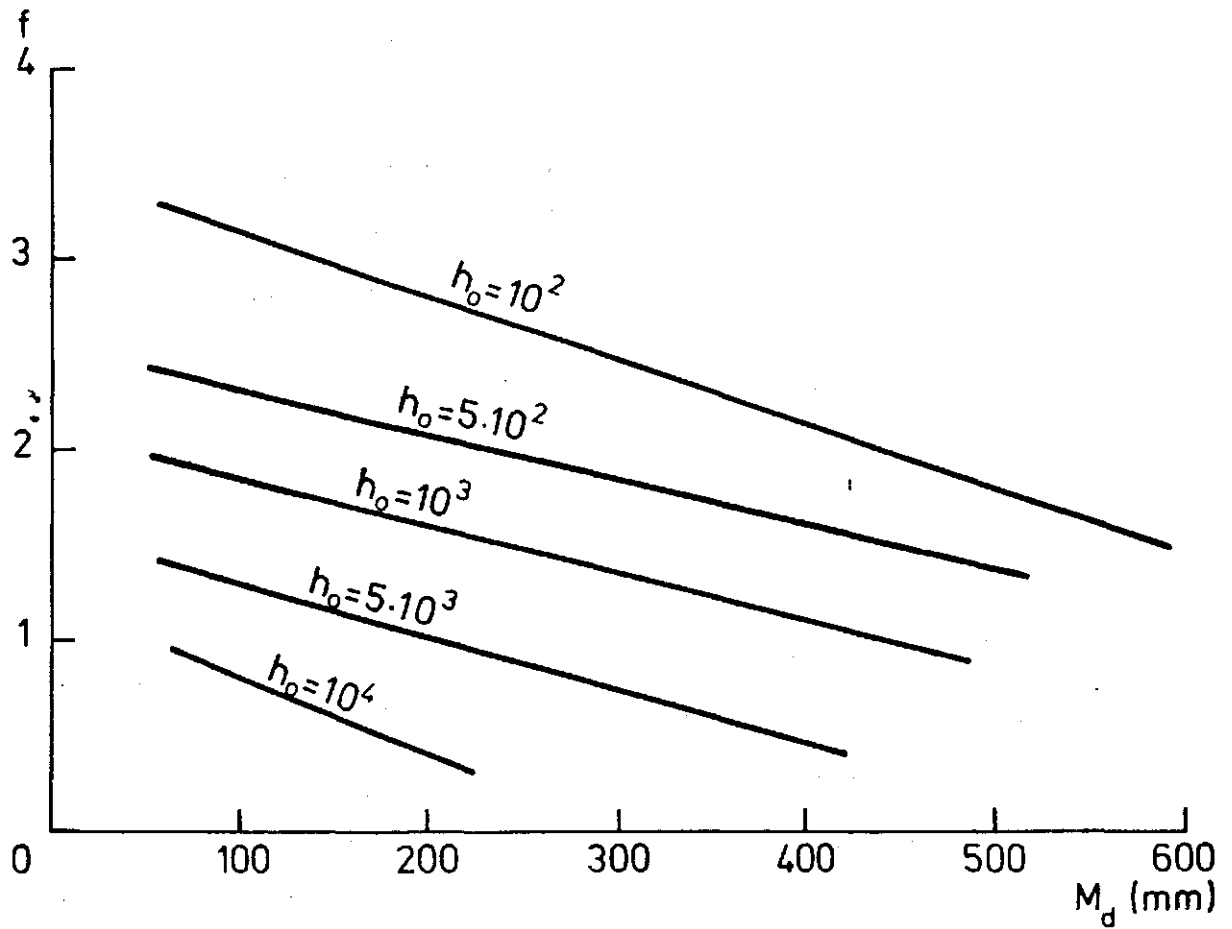


Fig. 2. Values of h of existing combinations of M and f . It is assumed that the M -values given for the lines are valid for the entire area between two lines.

for fen peat:

$$n_d = 2.54 - 2.42 \frac{g}{b} \quad (15)$$

for high bog peat:

$$n_d = 2.57 - 2.27 \frac{g}{b} \quad (16)$$

in which H is the humus content of the soil [%].

If in a layer horizontal cracking occurs, the following corrections should be made on the values of h_a/r and n_s (BLOEMEN, 1980a,b;

BLOEMEN and VAN GILS, 1982):

$$\frac{h_a}{r} = 100 * \left[\begin{array}{cc} h_a & h_s \\ 0.01 & \frac{n_s}{n_s + 1.7} \end{array} \right] \quad \text{for } \frac{h_a}{r} > -100 \quad (17)$$

$$n_s = n_s + 1.7 \quad (18)$$

2. STEADY STATE SOIL WATER FLOW

Steady state soil moisture flow in a 1-dimensional, vertical, soil profile is governed by Darcy's equation:

$$q = -K(h) \left(\frac{dh}{dz} + 1 \right) \quad (19)$$

where

q = soil moisture flux density [$\text{cm}^3 \cdot \text{cm}^{-2} \cdot \text{day}^{-1}$]

z = vertical coordinate with origin at the soil surface, directed positive upward [cm]

Rearranging eq.(19) yields:

$$\frac{dz}{dh} = \frac{-1}{1+q/K(h)} \quad (20)$$

Integration of eq.(20) for a soil profile consisting of m layers starting at the groundwater table, where $h=0$, results in:

$$z = - \int_0^{h_1} \frac{dh}{1+q/K(h)} - \int_{h_1}^{h_2} \frac{dh}{1+q/K(h)} - \dots - \int_{h_{m-1}}^{h_m} \frac{dh}{1+q/K(h)} \quad (21)$$

where $h_1, h_2, \dots, h_m$ are the pressure heads corresponding to the boundaries between the neighbouring layers, $z_1, z_2, \dots, z_m$. The values of h_1, h_2 , etc. are initially not known but must be determined during the integration procedure. Thus starting from zero-values of z and h at the water table, h is steadily decreased until z reaches z_i , the known height of the i -th boundary: the value h_i is thus found, when $z=z_i$ and since the pressure head is continuous across the boundary, h_i is the lower limit of the $(i+1)$ -th term of integration. In this way the integration may proceed until the last value h_m is reached or capillary rise reaches the soil surface.

Discretizing the integration interval into y subintervals of equal size ('delta' h), eq. (21) becomes :

$$z = \frac{y}{\Delta h} \left[1 + \frac{q}{K(h_{av})} \right] \quad (22)$$

y
 Δh
 $i=1$

where h_i and h_{i+1} are lower and upper boundary of the i th interval and

$$h_{av} = (h_i + h_{i+1})/2.$$

In case of infiltration, eq. (22) may cause problems because of the possibility that the term $q/K(h)$ may be smaller than -1, thus yielding a decreasing z , which is physically impossible. Therefore we use for infiltration a different approximation.

Rearranging eq. (19) to:

$$dh = - (1 + q/k(h)) dz \quad (23)$$

or

$$h_2 = h_1 - (z_2 - z_1) (1 + q/k(h')) \quad (24)$$

$$\text{where } h' = (h_1 + h_2)/2$$

This means that, starting from the groundwater level, where $z=0$ and $h=0$, the pressure head at some height z_2 may be found according to eq. (24).

As this value is not known at the time of calculation, an iterative procedure is used in CAPSEV.

3. ALTERNATIVE FUNCTIONS TO DESCRIBE THE $K(h)$ RELATIONSHIP

Besides the $K(h)$ relationship given by BLOEMEN (1980a) other expressions may be used, which are described below.

3.1 The first alternative is the description according to Brooks and Corey as given in eqs. 1 and 2.

3.2 The second alternative used in CAPSEV is the approach of RYTEMA(1965):

$$K = K_s \quad \text{for} \quad h \geq h_a \quad (25)$$

$$K = K_s \cdot e^{-b(h-h_a)} \quad \text{for} \quad h_{lim} \leq h < h_a \quad (26)$$

$$K = a \cdot (-h)^{-n} \quad \text{for} \quad h < h_{lim} \quad (27)$$

where

K_s = saturated hydraulic conductivity [cm.day]⁻¹
 h_a = pressure head at air entry point [cm]
 h_{lim} = some arbitrary pressure head limiting the validity of the conductivity function [cm]

a, b, n = constants

An example of this approach is given in fig. 3.

3.3 The third alternative has been described by WESSELING (1981) who approached the $K(h)$ relationship by three straight line pieces on a log-log scale. Each line piece is described by the following equation:

$$K = a \cdot (-h)^b \quad (28)$$

where a and b are constants.
 For an illustration see Fig. 4.

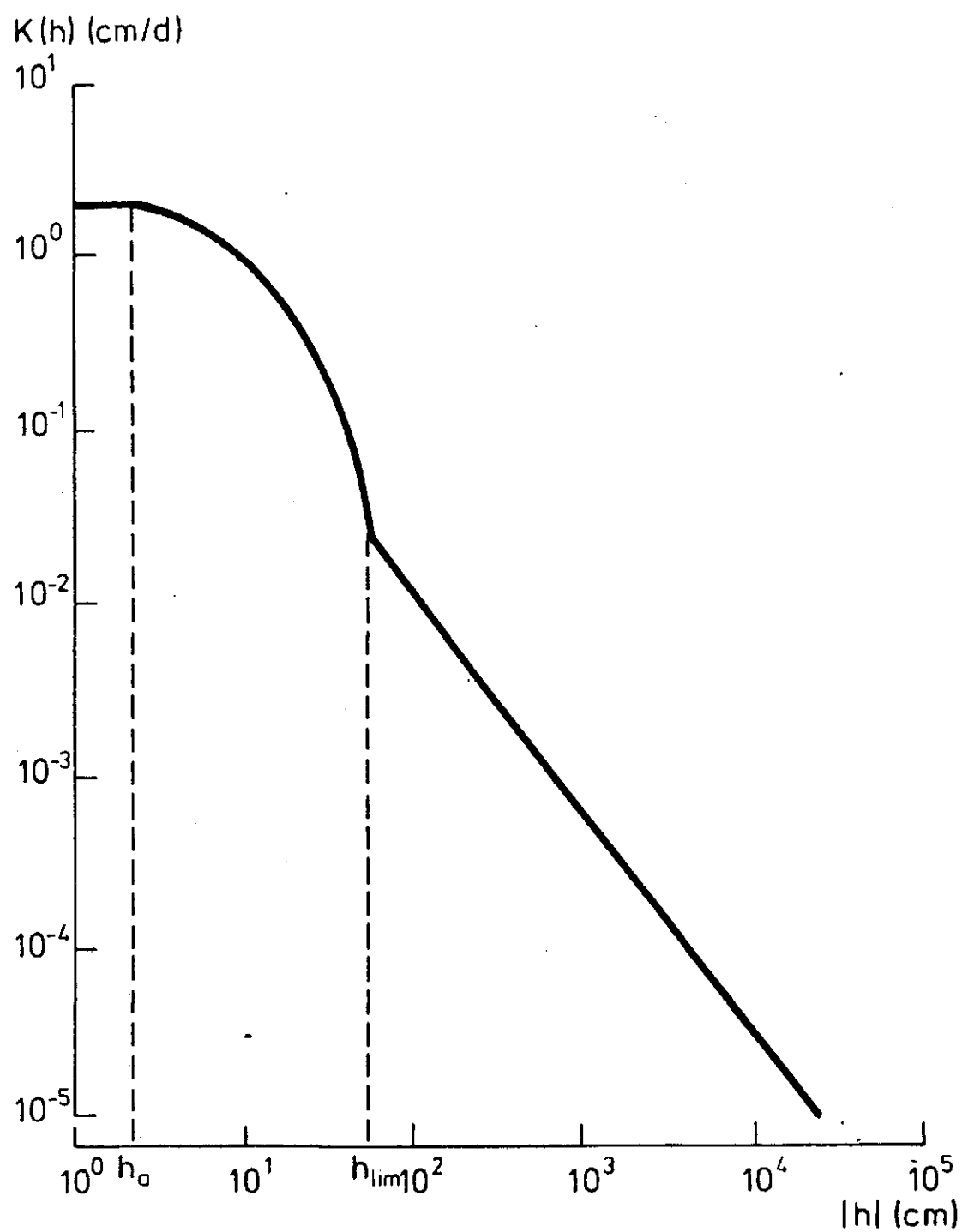


Fig. 3. $K(h)$ description according to Rytens(1965).

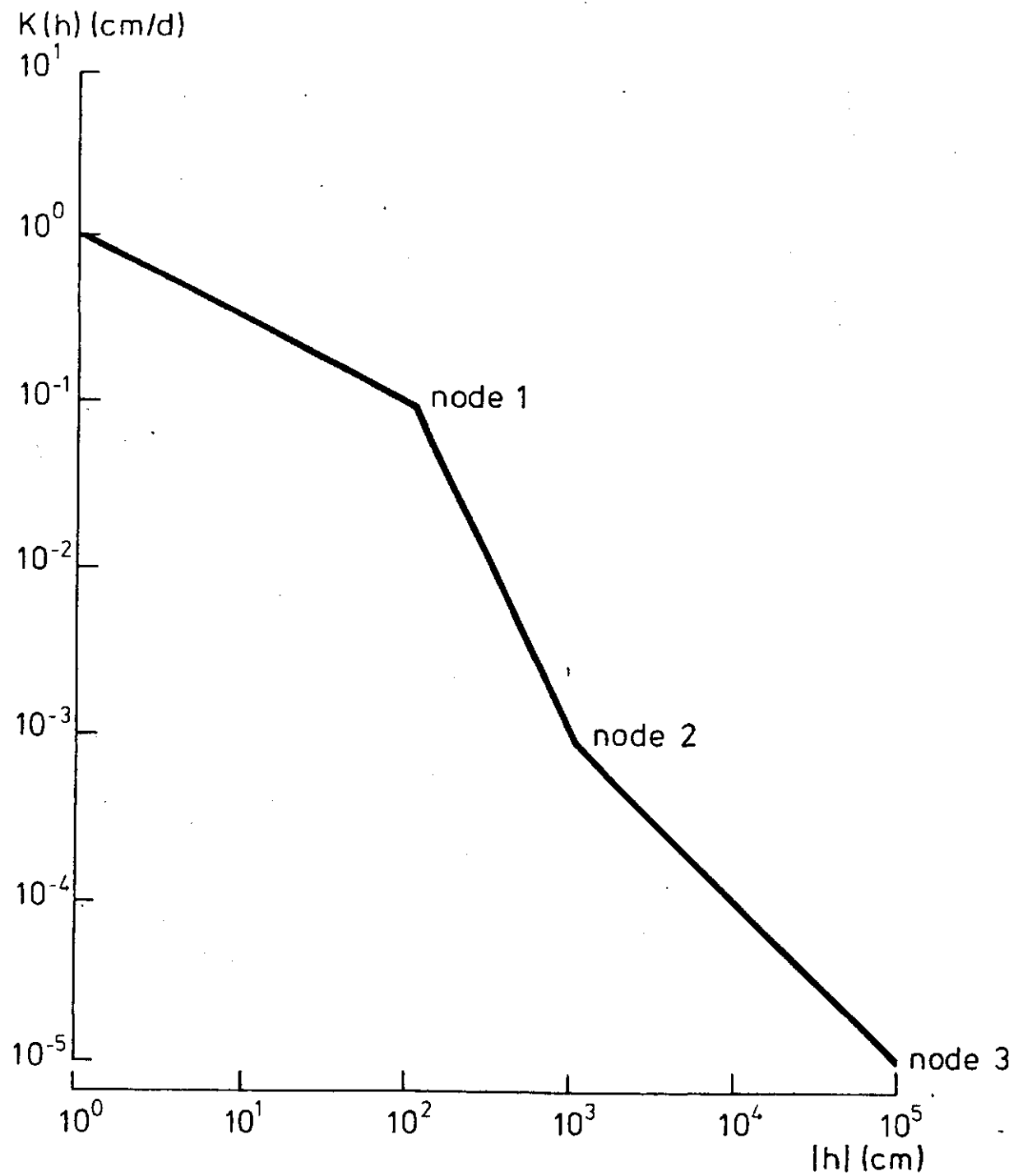


Fig. 4. Approximation of the $K(h)$ relationship by three power functions.

- 3.4 The last alternative is the description of K as a table of h. This alternative can easily be used to enter measured K(h) data. The step size of the table can be chosen freely. The program "CAPSEV" asks for the type of interpolation for values in between the prescribed values. This can be either linear or (double) logarithmic. The K-data in the table should be in ascending order. An example of such a table is given in Table 2.

Table 2. Example of a K(h) relation given as a table (Pucniew sand; after BRANDYK(1981)). h is given as an absolute value.

K (cm/d)	h (cm)	*	K (cm/d)	h (cm)	*	K (cm/d)	h (cm)
0.1706E-11	0.1000E+07	*	0.4187E-01	0.7900E+02	*	0.2794E+01	0.3100E+02
0.3700E-09	0.1000E+06	*	0.7456E-01	0.7300E+02	*	0.3549E+01	0.2700E+02
0.2558E-07	0.1500E+05	*	0.1223E+00	0.6800E+02	*	0.4519E+01	0.2200E+02
0.2461E-06	0.7000E+04	*	0.1892E+00	0.6300E+02	*	0.5830E+01	0.1700E+02
0.1753E-05	0.3000E+04	*	0.2799E+00	0.5900E+02	*	0.7923E+01	0.1000E+02
0.1834E-04	0.9000E+03	*	0.3999E+00	0.5500E+02	*	0.1135E+02	0.9000E+01
0.8563E-04	0.6500E+03	*	0.5557E+00	0.5100E+02	*	0.1654E+02	0.8000E+01
0.2867E-03	0.4200E+03	*	0.7551E+00	0.4800E+02	*	0.2412E+02	0.7000E+01
0.8659E-03	0.2600E+03	*	0.1006E+01	0.4500E+02	*	0.3572E+02	0.5000E+01
0.2894E-02	0.1300E+03	*	0.1320E+01	0.4200E+02	*	0.6019E+02	0.2500E+01
0.8715E-02	0.9400E+02	*	0.1709E+01	0.3800E+02	*	0.1589E+03	0.0010E+00
0.2089E-01	0.8600E+02	*	0.2193E+01	0.3500E+02	*		

4. THE PROGRAM

CAPSEV is able to calculate the pressure head distribution (h,z) for both capillary rise and infiltration in a layered soil profile (max. 10 layers). Pressure head distributions can be calculated for several flux densities q and various groundwater levels (max. 10). It is also possible to calculate maximally possible capillary fluxes for a number of groundwater levels. The output of the program is directed to a file called MOIST.OUT, which may be sent to a line printer.

The program CAPSEV consists of the following parts:

- main program
CAPSEV
- subroutine to show possible commands
HELP
- subroutines to read soil characteristics
GRNINP
LININP
BRCINP
TABINP
RYTINP
- subroutines to compute variables from grain size distribution
GRAIN
CALCUL
COMPHO
- subroutines used in calculations of pressure head distribution
CAPTOT
MAXFLX
INTEGR
CAPQUE
FLXQUE
CAPRIS
CAPINF
CONDOC
- subroutines for output
TABINF
TABEL

Now a short description of all the program parts is given.

CAPSEV : The main program welcomes the user and reads the commands (variable COMAND), after which it calls the appropriate subroutines.

HELP: Consists of only 1 write statement, resulting in a list of possible commands on the users terminal.

GRNINP: Performs the data input that is required to calculate the parameters of the hydraulic conductivity function from grain size distribution. There are 2 possible ways of input:

- a) From a terminal. In this way the program will ask the user to type in the data it requires.
- b) From a disk file with data prepared according to the questions that would be asked if method a) was chosen.

Which way of input will be chosen depends on the answers to questions that will be asked.

For the grain size classes:

-the value of the grain sizes between which the distribution must be known, may be typed in or

-the following standard set may be chosen:

2, 16, 50, 75, 105, 150, 210, 300, and 2000 μ .

Maximally 15 grain size classes may be entered.

GRAIN: Used to call the subroutines performing calculations on the soil texture data.

CALCUL: Computes the parameters of the conductivity function according to eqs. 3 to 18.

COMPHO: Assigns values to r and h .

0

CAPTOT: Controls the calculations of pressure head distribution. It reads the required depths of groundwater level from either terminal or file, and checks if the flux densities are positive or negative. A choice has to be made between two alternative ways to prepare the output :

- (1) For each groundwater level tables and printplots are prepared ; height of capillary rise versus height above the groundwater level in case of capillary rise, and pressure heads versus height above the groundwater level in case of infiltration.
- (2) A table is prepared of maximum capillary flux densities versus depth of the groundwater level for a specified pressure head, a printplot is optional.

MAXFLX: Performs calculations to find the maximally possible flux and creates an output table and (optionally) a printplot.

INTEGR: Function INTEGR performs the numerical integration and checks if a certain flux reaches a given level (e.g. the surface).

CAPQUE: Inquires which conductivity description function should be used. The answer is read into the variable METHOD, which may have one of the following values:

- 1 : Modified Brooks and Corey (eqs.1,2)
- 2 : Bloemen (eqs.3,4)
- 3 : Rijtema (eqs.25,26,27)
- 4 : Wesseling (eq. 28)
- 5 : Table

FLXQUE: Reads the flux densities for which the calculations should be

performed. It is possible to use one or both of the following 'standard' sets of flux densities:

- a) for infiltration: -0.5, -0.3, -0.2, -0.1, -0.05, 0.0,
- b) for capillary rise: 0.0, 0.05, 0.1, 0.2, 0.3 and 0.5 cm/day.

It is also possible to use values read from terminal or data file. A negative flux represents infiltration, a positive flux represents capillary rise. Please keep either a descending or ascending order.

BRCINP: Takes care of the input from terminal or file necessary for the modified Brooks and Corey method.

RYTINP: Reads data required for the $K(h)$ relationship according to Rytema from terminal or file.

LININP: Reads data required for the $K(h)$ relationship according to Wesseling. The K - and h -value of the end points of each line piece are either read from the terminal or from a data file.

TABINP: Reads the data when the $K(h)$ relationship is given as a table. Input is only possible as a file (see example 2).

CAPRIS: Calculates the height of capillary rise z according to eq. (22). The results are stored in the array Z for a range of pressure heads inbetween -1 and -1000000 cm. These pressure heads are divided into the following intervals:

for range		h-interval
1		
-1	to -10	-1
2		
-10	to -10	-10
3		
-10	to -10	-10
4		
-10	to -10	-10
5		
-10	to -10	-10
6		
-10	to -10	-10
Total: 55 h-values		

Calculations continue until either the lowest value of h is reached or z reaches the soil surface.

CAPINF: Calculates according to eq. (24) the pressure head distribution in the profile in case of infiltration. In some cases the pressure head may become positive. Then all the pressure heads for the corresponding flux density are set equal to 0. A warning is sent to the users terminal that the flux density as specified is for the soil under consideration physically impossible.

CONDUC: Function CONDUC calculates the unsaturated conductivity.

TABEL: Creates for positive flux densities (upward flow from the groundwater table) a table and printplot of height of capillary rise z as a function of pressure head h .

TABINF: Creates for negative flux densities (downward flow towards the groundwater table) a table and a printplot of pressure head h as a function of z .

The mutual relationship between the sub-programs mentioned is given in Fig. 5.

REMARK : As the calculation of the capillary fluxes is based on the
===== assumption of a steady state situation, it is unrealistic to assume that these fluxes do occur in reality. To calculate the pattern of the fluxes that occur in practice during the growing season, it is necessary to know the sequence of the different pressure heads. The fluxes that occur in reality can therefore differ considerably from those calculated by CAPSEV. The results from CAPSEV however, may be used to describe the hydrological properties of a profile, and to compare different profiles.

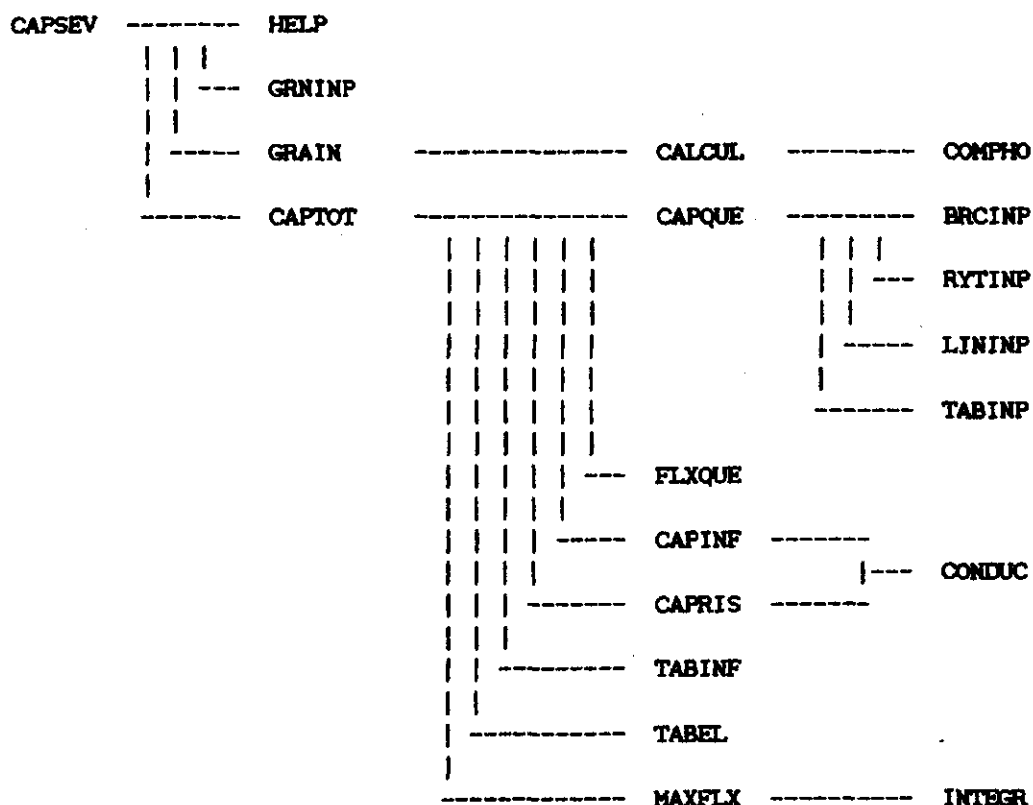


Fig. 5. Relation between the subprograms of CAPSEV.

5. Examples

5.1. Example of input.

CAPSEV is an interactive program with the possibility of reading data from files. As the interactive part of the program is self-explaining, only some examples will be given to show how to create the data files. In the examples a note of exclamation "!" is used to separate the data from some comments that were inserted.

As FORTRAN-77 has the ability of working with wildcards instead of FORMAT-statements, it is not necessary to prepare the input data according to a specific format.

The first example shows a data file that contains the answers to the questions CAPSEV asks when one calculates the parameters of the K(h)-relationship from soil texture and organic matter content.

Example 1. Input prepared for the computation of the K(h) relationship from soil texture and humus content ('Bloemen') of a 5 layer profile.

```
Marine clay      ! Name of soil profile
N               ! Non-standard grain sizes
2.             ! First boundary of grain size classes (mu)
16.            ! Second boundary etc.
50.
75.
105.
150.
210.
X              ! End of boundaries. Note: max. 15 classes
5              ! Number of layers in profile
Sandy clay      ! Description of top layer
15.            ! Thickness of top layer (cm)
5.4            ! Humus content of top layer (%), for peat: type P
19.2           ! Percentage of first grain size class
11.3           ! Percentage of second class etc.
43.8
12.6
9.4
2.6
1.2
N              ! No horizontal cracking in this layer
Heavy clay      ! Second layer
35.
3.7
50.
23.9
21.5
2.3
1.3
0.5
0.5
Y              ! Horizontal cracking does occur in this layer
Peat            ! Third layer
25.            ! Thickness of layer (cm)
P              ! P for peat
1              ! 1 for fen peat (2 for high bog peat)
0.24           ! Bulk density of peat (g/cm**3)
N              ! No horizontal cracking
Clayey sand     ! Fourth layer
75.
0.8
6.6
```

```

2.7
13.9
38.1
34.9
3.7
0.1
N
Sand                      ! Fifth layer
150.
0.6
3.3
2.6
11.9
19.8
27.7
27.4
6.7
N

```

The second example shows an input file for a 1-layer (homogeneous) profile when the K(h) relation has been given as a table. To save on typing, the h-values are given as positive numbers. The program will make them negative. Note: the sequence of K-values must be ascending, the sequence of h-values must correspond !!

Example 2. The K(h) relationship, given as a table. Input is only possible as a file. When the profile consists of more than one layer, add the data pertaining to these layers to the file. Start with the description of the layer.

```

Pucniew uniform sand      ! Name of soil profile
Sand                      ! Description of layer 1
200.                      ! Thickness of layer 1 (cm)
35                         ! Number of points in K(h)-table
.1000E+07 .1000E+06 .1500E+05 .7000E+04 .3000E+04 .9000E+03 .6500E+03 .4200E+03
.2600E+03 .1300E+03 .9400E+02 .8600E+02 .7900E+02 .7300E+02 .6800E+02 .6300E+02
.5900E+02 .5500E+02 .5100E+02 .4800E+02 .4500E+02 .4200E+02 .3800E+02 .3500E+02
.3100E+02 .2700E+02 .2200E+02 .1700E+02 .1000E+02 .9000E+01 .8000E+01 .7000E+01
.5000E+01 .2500E+01 .0010E+00      ! (Absolute) values of h (cm)
.1796E-11 .3700E-09 .2559E-07 .2461E-06 .1753E-05 .1834E-04 .8563E-03 .2867E-03
.8659E-03 .2894E-02 .8715E-02 .2089E-01 .4187E-01 .7456E-01 .1223E+00 .1892E+00
.2799E+00 .3999E+00 .5557E+00 .7551E+00 .1006E+01 .1320E+01 .1709E+01 .2193E+01
.2794E+01 .3549E+01 .4519E+01 .5830E+01 .7923E+01 .1135E+02 .1654E+02 .2412E+02
.3572E+02 .6019E+02 .1589E+03      ! Values of K (cm/day)

```

The third example is an input data-file, prepared for the RIJTEMA method.

Example 3. Input file using the K(h) relation according to RIJTEMA (eqs. 25-27)

Sandy loam	! Name of soil profile
Sandy loam	! Description of layer 1
3.52	! Parameter Ks (cm/day)
-42.4	! " " Ha (cm)
0.271	! " " b
-63.0	! " " Hlim (cm)
1.39	! " " a
1.12	! " " n
200.	! Thickness of the layer (cm)

The next example shows a file containing the data required for a 4-layered peaty-mucky soil profile. The K(h)-relation is described with 3 straight line pieces.

Example 4. The K(h) relationships of the four layers described according to WESSELING (1981). See eq. (28).

Peaty mucky soil	! Name of the profile
Muck	! Description of layer 1
91.5	! Saturated cond. (Ks, cm/d) of layer 1
.530E+02 .3092E+00	! Values of K (cm/d) and h (cm) at 1st node
.910E+03 .1266E-02	! Values of K and h at second node
.800E+07 .9748E-14	! Values of K and h at third node
20.	! Thickness of layer 1 (cm)
Peat	! Description of layer 2
37.5	! Ks etc.
.120E+03 .5932E-01	
.126E+04 .514E-03	
.800E+07 .5045E-14	
20.	
Peat-sand	! Layer 3
264.	
.11E+03 .6811E+00	

.100E+04 .1076E-02
 .220E+07 .7433E-12
 10.
 Sand
 491.
 .73E+02 .1758E+01
 .560E+03 .3888E-03
 .175E+06 .1921E-09
 151.

! Layer 4

The final example describes a profile consisting of 2 different layers. The K(h) relation is described according to Brooks and Corey.

Example 5. Input file when the K(h) relation is described according to Brooks and Corey (eqs. 1 and 2).

Imaginary soil profile	! Description of soil profile
Cover sand	! Description of layer 1
100.	! Thickness of layer 1 (cm)
93.5	! Effective conductivity (cm/day)
-7.	! Effective air entry value (cm)
3.31	! Slope
N	! No horizontal cracking
River clay	! Description of layer 2
150.	
9.0	
-17.	
1.26	
Y	

When the standard set of flux densities is not sufficient, or when some flux densities are not of interest it is possible to assign flux density values different from the standard set. These flux densities may be either read from the terminal or from a file.

Example 6. A data file containing flux densities (cm/d) different from the standard set. Either a descending or ascending order should be kept !

-.1
-.05
-.01
.0
.01
.05
.075
.1

Before starting the infiltration/capillary rise calculations, it is necessary to specify the depths of the groundwater table for which the computations have to be performed. One way is reading these depths from the terminal. If the groundwater levels are to be used for more profiles, it is advisable to make a data file and to read the depths from this file.

Example 7. Data file with groundwater levels (cm below soil surface) for which the infiltration/capillary rise calculations have to be performed. Use an ascending order !!

70.0
100.0
110.0
140.0
170.0

5.2 Examples of output.

In the first example of output the data of example 1 have been used. Both standard sets of flux densities have been applied, and a groundwater depth of 200 cm below the soil surface was taken. For

the profile under consideration the infiltration flux densities of -0.5 cm/day and -0.3 cm/day are physically impossible. Therefore the column representing the results of calculations with this flux density is filled with zeroes. The results are also shown in printplots.

The second example shows a table of maximally possible fluxes that reach the calculation level at several groundwater levels, and at a given pressure head. This is also shown in a printplot.

 * OUTPUT EXAMPLE 1 *

Marine clay

 DESCRPT. * THICK. HUM. MED. * S - VALUES IN MICRONS *****
 * (CM) % * 2. 16. 50. 75. 105. 150. 210. *****
 Sandy clay * 15.0 5.4 31.1 * 19.2 11.3 43.8 12.6 9.4 2.6 1.2 *****
 Heavy clay * 35.0 3.7 2.0 * 50.0 23.9 21.5 2.3 1.3 0.5 0.5 *****
 Peat * 25.0 * FEN PEAT, BULK DENSITY= 0.24 G. CM**-3 *****
 Clayey sand * 75.0 0.8 67.6 * 6.6 2.7 13.9 38.1 34.9 3.7 0.1 *****
 Sand * 150.0 0.6 88.4 * 3.3 2.6 11.9 19.8 27.7 27.4 6.7 *****

 LAYER Thick F N Ns ha ho Ksat r Ke ha/r Cracks *****
 Sandy clay 15. 0.55 2.01 1.74 -67.22 -1000000. 23.64 2.90 11.82 -23.18 N
 Heavy clay 35. 0.19 1.64 1.36 -403.70 -1000000. 0.26 2.90 0.13 -139.21 Y
 Peat 25. - 1.96 1.47 -84.13 -100000. 0.47 3.10 0.23 -27.14 N
 Clayey sand 75. 1.61 4.36 3.09 -74.21 -50000. 47.90 4.50 23.95 -16.49 N
 Sand 150. 1.27 3.76 2.83 -47.76 -100000. 95.48 4.50 47.74 -10.61 N

PRESSURE HEADS IN CASE OF INFILTRATION.

GROUNDWATER LEVEL = 200.0 CM.

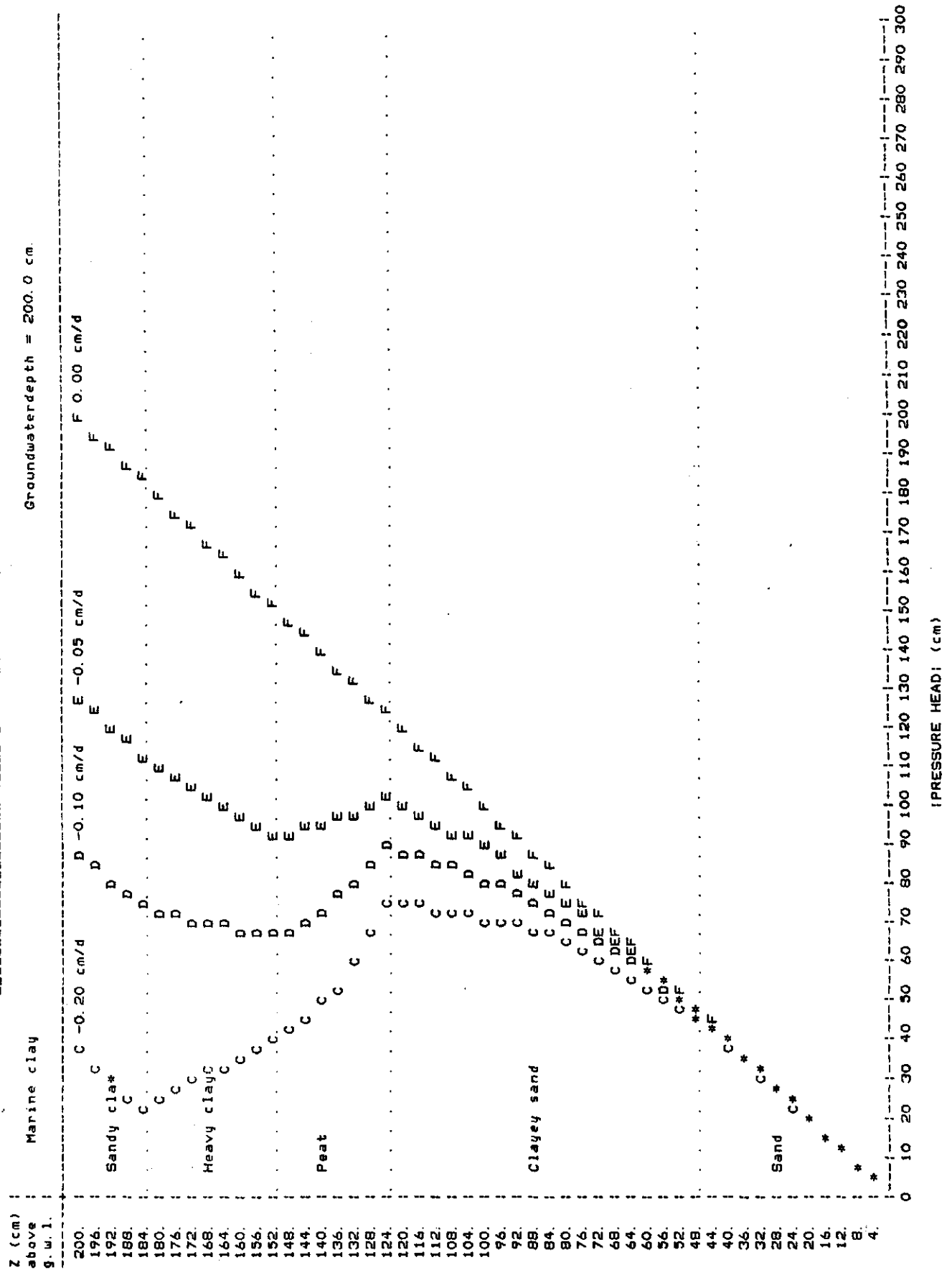
Marine clay

FLUX DENSITIES (CM/DAY)

Z * -0.500 -0.300 -0.200 -0.100 -0.050 0.000

CM.	*	-0.500	-0.300	-0.200	-0.100	-0.050	0.000
4.	*	0.0	0.0	-4.0	-4.0	-4.0	-4.0
8.	*	0.0	0.0	-8.0	-8.0	-8.0	-8.0
12.	*	0.0	0.0	-11.9	-12.0	-12.0	-12.0
16.	*	0.0	0.0	-15.9	-16.0	-16.0	-16.0
20.	*	0.0	0.0	-19.8	-19.9	-20.0	-20.0
24.	*	0.0	0.0	-23.7	-23.9	-24.0	-24.0
28.	*	0.0	0.0	-27.5	-27.8	-27.9	-28.0
32.	*	0.0	0.0	-31.2	-31.6	-31.8	-32.0
36.	*	0.0	0.0	-34.8	-35.4	-35.7	-36.0
40.	*	0.0	0.0	-38.2	-39.1	-39.5	-40.0
44.	*	0.0	0.0	-41.5	-42.7	-43.3	-44.0
48.	*	0.0	0.0	-44.7	-46.2	-47.1	-48.0
52.	*	0.0	0.0	-47.7	-49.7	-50.8	-52.0
56.	*	0.0	0.0	-50.7	-53.1	-54.5	-56.0
60.	*	0.0	0.0	-53.6	-56.5	-58.1	-60.0
64.	*	0.0	0.0	-56.2	-59.6	-61.7	-64.0
68.	*	0.0	0.0	-58.6	-62.7	-65.1	-68.0
72.	*	0.0	0.0	-60.8	-65.6	-68.5	-72.0
76.	*	0.0	0.0	-62.8	-68.3	-71.8	-76.0
80.	*	0.0	0.0	-64.6	-70.9	-74.9	-80.0
84.	*	0.0	0.0	-66.3	-73.3	-78.0	-84.0
88.	*	0.0	0.0	-67.7	-75.5	-80.9	-88.0
92.	*	0.0	0.0	-69.0	-77.6	-83.7	-92.0
96.	*	0.0	0.0	-70.1	-79.5	-86.4	-96.0
100.	*	0.0	0.0	-71.1	-81.2	-88.9	-100.0
104.	*	0.0	0.0	-72.0	-82.9	-91.3	-104.0
108.	*	0.0	0.0	-72.8	-84.3	-93.6	-108.0
112.	*	0.0	0.0	-73.4	-85.7	-95.7	-112.0
116.	*	0.0	0.0	-74.0	-86.9	-97.7	-116.0
120.	*	0.0	0.0	-74.5	-88.0	-99.6	-120.0
124.	*	0.0	0.0	-74.9	-88.9	-101.4	-124.0
128.	*	0.0	0.0	-75.4	-89.1	-100.4	-128.0
132.	*	0.0	0.0	-75.6	-89.3	-98.7	-132.0
136.	*	0.0	0.0	-75.6	-89.3	-97.1	-136.0
140.	*	0.0	0.0	-75.6	-89.3	-95.6	-140.0
144.	*	0.0	0.0	-75.2	-89.7	-94.3	-144.0
148.	*	0.0	0.0	-74.4	-89.4	-93.0	-148.0
152.	*	0.0	0.0	-73.9	-89.3	-91.7	-152.0
156.	*	0.0	0.0	-73.6	-89.2	-90.6	-156.0
160.	*	0.0	0.0	-73.6	-89.2	-90.6	-160.0
164.	*	0.0	0.0	-73.6	-89.2	-90.6	-164.0
168.	*	0.0	0.0	-73.6	-89.2	-90.6	-168.0
172.	*	0.0	0.0	-73.6	-89.2	-90.6	-172.0
176.	*	0.0	0.0	-73.6	-89.2	-90.6	-176.0
180.	*	0.0	0.0	-73.6	-89.2	-90.6	-180.0
184.	*	0.0	0.0	-73.6	-89.2	-90.6	-184.0
188.	*	0.0	0.0	-73.6	-89.2	-90.6	-188.0
192.	*	0.0	0.0	-73.6	-89.2	-90.6	-192.0
196.	*	0.0	0.0	-73.6	-89.2	-90.6	-196.0
200.	*	0.0	0.0	-73.6	-89.2	-90.6	-200.0

===== PRESSUREHEAD PROFILES IN CASE OF INFILTRATION =====



HEIGHT OF CAPILLARY RISE.

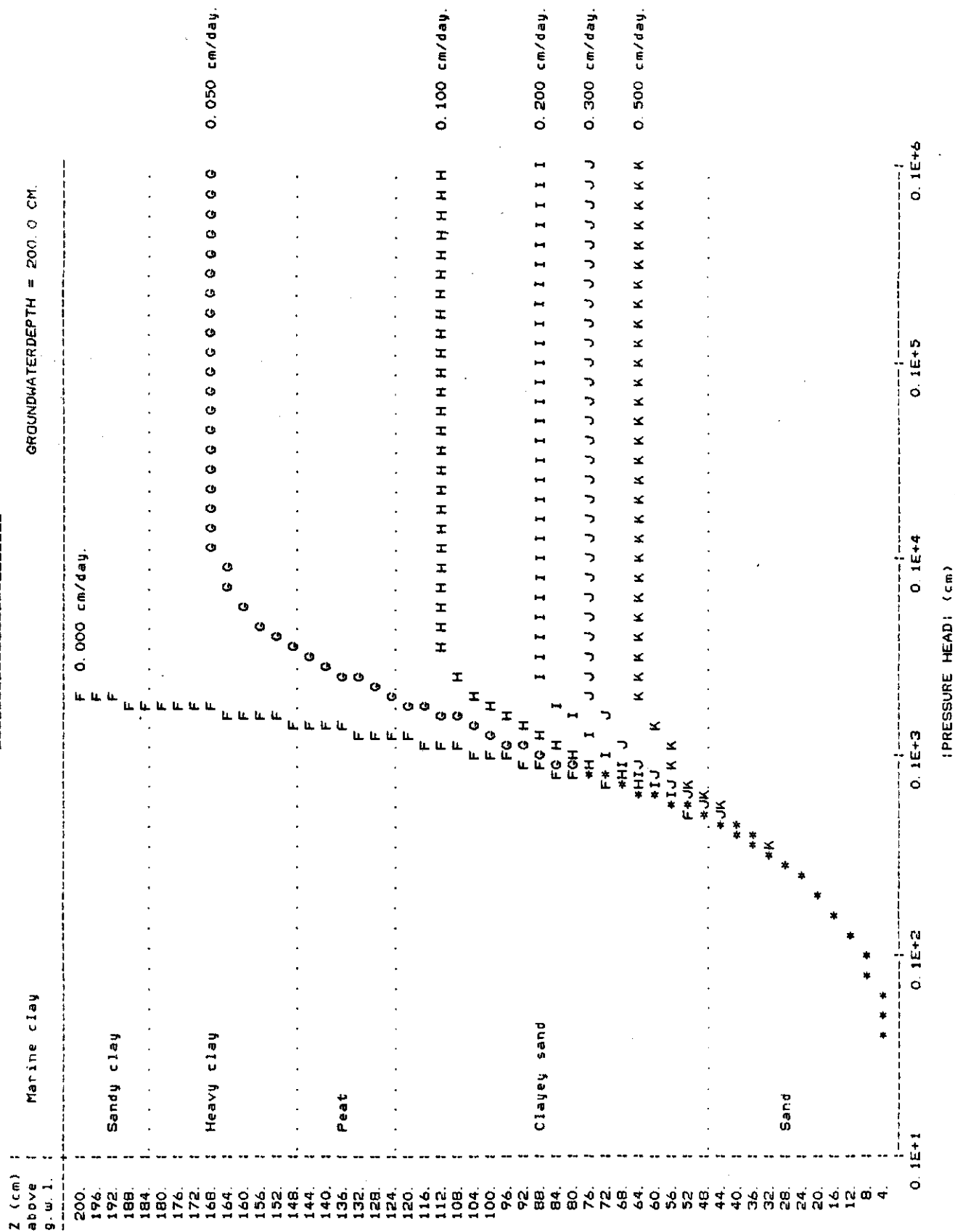
Marine clay

PR. HEAD * FLUX DENSITIES (CM/DAY)

CM.	*	0.000	0.050	0.100	0.200	0.300	0.500
-1.	*	1.0	1.0	1.0	1.0	1.0	1.0
-2.	*	2.0	2.0	2.0	2.0	2.0	2.0
-3.	*	3.0	3.0	3.0	3.0	3.0	3.0
-4.	*	4.0	4.0	4.0	4.0	4.0	4.0
-5.	*	5.0	5.0	5.0	5.0	5.0	5.0
-6.	*	6.0	6.0	6.0	6.0	6.0	6.0
-7.	*	7.0	7.0	7.0	7.0	7.0	7.0
-8.	*	8.0	8.0	8.0	8.0	8.0	8.0
-9.	*	9.0	9.0	9.0	9.0	8.9	8.9
-10.	*	10.0	10.0	10.0	10.0	9.9	9.9
-20.	*	20.0	20.0	19.9	19.8	19.8	19.6
-30.	*	30.0	29.8	29.7	29.4	29.1	28.5
-40.	*	40.0	39.5	39.1	38.3	37.5	36.2
-50.	*	50.0	48.9	48.0	46.3	44.8	42.3
-60.	*	60.0	58.1	56.4	53.4	50.9	47.1
-70.	*	70.0	66.8	64.2	59.7	56.2	50.8
-80.	*	80.0	75.0	71.0	65.0	60.5	53.9
-90.	*	90.0	82.5	77.0	69.3	63.8	56.2
-100.	*	100.0	89.3	82.2	72.8	66.4	57.9
-200.	*	200.0	129.8	105.4	86.3	76.0	64.0
-300.	*	0.0	141.4	110.8	89.1	77.9	65.1
-400.	*	0.0	151.7	112.8	90.1	78.6	65.5
-500.	*	0.0	158.5	113.6	90.5	78.9	65.7
-600.	*	0.0	162.3	114.1	90.8	79.0	65.8
-700.	*	0.0	164.6	114.4	90.9	79.1	65.9
-800.	*	0.0	166.1	114.6	91.0	79.2	65.9
-900.	*	0.0	167.1	114.7	91.1	79.2	65.9
-1000.	*	0.0	167.8	114.8	91.1	79.2	65.9
-2000.	*	0.0	170.1	115.0	91.2	79.3	66.0
-3000.	*	0.0	170.5	115.1	91.3	79.3	66.0
-4000.	*	0.0	170.6	115.1	91.3	79.3	66.0
-5000.	*	0.0	170.7	115.1	91.3	79.3	66.0
-6000.	*	0.0	170.7	115.1	91.3	79.4	66.0
-7000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-8000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-9000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-10000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-20000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-30000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-40000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-50000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-60000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-70000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-80000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-90000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-100000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-200000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-300000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-400000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-500000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-600000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-700000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-800000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-900000.	*	0.0	170.8	115.1	91.3	79.4	66.0
-1000000.	*	0.0	170.8	115.1	91.3	79.4	66.0

HEIGHT OF CAPILLARY RISE =====

GROUNDWATER DEPTH = 200.0 CM.



 * OUTPUT EXAMPLE 2 *

Testprofile 3

 DESCRIPT. * THICK. HUM. MED. * S - VALUES IN MICRONS
 * (CM) * 2. 16. 50. 75. 105. 150. 210. 300. 2000.

 (1) Sandy clay * 30.0 3.5 34.2 * 20.9 10.7 34.4 17.0 11.0 6.0 0.0 0.0 0.0
 (2) Light clay * 30.0 1.0 22.2 * 29.0 15.0 33.0 11.0 8.0 4.0 0.0 0.0 0.0
 (3) Peat * 25.0 FEN PEAT, BULK DENSITY= 0.18 g . CM**-3
 (4) Fine sand * 300.0 0.1 141.6 * 2.0 2.0 9.5 10.0 7.0 24.0 20.0 11.5 14.0

LAYER	Thick	F	N	Ns	ha	ho	Ksat	r	Ke	ha/r	Cracks
(1) Sandy clay	30.	0.49	1.99	1.73	-56.25	-1000000.	30.76	2.90	15.38	-19.40	N
(2) Light clay	30.	0.36	1.91	1.66	-65.94	-1000000.	16.97	2.90	8.48	-22.74	Y
(3) Peat	25.	-	2.11	1.56	-59.82	-5000.	1.42	3.10	0.71	-19.30	N
(4) Fine sand	300.	0.95	3.59	2.78	-24.14	-10000.	293.91	4.50	146.95	-5.36	N

MAXIMALLY POSSIBLE FLUXES (cm/day)

Testprofile 3

LEVEL OF CALCULATIONS= 0. CM. BELOW SURFACE

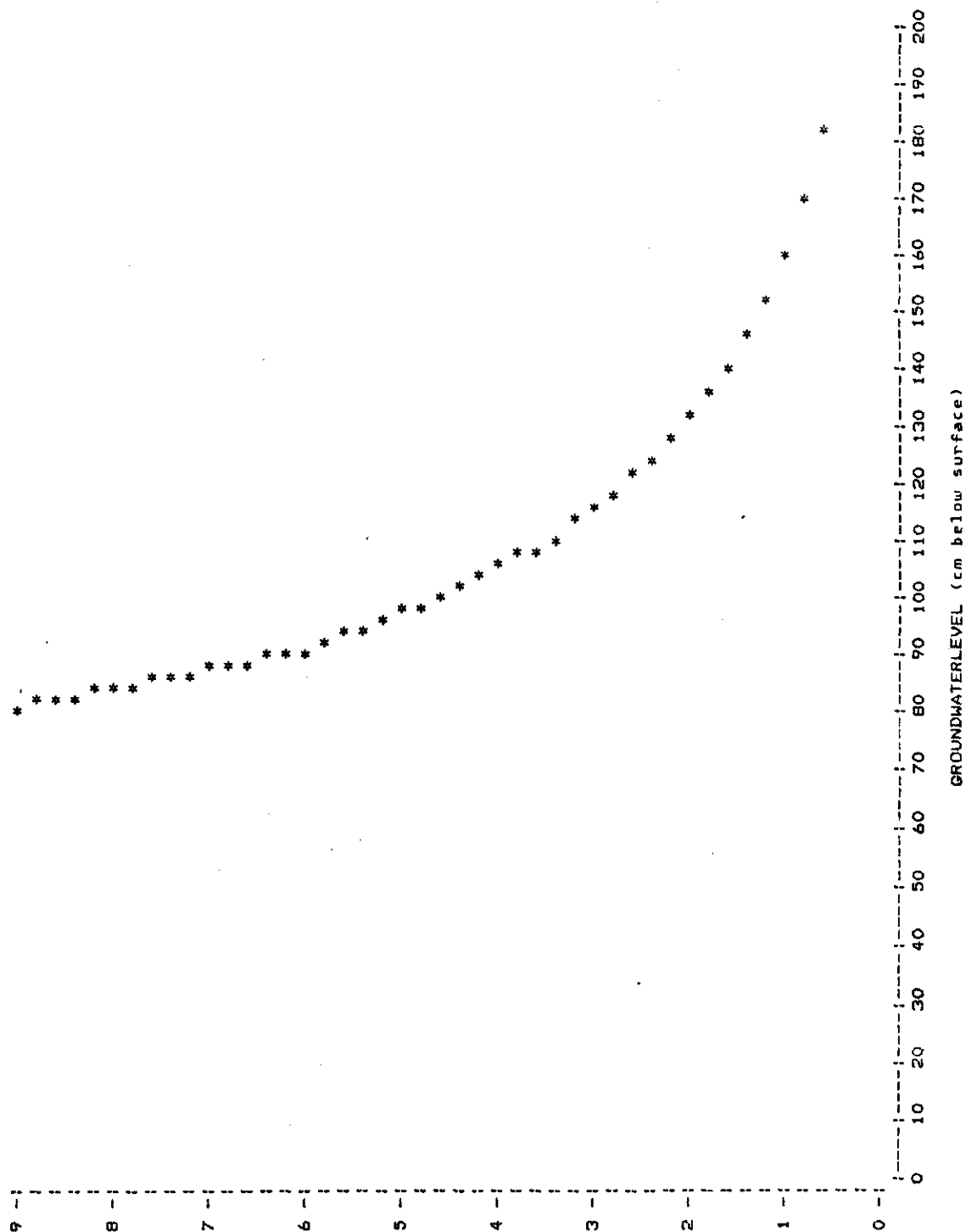
PR. HEAD (CM.)	* 60.	70.	80.	90.	100.	110.	120.	130.	140.	150.	160.	170.	180.	190.	200.
G R O U N D W A T E R L E V E L (CM. BELOW SURFACE)															
-1000.	* -1.000	-1.000	0.917	0.615	0.464	0.345	0.266	0.208	0.163	0.128	0.100	0.079	0.063	0.050	0.041

NOTE : The figure -1.000 indicates the occurrence of a flux > 1.0 cm/day !!

PRINTPLOT OF CAPILLARY RISE (mm/day) VERSUS GROUNDWATER DEPTH

Pressure head : -1000. cm.

Test profile 3



REFERENCES

- Aliverti-Piuri, E. and J.G.Wesseling. 1979. Calculation of height of capillary rise in non-homogeneous soil profiles. Nota ICW 1156, 46 pp.
- Bloemen, G.W. 1980a. Calculation of hydraulic conductivities from texture and organic matter content. Zeitschrift fuer Pflanzenernaehrung und Bodenkunde, 143. Band, Heft 5, Seite 581-605. (also TB 120, ICW)
- Bloemen, G.W. 1980b. Calculation of steady state capillary rise from the groundwater table in multi-layered soil profiles. Zeitschrift fuer Pflanzenernaehrung und Bodenkunde. 143. Band, Heft 6, Seite 701-719. (also TB 121, ICW)
- Bloemen, G.W., and J.B.H.M. van Gils, 1982. Guide to the program UNSLOW for the calculation of steady state infiltration and capillary rise. Nota ICW 1392, 31 pp.
- Brandyk, T., 1981. Zastosowanie modelu matematycznego do opisu uwilgotnienia gleby piaszczystej. Zesz. probl. Post. Nauk. vol. (in press).
- Rijtema, P.E., 1965. An analysis of actual evapotranspiration. Agric. Res. Rep. 659. PUDOC, Wageningen. 107 pp.
- Wesseling, J.G. 1981. Een computerprogramma voor het bepalen van de optimale ligging van drie lijnstukken door een serie getallenparen. Nota ICW 1313, 34 pp.

PROGRAM CAPSEV

```

=====
PROGRAM CAPSEV IS DEVELOPED TO CALCULATE:
=====
- HYDRAULIC CONDUCTIVITY FROM GRAIN SIZE DISTRIBUTION
  AND ORGANIC MATTER CONTENT
=====
- STEADY STATE CAPILLARY RISE ABOVE THE GROUNDWATER
  TABLE
=====
- STEADY STATE INFILTRATION TOWARDS THE WATER TABLE
=====
Program developed by
=====
Ir. J.G. Wesseling, Ing. G.W. Bloemen and
Ing. W.A.J.M. Kroonen,
INSTITUTE FOR LAND AND WATER MANAGEMENT,
P.O. Box 35,
6700 AA Wageningen.
The Netherlands
=====
REVISED VERSION.
NOVEMBER 1983.
=====

```

```

=====
INTEGER PEAT
LOGICAL CRACK
CHARACTER DESCR, HEAD, COMAND
REAL MEDIAN, KSAT, KSATEF
COMMON/TABDAT/TABPRH(10,80), TABCON(10,80), NUMTAB(10), INTERP
COMMON/SPONES/NFLNS, NFLNE, NFLPS, NFLPE
COMMON/RYTEMA/RYTEK(10), RYTEA(10), RYTE(10), RYTN(10),
* RYTHA(10), RYTHLM(10)
COMMON/LINE/SUCLIN(10,4), CONLIN(10,4), ALIN(10,3), BLIN(10,3)
COMMON/SOIL/THICK(10), THKLAY(10), GWL, DESCR(10,15)
COMMON/INFIL/SUCINF(15,51), ZINF(51), NZINF
COMMON/RISE/KSAT(10), PSTA(10), Z(15,54), H(54), FLUX(15),
* METHOD, NFLVKS, NLAYER, LAYER, HEAD(80)
COMMON/BLOEM/KSATEF(10), PSICOR(10), PSIEFF(10), PSIO(10),
* SLOPES(10), SLOPE(10), SLPOR(10), F(10), REDUC(10),
* DIFFER(10,15), SIZE(15), BULK(10), PEAT(10), HUMUS(10),
* MEDIAN(10), NSIZES, CRACK(10)
=====
OPEN OUTPUT FILE
OPEN(UNIT=10, FILE='MOIST. OUT', STATUS='NEW')
=====
WELCOME
WRITE(6,10:10)
1010 FORMAT(///, T30, ' Welcome to program CAPSEV. ',/,
* T30, ' =====', ///)
=====
CALL HELP
=====

```

```

=====
INPUT COMMAND
100 WRITE(6,10:50)
1050 FORMAT(//, ' Command? ', $)
1060 READ(5,1060) COMAND
1060 FORMAT(A1)
=====
C
IF(COMAND.NE.'C') GO TO 220
C CALCULATE CAPILLARY RISE
C CALL CAPTOT
C GO TO 100
=====
C
220 IF(COMAND.NE.'E') GO TO 240
C LEAVE PROGRAM
C WRITE(6,1100)
1100 * FORMAT(//, ' Your results are written to a file, named ',
' MOIST. OUT', //, T30, ' Bye. ', //, T30, ' ==', //)
C CLOSE(UNIT=10)
C CALL EXIT
=====
C
240 IF(COMAND.NE.'G') GO TO 260
C CALCULATION OF SOIL CHARACTERISTICS FROM GRAIN SIZE DISTRIBUTION
C CALL GRNINP
C CALL GRAIN
C GO TO 100
=====
C
260 IF(COMAND.NE.'H') GO TO 280
C LIST POSSIBLE COMMANDS
C CALL HELP
C GO TO 100
=====
C
280 UNKNOWN COMMAND
1200 WRITE(6,1200)
1200 FORMAT(//, ' ??? Illegal command ???')
C GO TO 100
=====
C
END
=====
C
SUBROUTINE HELP
=====
C
C = Subroutine HELP lists the commands that are allowed.
C =
=====
C
WRITE(6,1010)
1010 * FORMAT(//, ' The possible commands are: ',/,
* T10, ' C : ', T15, ' Compute height of capillary rise',/,
* T10, ' E : ', T15, ' Leave program',/,
* T10, ' G : ', T15, ' Compute soil characteristics from grain size',
* ' distribution',/,
* T10, ' H : ', T15, ' Show list of commands (this message)',/,
* //)
=====
C
RETURN
END
=====
C
C
=====

```



```

2100 READ(DEVICE,2100)(DESCR(LAYER,I),I=1,15)
      FORMAT(15A1)
2103 IF(DEVICE.EQ.5)WRITE(6,2103)
      FORMAT('What is thickness (cm) of this layer?',T50,'',$)
      READ(DEVICE,*)THKLAY(LAYER)
2110 IF(DEVICE.EQ.5)WRITE(6,2110)
      FORMAT('Type humuscontent (in %) or P for peat?',T50,'',$)
      READ(DEVICE,*,ERR=200)HUMUS(LAYER)
      IF(HUMUS(LAYER).LT.0.01)HUMUS(LAYER)=0.01

C -----
C 160 MINERAL SOIL
      PEAT(LAYER)=0
      TOTAL=0
2140 IF(DEVICE.EQ.5)WRITE(6,2140)
      FORMAT('Now the percentages between the grain ',
        'size classes will be asked. '//)
      DO 170 ISIZE=1,NSIZES
165 IF(DEVICE.EQ.5)WRITE(6,2150)SIZE(ISIZE)
2150 FORMAT('Percentage belonging to grain size class',FB.1,
        ' ',T50,'',$)
      READ(DEVICE,*,ERR=165)DIFFER(LAYER,ISIZE)
      TOTAL=TOTAL+DIFFER(LAYER,ISIZE)
      IF(TOTAL.LE.100.1001)GOTO 170
      WRITE(6,2155)
2155 FORMAT('The sum of the percentages exceeds 100% !',
        ' Try again. '//)
      GOTO 160
      CONTINUE

170 CALCULATION OF MEDIAN GRAIN SIZE
      SUBTOT=0
      DO 180 ISIZE=1,NSIZES
180 I=ISIZE
      SUBTOT=SUBTOT+DIFFER(LAYER,I)
      IF(SUBTOT.GE.50.0)GOTO 190
      CONTINUE
190 DIFF=50.0-SUBTOT
      MEDIAN(LAYER)=SIZE(I-1)+(DIFF/DIFFER(LAYER,I))*
        (SIZE(I)-SIZE(I-1))
      GOTO 250

C -----
C 200 PEAT SOIL
2160 IF(DEVICE.EQ.5)WRITE(6,2160)
      FORMAT('Type 1 for fen peat, 2 for high bog peat?',T50,'',$)
      READ(DEVICE,*)PEAT(LAYER)
      IF(PEAT(LAYER).NE.1.AND.PEAT(LAYER).NE.2)GOTO 200
2170 IF(DEVICE.EQ.5)WRITE(6,2170)
      FORMAT('What is bulk density of peat (g/cm3)?',T50,'',$)
      READ(DEVICE,*)BULK(LAYER)

C -----
C 250 CRACKING?
2180 IF(DEVICE.EQ.5)WRITE(6,2180)
      FORMAT('Does horizontal cracking occur? (Y/N)',$)
      READ(DEVICE,2190)ANSWER
2190 FORMAT(A1)
      IF(ANSWER.EQ.'Y')CRACK(LAYER)=.TRUE.

C -----
C 300 CONTINUE
      IF(DEVICE.EQ.21)CLOSE(UNIT=21)

      GO TO 950

*****
* SHOW INPUT DATA
*
*****
WRITE(10,5010)(HEAD(I),I=1,80)
FORMAT('','','BOA1,///)
WRITE(10,5020)
FORMAT(' ',132('*'))
WRITE(10,5030)(SIZE(I),I=1,NSIZES)
FORMAT(' DESCRIPT. ',T18,' * THICK. HUM. MED. ',T42,' *',T55,
  'S - VALUES IN MICRONS','',' ',T18,' * (CM)',T32,'%',
  T42,' *',3X,15F5.0)
WRITE(10,5020)
DO 930 LAYER=1,NLAYER
  IF(PEAT(LAYER).EQ.0)WRITE(10,5040)(DESCR(LAYER,I),I=1,15),
    THKLAY(LAYER),HUMUS(LAYER),MEDIAN(LAYER),
    (DIFFER(LAYER,ISIZE),ISIZE=1,NSIZES)
  IF(PEAT(LAYER).EQ.1)WRITE(10,5050)(DESCR(LAYER,I),I=1,15),
    THKLAY(LAYER),BULK(LAYER)
  IF(PEAT(LAYER).EQ.2)WRITE(10,5060)(DESCR(LAYER,I),I=1,15),
    THKLAY(LAYER),BULK(LAYER)
930 CONTINUE
5040 FORMAT(' ',15A1,T18,'*',FB.1,T28,F5.1,F7.1,T42,'*',3X,15F5.1)
5050 FORMAT(' ',15A1,T18,'*',FB.1,T35,' FEN PEAT, BULK DENSITY=',
  F7.2,' g . CM**-3')
5060 FORMAT(' ',15A1,T18,'*',FB.1,T35,
  ' HIGH BOG PEAT, BULK DENSITY=',F7.2,' g . CM**-3')
  WRITE(10,5020)
  RETURN
  END

*****
SUBROUTINE GRAIN
*****
SUBROUTINE TO SHOW THE RESULTS OF CALCULATING THE
HYDRAULIC CONDUCTIVITY FUNCTION FROM THE GRAIN SIZE
DISTRIBUTION

INTEGER PEAT
LOGICAL CRACK
CHARACTER DESCR,HEAD,CRS
REAL MEDIAN,KSAT,KSATEF,S(14)
COMMON/SOIL/THICK(10),THKLAY(10),GWL,DESCR(10,15)
COMMON/RISE/KSAT(10),PSIA(10),Z(15,54),H(54),FLUX(15),
  METHOD,NFLUXS,NLAYER,LAYER,HEAD(80)
COMMON/BLOEM/KSATEF(10),PSICOR(10),PSIEFF(10),PSIO(10),
  SLOPES(10),SLOPE(10),SLPCOR(10),F(10),REDUC(10),
  DIFFER(10,15),SIZE(15),BULK(10),PEAT(10),HUMUS(10),
  MEDIAN(10),NSIZES,CRACK(10)
  DATA S/-0.,-0.,-10.,-20.,-31.,-50.,-100.,-250.,-500.,

*****

```

```

      * -1000. -2500. -5000. -10000. -16000. /
C ----- CALCULATION OF CONDUCTIVITY PARAMETERS
C DO 10 LAYER=1,NLAYER
C CALL CALCU
C
C 10 CONTINUE
C
C ---- SHOW RESULTS
C WRITE(10,2010)
C 2010 FORMAT(///)
C 2020 WRITE(10,2020)
C 2020 FORMAT(' ',132('='))
C 2030 WRITE(10,2030)
C 2030 FORMAT(' LAYER',T19,'THICK',T13,'F',T44,'N',T54,'Ns',T65,
* 'ha',T75,'h0',T86,'Ksat',T99,'r',T108,'ke',T117,
* 'ha',T127,'Crack',T132('='))
C DO 100 LAYER=1,NLAYER
C
C IF(CRACK(LAYER)) CRS='V'
C IF(PEAT(LAYER).EQ.0)WRITE(10,2040) (DESCR(LAYER,I),I=1,15),
C THKLAY(LAYER),F(LAYER),SLOPE(LAYER),SLOPS(LAYER),
C PSIA(LAYER),PSIC(LAYER),KSAT(LAYER),REDUC(LAYER),
C KSAIEF(LAYER),PSIEFF(LAYER),CRS
C IF(PEAT(LAYER).NE.0)WRITE(10,2050) (DESCR(LAYER,I),I=1,15),
C THKLAY(LAYER),SLOPE(LAYER),SLOPS(LAYER),PSIA(LAYER),
C PSID(LAYER),KSAT(LAYER),REDUC(LAYER),KSAIEF(LAYER),
C PSIEFF(LAYER),CRS
C 100 CONTINUE
C 2040 FORMAT(' ',15A1,F7.0,4F11.2,F11.0,4F11.2,T129,A1)
C 2050 FORMAT(' ',15A1,F7.0,BX,'-',2X,3F11.2,F11.0,4F11.2,T129,A1)
C WRITE(10,2020)
C
C RETURN
C END
C
C *****
C SUBROUTINE CALCUL
C
C =====
C
C SUBROUTINE CALCUL CALCULATES THE CONSTANTS TO BE USED IN =
C THE HYDRAULIC CONDUCTIVITY FUNCTION. =
C =
C =====
C
C INTEGER PEAT
C LOGICAL CRACK
C CHARACTER DESCR,HEAD
C REAL MEDIAN,KSAT,PEATEF
C COMMON/SOIL/THICK(10),THKLAY(10),CAL,DESCR(10,15)
C COMMON/RISE/KSAT(10),PSIA(10),Z(15,54),H(54),FLUX(15),
C METHOD,NFLUX,NLAYER,LAYER,HEAD(80)
C COMMON/BLDEM/KSAIEF(10),PSICOR(10),PSIEFF(10),PSID(10),
C SLOPS(10),SLOPE(10),SLPCR(10),F(10),REDUC(10),
C DIPFER(10,15),SIZE(15),BULK(10),PEAT(10),HUMUS(10),
C MEDIAN(10),NSIZES,CRACK(10)
C
C ---- MINERAL OR PEAT?
C IF(PEAT(LAYER).NE.0)GO TO 200
C
C ----- MINERAL
C SUMF=0.0
C SUMPER=0.0
C PPLONE=DIPFER(LAYER,1)
C NST=NSIZES-1
C
C DO 100 I=1,NST
C I=I
C J=I+1
C P=PPLONE
C CALCULATE NEW P(I+1)
C PPLONE=PPLONE+DIPFER(LAYER,J)
C NEW SUM OF PERCENTAGES
C SUMPER=SUMPER+DIPFER(LAYER,J)
C CALCULATION OF F(I)
C ALOP=ALOG10(PPLONE/P)
C ALSZ=ALOG10(SIZE(J)/SIZE(I))
C FI=DIPFER(LAYER,J)*ALOP/ALSZ
C SUMF=SUMF+FI
C 100 CONTINUE
C
C CALCULATION OF F(LAYER)
C F(LAYER)=SUMF/SUMPER
C
C CALCULATION OF SLOPE OF HYDRAULIC CONDUCTIVITY CURVE
C SLOPE(LAYER)=1.4 + 4.536 * (EXP(0.3*F(LAYER))-1.0) -
C 0.75 * (F(LAYER)**1.6) * ALOG10(HUMUS(LAYER))
C
C CALCULATION OF AIR ENTRY VALUE PSIA
C PSIA(LAYER)=2914.0 * (MEDIAN(LAYER) ** (-0.96)) *
C (F(LAYER) ** (0.79))
C
C CALCULATION OF SATURATED CONDUCTIVITY KSAT
C KSAT(LAYER)=0.02 * (MEDIAN(LAYER) ** (1.93)) *
C (F(LAYER) ** (-0.74))
C
C CALCULATION OF PRESSURE HEAD, PSID, WHERE THE CONDUCTIVITY
C APPROACHES ZERO AND OF THE REDUCTION FACTOR r
C CALL COMPHO
C
C GO TO 900
C
C ---- PEAT
C IF(PEAT(LAYER).NE.1)GO TO 400
C 200 FEN PEAT
C
C CALCULATION OF SLOPE OF HYDRAULIC CONDUCTIVITY CURVE
C SLOPE(LAYER)=2.54 - 2.42 * BULK(LAYER)
C
C CALCULATION OF AIR ENTRY VALUE PSIA
C PSIA(LAYER)=-416.0 * (BULK(LAYER) ** 1.12)
C
C CALCULATION OF SATURATED CONDUCTIVITY KSAT
C KSAT(LAYER)=0.00266 * (BULK(LAYER) ** (-3.625))
C
C CALCULATION OF PSID AND REDUCTION FACTOR r
C CALL COMPHO
C
C GO TO 900
C
C ---- HIGH BOG PEAT

```

```

C -----
C 400 CALCULATION OF SLOPE OF HYDRAULIC CONDUCTIVITY CURVE
C SLOPE(LAYER)=2.57 - 2.27 * BULK(LAYER)
C -----
C CALCULATION OF AIR ENTRY VALUE PSIA
C PSIA(LAYER)=-794.0 * (BULK(LAYER) ** 1.17)
C -----
C CALCULATION OF SATURATED HYDRAULIC CONDUCTIVITY KSAT
C KSAT(LAYER)=0.0036 * (BULK(LAYER) ** (-2.83))
C -----
C CALCULATION OF PSIO AND REDUCTION FACTOR R
C CALL COMPHO
C -----
C CALCULATION OF EFFECTIVE CONDUCTIVITY AND PRESSURE HEAD
C KSATEF(LAYER)=0.5*KSAT(LAYER)
C PSIEFF(LAYER)=PSIA(LAYER)/REDUC(LAYER)
C -----
C CALCULATION OF NS
C SLOPES(LAYER)=(ALOG10(2.0*((PSIA(LAYER)/PSIO(LAYER))**
C * SLOPE(LAYER))))/(ALOG10(PSIEFF(LAYER)/PSIO(LAYER)))
C -----
C CORRECTIONS FOR HORIZONTAL CRACKING
C SLPCOR(LAYER)=SLOPES(LAYER)
C IF(CRACK(LAYER))SLPCOR(LAYER)=SLPCOR(LAYER)+1.7
C PSICOR(LAYER)=PSIEFF(LAYER)
C IF(CRACK(LAYER).AND.PSIEFF(LAYER).GT.-100.)PSICOR(LAYER)=
C -100.0*((-0.01*PSIEFF(LAYER))**(SLOPES(LAYER)/SLPCOR(LAYER)))
C RETURN
C -----
C END
C *****
C SUBROUTINE COMPHO
C =====
C SUBROUTINE TO COMPUTE PSIO(LAYER) AND REDUCTION FACTOR R
C FROM GRAIN SIZE DISTRIBUTION AND MEDIAN GRAIN SIZE
C =====
C
C INTEGER PEAT
C LOGICAL CRACK
C CHARACTER DESCR,HEAD
C REAL MEDIAN,KSAT,KSATEF
C DIMENSION HO(6),BLMA(5),BLM(5)
C COMMON/SOIL/THICK(10),THKLAY(10),GWL,DESCR(10,15)
C COMMON/RISE/KSAT(10),PSIA(10),Z(15,54),H(54),FLUX(15),
C * METHOD,NFLUXS,NLAYER,LAYER,HEAD(80)
C COMMON/BLOEM/KSATEF(10),PSICOR(10),PSIEFF(10),PSIO(10),
C * SLOPES(10),SLOPE(10),SLPCOR(10),F(10),REDUC(10),
C * DIFFER(10,15),SIZE(15),BULK(10),PEAT(10),HUMUS(10),
C * MEDIAN(10),NSIZES,CRACK(10)
C DATA HO/-1.E6,-1.E4,-5.E3,-1.E3,-5.E2,-2.E2/
C DATA BLMA/0.004,0.00286,0.0025,0.00225,0.00341/
C DATA BLM/1.2,1.6,2.1,2.5,3.5/
C -----
C MINERAL SOIL OR PEAT?
C IF(PEAT(LAYER).NE.0)GO TO 430
C -----
C MINERAL SOIL

```

```

C -----
C REDUCTION FACTOR r
C REDUC(LAYER)=2.9
C IF(MEDIAN(LAYER).GT.50.0)REDUC(LAYER)=4.5
C -----
C COMPUTATION OF PRESSURE HEAD HO WHERE CONDUCTIVITY APPROACHES 2
C DO 100 I=1,5
C   NVAL=I
C   SUM=F(LAYER)+BLMA(I)*MEDIAN(LAYER)
C   IF(SUM.LT.BLM(I))GO TO 200
C   CONTINUE
C   PSIO(LAYER)=HO(6)
C   GO TO 500
C 100 PSIO(LAYER)=HO(NVAL)
C   GO TO 500
C 200 PSIO(LAYER)=HO(NVAL)
C   GO TO 500
C -----
C PEAT
C =====
C 400 IF(PEAT(LAYER).EQ.2)GO TO 420
C -----
C FEN PEAT
C REDUC(LAYER)=3.1
C GO TO 450
C -----
C HIGH BOG PEAT
C REDUC(LAYER)=1.9
C IF(BULK(LAYER).GT.0.1)REDUC(LAYER)=3.4
C -----
C CALCULATION OF PRESSURE HEAD PSIO
C IF(BULK(LAYER).LE.0.2)PSIO(LAYER)=-5000.
C IF(BULK(LAYER).GT.0.2)PSIO(LAYER)=-10000.
C RETURN
C END
C *****
C SUBROUTINE CAPTOT
C =====
C
C SUBROUTINE CAPTOT CONTROLS INPUT, CALCULATIONS AND OUTPUT
C FOR THE CALCULATION OF THE SOIL MOISTURE DISTRIBUTION IN
C CASE OF CAPILLARY RISE AND INFILTRATION.
C =====
C
C INTEGER PEAT
C LOGICAL CRACK,FLN,FLP,ERROR
C CHARACTER DESCR,HEAD,ANSWER
C CHARACTER*20 FILNAM
C REAL MEDIAN,KSAT,KSATEF
C DIMENSION GWL(15)
C COMMON/TABDAT/TABPRH(10,80),TABCON(10,80),NUMTAB(10),INTERP
C COMMON/GPONEG/NFLNS,NFLNE,NFLPS,NFLPE
C COMMON/RYTEMA/RYTKO(10),RYTETA(10),RYTA(10),RYTN(10),
C * RYTHA(10),RYTHLM(10)
C COMMON/LINE/SUCLIN(10,4),CONLIN(10,4),ALIN(10,2),BLIN(10,3)

```

```

COMMON/SDIL/THICK(10), THKLAY(10), GWL, DESCR(10, 15)
COMMON/INFIL/SUCINF(15, 51), ZINF(51), NZINF
COMMON/RISE/KSAT(10), PSIA(10), Z(15, 54), H(54), FLUX(15),
* METHOD, NFLUXS, NLAYER, LAYER, HEAD(80)
COMMON/BLOEM/KSATEF(10), PSICOR(10), PSIEFF(10), PSIO(10),
* SLOPES(10), SLOPE(10), SLPCOR(10), F(10), REDUC(10),
* DIFFER(10, 15), SIZE(15), BULK(10), PEAT(10), HUMUS(10),
* MEDIAN(10), NSIZES, CRACK(10)
C
C ---- WHAT METHOD OF CONDUCTIVITY DESCRIPTION SHOULD BE USED?
CALL CAPQUE(ERROR)
IF(ERROR) RETURN
C
C ---- WHAT KIND OF CALCULATIONS?
WRITE(6, 1001)
1001 FORMAT('What kind of calculations: ', ' (1) Pressure ',
* 'head distribution and height of capillary rise (type 1), or ',
* ' (2) Maximally possible fluxes (type 2)? ', '$')
READ(5, *) IANS
IF(IANS.NE. 1. AND. IANS.NE. 2) GOTO 2
C
C ---- FOR WHICH FLUX DENSITIES SHOULD THE CALCULATIONS BE PERFORMED?
IF(IANS.EQ. 1) CALL FLXQUE
C
C =====
C =
C = GROUNDWATER LEVELS
C =
C =====
C
C ---- HOW MANY GROUNDWATER LEVELS HAVE TO BE CONSIDERED?
WRITE(6, 1010)
1010 FORMAT('How many groundwater levels should be taken ',
* '(max. 15)? ', '$')
READ(5, *) NGWLS
IF(NGWLS.LE. 0. OR. NGWLS.GT. 15) GO TO 10
C
C ---- FROM WHAT DEVICE SHOULD THEY BE READ?
WRITE(6, 1030)
1030 FORMAT('Should the groundwater levels be read from a file ',
* '(Y/N)? ', '$')
READ(5, 1040) ANSWER
FORMAT(A1)
C
C IF(ANSWER.EQ. 'Y') GO TO 200
C
C ---- READING GROUNDWATER LEVELS FROM TERMINAL
WRITE(6, 1100)
1100 FORMAT('Type the groundwater levels to be used in ',
* 'ascending order' / ' (in cm ',
* 'below the soil surface): ', '/')
DO 100 IGWL=1, NGWLS
WRITE(6, 1110) IGWL
1110 FORMAT('Groundwaterlevel(', I2, ') = ', '$')
READ(5, *) GWLG(IGWL)
IF(IGWL.GT. 1. AND. GWLG(IGWL).LT. GWLG(IGWL-1)) THEN
WRITE(6, 1112)
1112 FORMAT('*** Groundwaterlevels should be entered in ',
* 'ascending order. Try again! ***')
GOTO 1108
END IF
C
C *****
C
100 CONTINUE
GO TO 300
C
C ---- READING GROUNDWATER LEVELS FROM DISK
WRITE(6, 1122)
1122 FORMAT('What is the name of the file? ', '$')
READ(5, 1123) FILNAM
FORMAT(A20)
OPEN(UNIT=21, NAME=FILNAM, TYPE='OLD', ERR=230)
DO 220 IGWL=1, NGWLS
READ(21, *) END=250) GWLG(IGWL)
IF(IGWL.GT. 1. AND. GWLG(IGWL).LT. GWLG(IGWL-1)) THEN
WRITE(6, 1112)
GOTO 20
END IF
CONTINUE
CLOSE(UNIT=21)
GO TO 300
C
C ---- ERROR IN FILENAME
WRITE(6, 1125) FILNAM
1125 FORMAT('??? Error opening file ', A20, ' ???', /,
* ' Retype filename: ', '$')
GO TO 210
C
C ---- REQUIRED AMOUNT OF GROUNDWATERLEVELS NOT IN FILE
CLOSE(UNIT=21)
NGWLS=IGWL
WRITE(6, 1130) NGWLS
1130 FORMAT('??? Only ', I2, ' Groundwaterlevels in file ???', /,
* ' Stop execution (Y/N)? ', '$')
READ(5, 1040) ANSWER
IF(ANSWER.NE. 'Y') GO TO 300
RETURN
C
C ---- CALCULATIONS AND OUTPUT
IF(IANS.EQ. 1) GOTO 305
CALL MAXFLX(GWLQ, NGWLS)
RETURN
C
C ---- ARE THERE POSITIVE AND NEGATIVE FLUXES?
FLP=.FALSE.
IF(NFLPS.NE. 0) FLP=.TRUE.
FLN=.FALSE.
IF(NFLNS.NE. 0) FLN=.TRUE.
C
C ---- CALCULATIONS OF SOIL MOISTURE DISTRIBUTION
DO 400 IGWL=1, NGWLS
GWL=GWLG(IGWL)
IF(FLN) CALL CAPINF
IF(FLN) CALL TABINF
IF(FLP) CALL CAPRIS
IF(FLP) CALL LABEL
400 CONTINUE
C
C RETURN
END
C
C *****

```



```

DO 960 I=IFL+1,NFLXS
  IFL=1
  IF(FLUX(IFL),LT.0.0)GO TO 980
  CONTINUE
  IFL=IFL+1
C 960
C 970
C 980
  NFLPE=IFL-1
  IF(NFLPE.EQ.NFLPS.AND.ABS(FLUX(NFLPE)),LT.1E-6)THEN
    NFLPE=0
    NFLPS=0
  END IF
C 999
  RETURN
  END
C *****
C SUBROUTINE MAXFLX(GWLQ,NGWLS)
C =====
C =
C = SUBROUTINE MAXFLX PERFORMS THE CALCULATIONS TO FIND THE
C = MAXIMALLY POSSIBLE FLUX AT GIVEN PRESSURE HEAD AND
C = GROUNDWATER LEVEL
C =
C =====
C LOGICAL INTEGR, OPEN
C CHARACTER HEAD, REGL(100), CI*5
C DIMENSION PRHQ(10),Q(10,15),GWLQ(15)
C COMMON/SOIL/THICK(10),THKLAY(10),GWL,DESCR(10,15)
C COMMON/RISE/KSAT(10),PSIA(10),Z(15,54),H(54),FLUX(15),
C METHOD,NFLXS,NLAYER,LAYER,HEAD(80)
C *****
C FOR WHICH PRESSURE HEADS SHOULD CALCULATIONS BE PERFORMED?
C 5
  WRITE(6,2010)
  FORMAT(/,' How many pressure heads should be ',
  * 'considered? (max. 10) ',)
  READ(5,*)NPRHQ
  IF(NPRHQ.LT.1.OR.NPRHQ.GT.10)GOTO 5
  DO 6 J=1,NPRHQ
    WRITE(6,2020)J
    FORMAT(' Please type pressure head('',12,'') in cm.? ',)
    READ(5,*)PRHQ(J)
    IF(AMOD(PRHQ(J),100.0).GT.1.E-5) THEN
      WRITE(6,2035)
      FORMAT(' *** Pressure heads should be multiples ',
      * ' of 100. Try again. ***')
      GOTO 2015
    END IF
    PRHQ(J)=-1.0*ABS(PRHQ(J))
  CONTINUE
C 6
C FOR WHAT LEVEL SHOULD CALCULATIONS BE PERFORMED?
  WRITE(6,2030)
  FORMAT(/,' For which depth below the surface should ',
  * 'calculations be performed? (cm.) ',)
  READ(5,*)DEPTH
C *****
  INITIALIZE ARRAY
  DO 20 J=1,10
    DO 10 I=1,10
      G(J,I)=0.0
      CONTINUE
    CONTINUE
    GROUNDWATER LEVELS
    WRITE(6,2032)
    FORMAT(/)
    IGWL=0
    25 IGWL=IGWL+1
    GWL=GWLQ(IGWL)
    WRITE(6,2035)IGWL,GWL
    FORMAT('','',1)'m working on groundwater level ('',12,''), ',
    * F4.0, ' cm. ')
    2035
    C -----
    C -----
    C CALCULATE POSITION OF GROUNDWATER LEVEL RELATIVE TO TOP OF
    C SOIL PROFILE.
    C
    THTOT=0.0
    DO 30 ILAYER=1,NLAYER
      LAY=ILAYER
      THTOT=THTOT+THKLAY(LAY)
      IF(THTOT.GE.GWL)GO TO 40
    CONTINUE
    30
    C -----
    C -----
    C GROUNDWATERLEVEL BELOW SOIL PROFILE.
    WRITE(6,2040)GWL,THTOT
    FORMAT(/,' ??? WARNING: GROUNDWATERLEVEL ',F7.1,' BELOW ',
    * ' SOIL PROFILE ',F7.1,' ???')
    DO 35 IPQ=1,NPRHQ
      G(IPQ,IGWL)=0.0
    CONTINUE
    GOTO 210
    35
    C -----
    C -----
    C POSITION OF BOUNDARIES OF LAYERS
    THICK(LAY)=GWL-THTOT+THKLAY(LAY)
    IF(LAY.EQ.1)GO TO 55
    DO 50 I=LAY-1,1,-1
      THICK(I)=THICK(I+1)+THKLAY(I)
    CONTINUE
    50
    C -----
    C -----
    C START OF ITERATION PROCEDURE
    55 DO 200 IPQ=1,NPRHQ
      PQ=PRHQ(IPQ)
      DO 60 IFQ=1,10
        IFQ=IFQ
        FQ=IFQ*0.1
        LAYER=LAY
        IF(.NOT.(INTEGR(PQ,FQ,DEPTH)))GOTO 70
        CONTINUE
      GOTO 150
      60
      C -----
      C -----
      C SECOND ITERATION ROUND
      FQ=0.1*(IFQ1-1)
      DO 100 IFQ=1,9
        FQ=FQ+0.01
        LAYER=LAY
        IF(.NOT.(INTEGR(PQ,FQ,DEPTH)))GOTO 150
        CONTINUE
        FQ=FQ+0.01
      100
      C -----
      C -----

```

```

C -----
150  ROUNDED THE FLUX
      FG=FG-O.005
      LAYER=LAY
      IF (.NOT. (INTEGR(IPQ,FG,DEPTH))) THEN
        G(IPG,IGWL)=FG-O.005
      ELSE
        G(IPG,IGWL)=FG+O.005
      END IF
      GOTO 200
C
C -----
180  FLUX > 10 MM
      G(IPG,IGWL)=-1.0
C
C -----
200  CONTINUE
C
C -----
210  NEXT GROUNDWATERLEVEL
      IF (IGWL.LT.NGWLS)GOTO 25
      WRITE(6,2045)
      FORMAT('+',I,'m ready
*,
2045  *,
C
C -----
2550  PREPARING THE OUTPUT
      HEADING
      WRITE(10,2050)(HEAD(I),I=1,80),DEPTH
      FORMAT(///,T45,'MAXIMALLY POSSIBLE FLUXES
T45, '
*,
2560  T85,'LEVEL OF CALCULATIONS=',F5.0,' CM.
      WRITE(10,2060)
      FORMAT(' ',130('='))
      WRITE(10,2070)(GWLQ(I),I=1,NGWLS)
      FORMAT(' ',PR,HEAD',T13,'*,T40,'G R O U
*,
2570  ' L E V E L (CM. BELOW SURFACE)',/,/,
*,
      T13,'*,15F7.0)
      WRITE(10,2060)
C
C -----
2580  FLUXES
      DO 300 IPRH=1,NPRHG
        WRITE(10,2080)PRHG(IPRH),(G(IPRH,IGWL
        FORMAT(' ',F8.0,T13,'*,15F7.2)
      CONTINUE
      WRITE(10,2060)
      WRITE(10,2090)
      FORMAT(/, ' NOTE : The figure -1.00 indic
*,
2590  ' of a flux > 1.0 cm/day !',/, ' ----',/,
C
C -----
310  PREPARING A PRINTPLOT OF THE RESULTS
      WRITE(6,2095)
      FORMAT(/, ' For which pressure head (cm) o
2095  *,
      ' Standard is -1000 cm.
      ',$)
      READ(5,*,ERR=410)IPR
      PR=-1.0*ABS(IPR)
      DO 400 J=1,NPRHG
        IF (ABS(PRHG(J)-PR).LE.1E-4) THEN
          IPR=J
          GOTO 450
        END IF
      CONTINUE
      DO 400
C
C -----
410  NOT FOUND
      WRITE(6,2098)IPR
      FORMAT(' Pressure head ',F6.0,' not in
2098

```

```

C *****
C C-----
C 450 PRINTPLOT
C 2099 WRITE(10,2099)(HEAD(I),I=1,80),PR
      FORMAT('1'//T35,'PRINTPLOT OF CAPILLARY RISE (mm/day) VERSUS',
      * 'GROUNDWATERDEPTH'/T35,60('=')//T12,80A1,T95,'Pressure',
      * head : ',FB.O.',cm.'//')
      DO 900 I=100,0,-2
        DO 480 J=1,100
          REGE(J)=', '
        CONTINUE
        RI=1/100.0
        CI=', '
        IF (MOD(I,10).EQ.0) THEN
          II=I/10
          WRITE(CI, '(I2)' )II
          GI(3:5)=' -I',
        END IF
        DO 500 IGWL=1,NGLWS
          IF ((G(IPR,IGWL).GE.0.)AND.(G(IPR,IGWL).LE.RI)) GOTO 600
        CONTINUE
        NOT FOUND
        GOTO 800
      CONTINUE
      INTERPOLATION
      IF (G(IPR,IGWL-1).LT.0.0) GOTO 900
      PART=(G(IPR,IGWL-1)-RI)/(G(IPR,IGWL-1)-G(IPR,IGWL))
      PLGWL=GWLQ(IGWL-1)+(GWLQ(IGWL)-GWLQ(IGWL-1))*PART
      IPLGWL=(PLGWL)/2.0+1.5
      REGE(IPLGWL)='*',
      WRITE(10,3000)CI,REGE
      FORMAT(5X,A5,100A1)
      CONTINUE
    X-AXIS
    WRITE(10,3010)(I,I=10,200,10)
    FORMAT(10X,20('-'),',',10X,'O ',20(2X,I3)//T45,'GROUNDWATER',
    * 'LEVEL (cm below surface)')
    RETURN
    END
C *****
C C-----
C LOGICAL FUNCTION INTEGR(PG,FG,DEPTH)
C =====
C =
C =
C =
C =
C FUNCTION INTEGR PERFORMS THE NUMERICAL INTEGRATION
C =====
C =
C =
C =
C INTEGER COUNT
C COMMON/SOIL/THICK(10),THKLAY(10),GWL,DESCR(10,15)
C COMMON/RISE/KSAT(10),PSIA(10),Z(15,54),H(54),FLUX(15),
C METHOD,NFLUXS,NLAYER,LAYER,HEAD(80)
C
C INTEGR=.FALSE.
C
C C-----
C CALCULATION OF HEIGHT OF CAPILLARY RISE
C STEP=-1.0

```

```

      SIZINT=-0.1  

      COUNT=-1  

      SUCT=0.0  

      ZOLD=0.0  

      ZH=0.0  

      DO 200 ISTEP=1,54  

        IF(ISTEP.EQ.1)GO TO 100  

        SET HEIGHT EQUAL TO THAT IN PREVIOUS STEP  

        IS1=ISTEP-1  

        ZOLD=ZH  

        COUNT=COUNT+1  

        IF(COUNT.NE.10)GO TO 110  

        COUNT=1  

        NEW STEP SIZES  

        SIZINT=STEP  

        STEP=10.0+STEP  

        SUCB=SUCT  

        SUCT=SUCT+STEP  

        SUCL=SUCB-SIZINT  

        SUCU=SUCB  

        DIVIDE INTERVAL IN 10 PIECES AND INTEGRATE  

        DO 170 ISIZE=1,10  

          SUCL=SUCL+SIZINT  

          SUCU=SUCU+SIZINT  

          SUCAV=0.5*(SUCL+SUCU)  

          CONDUCTIVITY  

          CAPCON=CONDC(SUCAV)  

          HEIGHT OF CAPILLARY RISE  

          IF(CAPCON.LT.1.E-16)GO TO 170  

          DZ=SIZINT/(1.0 + (FG/CAPCON))  

          IF(DZ.GT.-1.E-16)GO TO 170  

          ZH=ZH-DZ  

          BOUNDARY BETWEEN LAYERS?  

          IF(LAYER.EQ.1.OR.ZH.LT.THICK(LAYER))GO TO 140  

          CORRECTION. FIND BOUNDARY SUCTION  

          ZN=THICK(LAYER)  

          BOUND=SUCL-(THICK(LAYER)-ZOLD)*(SIZINT/DZ)  

          NEXT LAYER  

          LAYER=LAYER-1  

          SUCAV=0.5*(SUCU+BOUND)  

          CONDUCTIVITY  

          CAPCON=CONDC(SUCAV)  

          CAPILLARY HEIGHT  

          IF(CAPCON.LT.1.E-16)GO TO 170  

          DZ=(SUCU-BOUND)/(1.0 + (FG/CAPCON))  

          IF(DZ.GT.-1.E-16)GO TO 170  

          ZH=ZN-DZ  

          HEIGHT  

          ZOLD=ZH  

          READY?  

          IF(ZH.GE.THICK(1)-DEPTH)GOTO 220  

          WRITE(6,1010)GWL,THTOT
    
```

```

1010 *   FORMAT(/, ' ??? WARNING: GROUNDWATERLEVEL ', F7.1, ' BELOW ',
      *   ' SOIL PROFILE ', F7.1, ' ???')
      *   GWL=THTOT
C -----
C 40    POSITION OF BOUNDARIES OF LAYERS
      *   THICK(LAYER)=GWL-THTOT+THKLAY(LAYER)
      *   IF(LAYER.EQ.1)GO TO 60
      *   DO 50 I=LAYER-1,1,-1
      *     THICK(I)=THICK(I+1)+THKLAY(I)
      *   CONTINUE
C -----
C 60    DO 70 I=NFLPS,NFLPE
      *   INTPOS(I)=LAYER
      *   CONTINUE
C -----
C 70    CALCULATION OF HEIGHT OF CAPILLARY RISE
      *   STEP=-1.0
      *   SIZINT=-0.1
      *   COUNT=-1
      *   SUCT=0.0
      *   DO 200 ISTEP=1,54
      *     IF(ISTEP.EQ.1)GO TO 100
      *     SET HEIGHT EQUAL TO THAT IN PREVIOUS STEP
      *     ISI=ISTEP-1
      *     DO 90 J=NFLPS,NFLPE
      *       Z(J,ISTEP)=Z(J,ISI)
      *     CONTINUE
      *     COUNT=COUNT+1
      *     IF(COUNT.NE.10)GO TO 110
      *     COUNT=1
      *     NEW STEP SIZES
      *     SIZINT=STEP
      *     STEP=10.0*STEP
      *     SUCB=SUCT
      *     SUCT=SUCT+STEP
      *     H(ISTEP)=SUCT
      *     SUGL=SUCB-SIZINT
      *     SUCU=SUCB
      *     DIVIDE INTERVAL IN 10 PIECES AND INTEGRATE
      *     DO 170 ISIZE=1,10
      *       SUGL=SUGL+SIZINT
      *       SUCU=SUCU+SIZINT
      *       DO 150 IFL=NFLPS,NFLPE
      *         IFLUX=IFL
      *       ALREADY ABOVE SOIL SURFACE?
      *       IF(FINISH(IFLUX))GO TO 150
      *       LAYER=INTPOS(IFLUX)
      *       SUCAV=0.5*(SUGL+SUCU)
      *     CONDUCTIVITY
      *     CAPCON=CONDOC(SUCAV)
      *   HEIGHT OF CAPILLARY RISE
      *   IF(CAPCON.LT.1.E-16)GO TO 150
      *   DZ=SIZINT/(1.0 + (FLUX(IFLUX)/CAPCON))
      *   IF(DZ.GT.-1.E-16)GO TO 150
      *   ZH=Z(IFLUX,ISTEP)-DZ
      *   BOUNDARY BETWEEN LAYERS?

```

```

      *   IF(LAYER.EQ.1.OR.ZH.LT.THICK(LAYER))GO TO 140
      *   CORRECTION. FIND BOUNDARY SUCTION
      *   ZH=THICK(LAYER)
      *   BOUND=SUGL-(THICK(LAYER)-Z(IFLUX,ISTEP))*
      *     (SIZINT/DZ)
      *   NEXT LAYER
      *   LAYER=LAYER-1
      *   INTPOS(IFLUX)=LAYER
      *   SUCAV=0.5*(SUCU+BOUND)
      *   CONDUCTIVITY
      *   CAPCON=CONDOC(SUCAV)
      *   CAPILLARY HEIGHT
      *   IF(CAPCON.LT.1.E-16)GO TO 150
      *   DZ=(SUCU-BOUND)/(1.0 + (FLUX(IFLUX)/CAPCON))
      *   IF(DZ.GT.-1.E-16)GO TO 150
      *   ZH=ZH-DZ
      *   HEIGHT
      *   Z(IFLUX,ISTEP)=ZH
      *   CONTINUE
      *   CONTINUE
      *   READY
      *   HALT=.TRUE.
      *   DO 180 I=1,NFLUXS
      *     IF(FINISH(I))GO TO 180
      *     IF(Z(I,ISTEP).GT.THICK(I))GO TO 175
      *     HALT=.FALSE.
      *     GO TO 180
      *   FINISH(I)=.TRUE.
      *   CONTINUE
      *   IF(HALT)GO TO 250
      *   CONTINUE
      *   RETURN
      *   END
C -----
C *****
C SUBROUTINE CAPINF
C =====
C =
C = SUBROUTINE TO CALCULATE PRESSURE HEADS IN CASE OF
C = INFILTRATION.
C =
C =====
C
C INTEGER PEAT,COUNT
C LOGICAL CRACK,ILLFLX(15)
C CHARACTER DESCR,HEAD
C REAL MEDIAN,KSAT,KSATEF
C COMMON/TABDAT/TABPRH(10,80),TABCON(10,80),NUMTAB(10),INTERP
C COMMON/OPDNEG/NFLNS,NFLNE,NFLPS,NFLPE
C COMMON/RYTEMA/RYTOKO(10),RYTETA(10),RYTA(10),RYTN(10),
C RYTHA(10),RYTHLM(10)
C * COMMON/LINE/SUCLIN(10,4),CONLIN(10,4),ALIN(10,3),BLIN(10,3)

```

```

COMMON/SOIL/THICK(10), THKLAY(10), GWL, DESCR(10, 15)
COMMON/INFL/SUCINF(15, 51), ZINF(51), NZINF
COMMON/RISE/KSAT(10), PSIA(10), Z(15, 54), H(54), FLUX(15),
METHOD, NPLUXS, NLAYER, LAYER, HEAD(80)
COMMON/BLOEM/KSAFEF(10), PSICOR(10), PSIEFF(10), PSID(10),
SLOPES(10), SLOPE(10), SLPCOR(10), F(10), REDUC(10),
DIPER(10, 15), SIZE(15), BULK(10), PEAT(10), HUMUS(10),
MEDIAN(10), NSIZES, CRACK(10)

C C -----
MAXIMUM ALLOWED NUMBER OF ITERATIONS.
MAITR=25

C C -----
INITIALISATION OF ARRAYS
DO 5 I=1, 15
    ILLFLX(I)=FALSE.
5 CONTINUE

C DO 20 J=1, 51
    DO 10 I=1, 15
        SUCINF(I, J)=0.0
10 CONTINUE
20 CONTINUE
ZINF(J)=0.0

C C -----
POSITION OF GROUNDWATER LEVEL
THTOT=0.0
DO 30 ILAYER=1, NLAYER
    LAYER=N_LAYER
    THTOT=THTOT+THKLAY(LAYER)
IF(THTOT.GE. GWL)GO TO 40
30 CONTINUE

C C -----
GROUNDWATER LEVEL BELOW DEPTH OF SOIL PROFILE
WRITE(6, 1010)GWL,THTOT
FORMAT(/, , ??? WARNING: GROUNDWATERLEVEL ', F7.1,' BELOW ',
' SOIL PROFILE ', F7.1,' ???')
THTOT=GWL

C 40 THICK(LAYER)=GWL-THTOT+THKLAY(LAYER)
IF(LAYER.EQ. 1)GO TO 60
DO 50 I=LAYER-1, 1,-1
    THICK(I)=THICK(I+1)+THKLAY(I)
50 CONTINUE

C C -----
WHAT STEP SIZE?
60 DZ=FIX(GWL/50. + 0.999)

C C -----
INTEGRATION
LAYER=N_LAYER
ZH=0.0
DZI=0.05*DZ
ZAV=-0.25*DZI
DO 90 I=2, 51
    DO 90 IFLUX=1,NPLUXS
        SUCINF(IFLUX, I)=SUCINF(IFLUX, I-1)
90 CONTINUE
DO 290 KL=1, 20
    ZH=ZH+DZI
```

```

C -----
C
AVERAGES
ZAV=ZAV+DZ1
IF (ZH.GT.GWL) GO TO 400
NZINF=1
ZINF(NZINF)=ZH
IF (ZAV.LT.THICK(LAYER)) GO TO 110
LAYER=LAYER+1
DO 200 IFLUX=NFLNS,NFLNE
110
C
C -----
C
INTEGRATION NECESSARY?
IF (ILLFLX(IFLUX)) GO TO 200
C
C -----
C
START OF INTEGRATION
NUMITR=0
SUCOLD=SUCINF(IFLUX,NZINF)
SUCNEW=SUCOLD
SUCANT=SUCOLD
DO WHILE (NUMITR.LE.MAXITR)
SUCAV=(SUCNEW+SUCOLD+SUCANT)/3.0
C
C -----
C
CONDUCTIVITY
CAPCON=CONDOC(SUCAV)
C
C -----
C
NEW PRESSURE HEAD
SUCTST=SUCOLD-DZ1*(1.0+(FLUX(IFLUX)/CAPCON))
C
C -----
C
IS IT GOOD ENOUGH?
IF (ABS(SUCTST-SUCNEW).LT.ABS(0.01*SUCTST)) GO TO 150
C
C -----
C
NO. START ANOTHER ITERATION
SUCANT=SUCNEW
SUCNEW=SUCTST
NUMITR=NUMITR+1
END DO
C
C -----
C
REQUIRED ACCURACY NOT REACHED
WRITE(6,3010) IFLUX,NZINF,MAXITR,SUCTST
FORMAT(' ??? AT FLUX',I3,' AND HEIGHT',I3,' MAXIMUM',
' ALLOWED NUMBER OF ITERATIONS (' ,I3,' ) REACHED. ',/,
' PRESURE HEAD ',F7.2,' CM. ASSUMED. ',/,/)
C
C -----
C
CORRECT VALUE
SUCINF(IFLUX,NZINF)=SUCTST
IF (SUCINF(IFLUX,NZINF).GT.0.0) ILLFLX(IFLUX)=.TRUE.
C
C -----
C
CONTINUE
CONTINUE
CONTINUE
C
C -----
C
ILLEGAL FLUXES?
DO 500 IFLUX=NFLNS,NFLNE
IF (.NOT. ILLFLX(IFLUX)) GO TO 500
WRITE(6,1090) IFLUX(IFLUX)
FORMAT(' ',I3,' ???', FLUX OF ',F7.4,' CM/DAY IS NOT',
' REALISTIC FOR THIS SOIL ???')
DO 450 I=1,51
SUCINF(IFLUX,I)=0.0
CONTINUE
CONTINUE
CONTINUE
C
C -----
C
450
500
C
3010
*
*
150
200
290
300
C
C -----
C
400
1090
*
450
500
C
RETURN

```

END

27

SUBROUTINE BRG1NP

```

=====
SUBROUTINE TO TAKE CARE OF THE INPUT NECESSARY FOR THE
CALCULATIONS WHEN THE CONDUCTIVITY IS DESCRIBED ACCORDING TO
THE BROOKS AND COREY METHOD.
=====

```

INTEGER PEAT

LOGICAL CRACK

CHARACTER DESCR, HEAD, ANSWER

CHARACTER*20 FILNAM

REAL MEDIAN, KSAT, KSATF

COMMON/SOIL/THICK(10), THKLAY(10), GML, DESCR(10,15)

COMMON/RISE/KSAT(10), PSIA(10), Z(15,54), H(54), FLUX(15),

METHOD, NFLUXS, NLAYER, LAYER, HEAD(80)

COMMON/BLOEM/KSATF(10), PSICOR(10), PSIEFF(10), PSID(10),

SLOPES(10), SLOPE(10), SLPICOR(10), F(10), REDUC(10),

DIFPER(10,15), SIZE(15), BULK(10), PEAT(10), HUMUS(10),

MEDIAN(10), NSIZES, CRACK(10)

INPUT FROM TERMINAL OR FILE?

WRITE(6,1000)

FORMAT(/, ' Did you prepare the data in a file? (Y/N) ', \$)

READ(5,1010) ANSWER

FORMAT(A1)

IF(ANSWER.EQ. 'Y') GO TO 300

INPUT FROM TERMINAL

WRITE(6,1020)

FORMAT(/, ' Give a description of the soil profile. '

READ(5,1030)(HEAD(I), I=1,80)

FORMAT(80A1)

READ THE NUMBER OF LAYERS IN THE PROFILE

WRITE(6,1040)

FORMAT(/, ' How many layers are in the profile? ', T60, ' ', \$)

READ(5,*,ERR=110) NLAYER

READ THE DATA FOR EACH LAYER

DO 280 LAYER=1, NLAYER

WRITE(6,1060) LAYER

FORMAT(/, ' Type a short description of layer ', I2,

' (max. 15 char.) ', T60, ' ', \$)

READ(5,1030)(DESCR(LAYER,I), I=1,15)

WRITE(6,1070) LAYER

FORMAT(/, ' What is the thickness of layer ', I2,

' (cm.) ', T60, ' ', \$)

READ(5,*,ERR=150) THKLAY(LAYER)

WRITE(6,1090) LAYER

FORMAT(/, ' What is the effective conductivity of layer ', I2,

' (cm/day) ', T60, ' ', \$)

READ(5,*,ERR=180) KSATF(LAYER)

WRITE(6,1100) LAYER

FORMAT(/, ' What is the effective air entry value of layer ',

28

```

12, ' (cm.) ', T60, ' ', $)
READ(5,*,ERR=200) PSIEFF(LAYER)
PSIEFF(LAYER)=-1.0*ABS(PSIEFF(LAYER))
WRITE(6,1110) LAYER

```

FORMAT(/, ' What is the slope of the pF-curve for layer ',

I2, ' ', T60, ' ', \$)

READ(5,*,ERR=220) SLOPES(LAYER)

WRITE(6,1120) LAYER

FORMAT(/, ' Does horizontal cracking occur in layer ',

I2, ' (Y/N) ', T60, ' ', \$)

READ(5,1010) ANSWER

CRACK(LAYER)=FALSE

IF(ANSWER.EQ. 'Y') CRACK(LAYER)=TRUE

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

280

CONTINUE

GO TO 500

```

30
DO 200 LAYER=1,NLAYER
  WRITE(6,2045)LAYER
  FORMAT(/,' Give a short description of layer',I3,
    (max. 15 char.)?',T60,'',$)
  READ(5,2020)(DESCR(LAYER,I),I=1,15)
  WRITE(6,2050)LAYER
  FORMAT(' What is the saturated conductivity (cm/d) of layer',
    I3,'?',T60,'',$)
  READ(5,*)RYTKO(LAYER)
  WRITE(6,2070)LAYER
  FORMAT(' What is the air entry value (cm) of layer',I3,
    '?',T60,'',$)
  READ(5,*)RYTHA(LAYER)
  RYTHA(LAYER)=-1.0*ABS(RYTHA(LAYER))
  WRITE(6,2080)LAYER
  FORMAT(' What is the value of b for layer',I3,'?',
    T60,'',$)
  READ(5,*)RYTETA(LAYER)
  WRITE(6,2090)LAYER
  FORMAT(' What is the limiting pressure head (cm) ',
    'for layer',I3,'?',T60,'',$)
  READ(5,*)RYTHLM(LAYER)
  RYTHLM(LAYER)=-1.0*ABS(RYTHLM(LAYER))
  WRITE(6,2100)LAYER
  FORMAT(' What is the value of the coefficient a of layer',
    I3,'?',T60,'',$)
  READ(5,*)RYTA(LAYER)
  WRITE(6,2110)LAYER
  FORMAT(' What is the value of coefficient n of layer',I3,
    '?',T60,'',$)
  READ(5,*)RYTN(LAYER)
  RYTN(LAYER)=ABS(RYTN(LAYER))
  WRITE(6,2120)LAYER
  FORMAT(' What is the thickness (cm) of layer',I3,'?',
    T60,'',$)
  READ(5,*)THKLAY(LAYER)
  200 CONTINUE
  GO TO 300

=====
=
= INPUT FROM DISK
=
=====

300 WRITE(6,3005)
3005 FORMAT(' What is the name of the datafile?', $)
305 READ(5,3006)FILNAM
3006 FORMAT(A20)
  OPEN(UNIT=21,NAME=FILNAM,TYPE='OLD',ERR=310)
  GO TO 315

  ERROR OPENING FILE
  310 WRITE(6,3007)FILNAM
3007 FORMAT(' ??? Error opening file ',A20./,' Type correct',
  ' filename?', $)
  GO TO 305

  READING DATA
  315 READ(21,3010)(HEAD(I),I=1,80)

```

```

3010 FORMAT(BOA1)
320 NLAYER=O
    NLAYER=N-LAYER+1
    READ(21,3015,END=330)(DESCR(NLAYER,I),I=1,15)
3015 FORMAT(15A1)
    READ(21,*)RYTKO(NLAYER),RYTHA(NLAYER),RYTETA(NLAYER),
    RYTHLM(NLAYER),RYTA(NLAYER),RYTN(NLAYER),THKLAY(NLAYER)
    RYTHA(NLAYER)=-1.0*ABS(RYTHA(NLAYER))
    RYTHLM(NLAYER)=-1.0*ABS(RYTHLM(NLAYER))
    RYTIN(NLAYER)=ABS(RYTIN(NLAYER))
    GO TO 320
C
330 NLAYER=N-LAYER-1
    CLOSE(UNIT=21)
C
C ---- SHOW THE READ DATA
C =====
500 WRITE(10,7000)(HEAD(I),I=1,80)
7000 FORMAT(' ',BOA1,' ')
    DO 710 LAYER=1,NLAYER
        WRITE(10,7030)LAYER,(DESCR(LAYER,I),I=1,15),THKLAY(LAYER),
        RYTKO(LAYER),RYTHA(LAYER),RYTMO(LAYER),RYTETA(LAYER),
        RYTHAL(LAYER),RYTHLM(LAYER),RYTHA(LAYER),RYTA(LAYER),
        RYTIN(LAYER),RYTHLM(LAYER)
        CONTINUE
710 FORMAT(' ',LAYER,' ',13,T30,15A1,T60,THICKNESS='F7.1','CM',
    //,'TIO','K','=','F10.1','CM/DAY',T80,'IF','F7.1','<=','H',//,
    T10,'K','=','F10.1',' * EXP('F8.5',' * ('F7.1',' + H'))',
    T80,'IF','F7.1','<=','H<',F7.1/T10,' K','=','F10.2',
    ' * ('(-H) ** -'F7.4')',T80,'IF H<',F7.1)
C
    RETURN
    END
C *****
C SUBROUTINE LINIMP
C =====
C
C This subroutine reads the data and gives them in a table =
C when an approximation of the hydraulic conductivity =
C function by three straight line pieces has been chosen. =
C =====
C
REAL KSAT
CHARACTER HEAD,ANSWER,DESCR
CHARACTER*20 FILNAM
COMMON/LINE/SUCLIN(10,4),CONLIN(10,4),ALIN(10,3),BLIN(10,3)
COMMON/SOL/THICK(10),THKLAY(10),GWL,DESCR(10,15)
COMMON/RISE/KSAT(10),PSIA(10),Z(15,54),H(54),FLUX(15),
METHOD,NFLUXS,NLAYER,LAYER,HEAD(80)
C
C ----- From where should the data be read?
C
1010 WRITE(6,1010)
    FORMAT(' Did you prepare the data in a datafile ',
    '(Y/N)?','$')
    READ(5,1020)ANSWER
    IF(ANSWER.EQ.'Y') GO TO 300
    INPUT FROM TERMINAL
    =====
    WRITE(6,2010)
    FORMAT(' Give a description of the soil profile (max: 80 ch.):'
    READ(5,2020)(HEAD(I),I=1,80)
    FORMAT(BOA1)
C
2030 WRITE(6,2030)
    FORMAT(' Of how many layers does the profile consist?',T60,
    '$')
    READ(5,*)NLAYER
C
DO 200 LAYER=1,NLAYER
    SUCLIN(LAYER,1)=1.0
    WRITE(6,2045)LAYER
    FORMAT(' Give a short description of layer','13,
    '(max: 15 char.)?',T60,'$',
    READ(5,2050)(DESCR(LAYER,I),I=1,15)
    WRITE(6,2050)LAYER
    FORMAT(' +type the saturated conductivity of layer','13,
    '(cm/d) ?',T60,'$',
    READ(5,*)CONLIN(LAYER,1)
    WRITE(6,2070)LAYER
    FORMAT(' +what is the pressure head (cm) at the first',
    ' node of layer','13,?',T60,'$',
    READ(5,*)SUCLIN(LAYER,2)
    WRITE(6,2075)LAYER
    FORMAT(' +what is the conductivity (cm/d) at the first',
    ' node of layer','13,?',T60,'$',
    READ(5,*)CONLIN(LAYER,2)
    WRITE(6,2080)LAYER
    FORMAT(' +type the pressure head (cm) at the second',
    ' node of layer','13,?',T60,'$',
    READ(5,*)SUCLIN(LAYER,3)
    WRITE(6,2085)LAYER
    FORMAT(' +type the conductivity(cm/d) at the second node',
    ' of layer','13,?',T60,'$',
    READ(5,*)CONLIN(LAYER,3)
    WRITE(6,2090)LAYER
    FORMAT(' +what is the pressure head (cm) at the last node of',
    ' layer','13,?',T60,'$',
    READ(5,*)SUCLIN(LAYER,4)
    WRITE(6,2095)LAYER
    FORMAT(' +what is the conductivity (cm/d) at the last node',
    ' of layer','13,?',T60,'$',
    READ(5,*)CONLIN(LAYER,4)
    WRITE(6,2100)LAYER
    FORMAT(' +what is the thickness of layer','13,?(cm)?',
    T60,'$',
    READ(5,*)THKLAY(LAYER)
    CONTINUE
200 GO TO 500
C
C ---- INPUT FROM FILE
C =====

```

```

C -----
C 300 FILENAME
C 3010 WRITE(6,3010)
C 3010 FORMAT('What is the name of the file? ', $)
C 310 READ(5,3020)FILNAM
C 3020 FORMAT(A20)
C 3020 OPEN(UNIT=21, NAME=FILNAM, TYPE='OLD', ERR=317)
C 3020 GO TO 319
C -----
C 317 ERROR IN FILENAME
C 3030 WRITE(6,3030)FILNAM
C 3030 FORMAT(' ??? Error opening file ', A20, /,
* ' Please retype filename: ', $)
C 3030 GO TO 310
C -----
C 319 READ SOIL DESCRIPTION
C 3040 READ(21,3040) (HEAD(I), I=1,80)
C 3040 FORMAT(80A1)
C -----
C 320 DATA FOR EVERY LAYER
C 320 NLayer=0
C 320 NLayer=NLayer+1
C 3050 READ(21,3050,END=330) (DESCR(NLayer, I), I=1,15)
C 3050 FORMAT(15A1)
C 3050 READ(21,*) CONLIN(NLayer, 1), SUCLIN(NLayer, 2),
* CONLIN(NLayer, 2), SUCLIN(NLayer, 3), CONLIN(NLayer, 3),
* SUCLIN(NLayer, 4), CONLIN(NLayer, 4), THKLAY(NLayer)
C 3050 SUCLIN(NLayer, 1)=1.
C 3050 GO TO 320
C -----
C 330 NLayer=NLayer-1
C 330 CLOSE(UNIT=21)
C -----
C 340 CHECK THE PRESSURE HEADS
C 340 =====
C 500 DO 520 LAYER=1, NLayer
C 510 DO 510 I=1, 4
C 520 SUCLIN(LAYER, I)=-1.0*ABS(SUCLIN(LAYER, I))
C 520 CONTINUE
C -----
C 530 CALCULATION OF A AND B IN CONDUCTIVITY = A*(PRESSURE HEAD **B)
C 530 DO 600 LAYER=1, NLayer
C 530 ALIN(LAYER, 1)=CONLIN(LAYER, 1)
C 530 BLIN(LAYER, 1)=(ALOG(CONLIN(LAYER, 2))-ALOG(ALIN(LAYER, 1)))/
* ALOG((-1.0*SUCLIN(LAYER, 2)))
C 530 DO 550 I=2, 3
C 550 II=I+1
C 550 BLIN(LAYER, I)=ALOG(CONLIN(LAYER, II))/CONLIN(LAYER, I))/
* ALOG((-1.0*SUCLIN(LAYER, II))/(-1.0*SUCLIN(LAYER, I)))
C 550 ALIN(LAYER, I)=CONLIN(LAYER, I)/((-1.0*SUCLIN(LAYER, I)))**
* BLIN(LAYER, I))
C 600 CONTINUE
C -----
C 610 SHOW THE DATA
C 610 =====
C 610 WRITE(10, 7000) (HEAD(I), I=1, 80)

```

```

7000 FORMAT(/, ' ', 80A1, '/')
7010 WRITE(10, 7010)
7010 FORMAT(' ', 132('='))
7020 WRITE(10, 7020)
7020 FORMAT(' LAYER', T12, 4('SUCTION', 8X, 'CONDUCT', 7X), /, ' ', T14,
* 4('CM'), 8X, ' (CM/DAY)', 8X))
7020 WRITE(10, 7010)
7020 DO 710 LAYER=1, NLayer
7030 WRITE(10, 7030) LAYER, (SUCLIN(LAYER, I), CONLIN(LAYER, I), I=1, 4)
710 FORMAT(' ', 13, 6X, 4(E11.4, 2X, E11.4, 4X))
710 CONTINUE
710 WRITE(10, 7010)
C -----
7050 WRITE(10, 7050)
7050 FORMAT(/, '/')
7050 WRITE(10, 7010)
7050 WRITE(10, 7060) (I, I=1, 3)
7060 FORMAT(T10, ' LAYER', T37, 3('A', I1, 13X, 'B', I1, 13X), T121,
* 'THICKNESS', /, T122, ' (CM)')
7060 WRITE(10, 7010)
7060 DO 740 LAYER=1, NLayer
740 WRITE(10, 7070) LAYER, (DESCR(LAYER, I), I=1, 15), (ALIN(LAYER, I),
* BLIN(LAYER, I), I=1, 3), THKLAY(LAYER)
7070 FORMAT(' ', 13, 3X, 15A1, 10X, 3(E10.3, 3X, E10.3, 6X), T120, 8B, 1)
740 CONTINUE
740 WRITE(10, 7010)
C -----
C 750 RETURN
C 750 END
C -----
C *****
C SUBROUTINE TABINP
C =====
C =
C = SUBROUTINE TO READ THE K-H RELATION OF A SOIL WHEN
C = IT IS DESCRIBED BY A TABLE OF VALUES.
C =
C =
C =====
C CHARACTER DESCR, HEAD
C CHARACTER*20 FILNAM
C CHARACTER*11 INTXT(2)
C REAL KSAT
C COMMON/TABDAT/TABPRH(10,80), TABCON(10,80), NUMTAB(10), INTERP
C COMMON/SOIL/THICK(10), THKLAY(10), GWL, DESCR(10,15)
C COMMON/RISE/KSAT(10), PSIA(10), Z(15,54), H(54), FLUX(15),
* METHOD, NFLUXS, NLayer, LAYER, HEAD(80)
C DATA INTXT/'LINEAR', 'LOGARITHMIC'/
C -----
C ---- INITIALISATION
C DO 20 I=1, 10
C DO 10 J=1, 80
C TABPRH(I, J)=0.0
C TABCON(I, J)=0.0
C 10 CONTINUE
C NUMTAB(I)=0
C 20 CONTINUE
C -----
C *****

```

```

C ----- WHERE ARE THE DATA? 35
1010 WRITE(6,1010)
1100 FORMAT(//, 'What file contains the required data?', '$')
1020 READ(5,1020)FILNAM
1030 FORMAT(A20)
      OPEN(UNIT=21, NAME=FILNAM, TYPE='OLD', ERR=120)
      GO TO 130
C -----
1200 ERROR
1210 WRITE(6,1030)FILNAM
10300 FORMAT(' ??? Error opening file ',A20,/,
      * ' Please retype filename: ', '$')
      GO TO 110
C -----
1300 READING THE DATA
1310 READ(21,1040)(HEAD(I), I=1,80)
10400 FORMAT(80A1)
C -----
1400 NLAYER=0
      NLAYER=NLAYER+1
      IF(NLAYER.GT.10)GO TO 200
      READ(21,1050,END=200)(DESCR(NLAYER,I), I=1,15)
      FORMAT(15A1)
      READ(21,*,END=200)THKLAY(NLAYER)
      READ(21,*,END=200)NT
      NUMTAB(NLAYER)=NT
      READ(21,*)(TABPRH(NLAYER,I), I=1,NT)
      READ(21,*)(TABCON(NLAYER,I), I=1,NT)
      DO 190 I=1,NT
        TABPRH(NLAYER,I)=-1.0*ABS(TABPRH(NLAYER,I))
      CONTINUE
      GO TO 140
C -----
1900 NLAYER=NLAYER-1
      CLOSE(UNIT=21)
C -----
2000 KIND OF INTERPOLATION
1100 WRITE(6,1110)
1110 FORMAT(//, 'What kind of interpolation between the',
      * ' points in the table do you want?',/, ' Linear (type 1), ',
      * ' or logarithmic (type 2) ', '$')
      READ(5,1120)INTERP
      FORMAT(I1)
      IF((INTERP.NE.1).AND.(INTERP.NE.2))GO TO 1100
C -----
2010 SHOW THE DATA
      WRITE(10,2010)(HEAD(I), I=1,80)
      FORMAT(//, ' ', 80A1, //)
C -----
2020 DO 300 LAYER=1,NLAYER
      WRITE(10,2020)LAYER, (DESCR(LAYER,I), I=1,15), THKLAY(LAYER),
      * INTXT(INTERP)
      * FORMAT(//, TIO, ' LAYER ', I2, T30, T5A1, T50, ' THICKNESS=', F7.1,
      * ' CM ', T85, ' INTERPOLATION: ', A11,/, ' ', I31('=',),/,
      * T4,4, ' PRESS. HEAD ', 2X, ' CONDUCTIVITY ', 6X,/, I31('=',))
      NROW=0.25 * NUMTAB(LAYER) + 1.0
      IF(MOD(NUMTAB(LAYER),4).EQ.0)NROW=NROW-1
      DO 250 NR=1,NROW
        NRX=NR
        WRITE(10,2030)(TABPRH(LAYER,NRX+J*NROW),
      * TABCON(LAYER,NRX+J*NROW), J=0,3)
20300 FORMAT(' ', T4,4(E11.4,3X,E11.4,6X))
250 CONTINUE
2040 WRITE(10,2040)
      FORMAT(' ', I31('=',),/)
300 CONTINUE
      RETURN
      END
C -----
C *****
C FUNCTION CONDC(SUC)
C =====
C *****
C FUNCTION TO CALCULATE THE HYDRAULIC CONDUCTIVITY BELONGING =
C TO A SPECIFIED PRESSURE HEAD.
C =====
C *****
C INTEGER PEAT
C LOGICAL CRACK
C CHARACTER DESCR, HEAD
C REAL MEDIAN, KSAT, KSATEF
C COMMON/TABDAT/TABPRH(10,80), TABCON(10,80), NUMTAB(10), INTERP
C COMMON/RVTETA/RVTKO(10), RVTETA(10), RYTA(10), RVTN(10),
C * RYTHA(10), RYTHLM(10)
C COMMON/LINE/SUCLIN(10,4), CONLIN(10,4), ALIN(10,3), BLIN(10,3)
C COMMON/SOIL/THICK(10), THKLAY(10), GML, DESCR(10,15)
C COMMON/RISE/KSAT(10), PSIA(10), Z(15,54), H(54), FLUX(15),
C * METHOD, NFLUXS, NLAYER, LAYER, HEAD(80)
C COMMON/BLOEM/KSATEF(10), PSICOR(10), PSIEFF(10), PSID(10),
C * SLOPES(10), SLOPE(10), SLPOR(10), F(10), REDUC(10),
C * DIPER(10,15), SIZE(15), BULK(10), PEAT(10), HUMUS(10),
C * MEDIAN(10), NSIZES, CRACK(10)
C -----
C WHAT METHOD OF CONDUCTIVITY DESCRIPTION IS IN USE?
      GO TO (90,90,200,300,400),METHOD
C -----
90 IF(SUC.LT.PSIEFF(LAYER))GO TO 100
      CONDC=KSATEF(LAYER)
      GO TO 800
C -----
100 EFFECTIVE CRACKS?
      IF(CRACK(LAYER).AND.SUC.LT.-100)GO TO 120
C -----
110 NO CRACKS
      CONDC=KSATEF(LAYER)*((PSIEFF(LAYER)/SUC)**SLOPES(LAYER))
      GO TO 800
C -----
120 CRACKS.
      CONDC=KSATEF(LAYER)*((PSICOR(LAYER)/SUC)**SLPOR(LAYER))
      GO TO 800

```

```

C
C
C =====
C =
C = METHOD RIJTEMA
C =
C =====
C
C 200 IF(SUC.LT.RYTHA(LAYER))GO TO 220
C      CONDOC=RYTKO(LAYER)
C      GO TO 800
C
C 220 IF(SUC.LT.RYTHLM(LAYER))GO TO 240
C      CONDOC=RYTKO(LAYER)*EXP(RYTETA(LAYER))*(SUC-RYTHA(LAYER))
C      GO TO 800
C
C 240 CONDOC=RYTHA(LAYER)*((-1.0*SUC)**(-1.0*RYTN(LAYER)))
C      GO TO 800
C
C =====
C =
C = STRAIGHT LINES
C =
C =====
C
C 300 IF(SUC.LE.SUCLIN(LAYER,1))GO TO 310
C      CONDOC=CONLIN(LAYER,1)
C      GO TO 800
C
C 310 IF(SUC.LE.SUCLIN(LAYER,4))GO TO 340
C      IF(SUC.LE.SUCLIN(LAYER,2))GO TO 320
C      CONDOC=ALIN(LAYER,1)*((-1.0*SUC)**BLIN(LAYER,1))
C      GO TO 800
C
C 320 IF(SUC.GT.SUCLIN(LAYER,3))GO TO 330
C      CONDOC=ALIN(LAYER,2)*((-1.0*SUC)**BLIN(LAYER,2))
C      GO TO 800
C
C 330 CONDOC=ALIN(LAYER,3)*((-1.0*SUC)**BLIN(LAYER,3))
C      GO TO 800
C
C 340 CONDOC=0.0
C      GO TO 800
C
C =====
C =
C = TABEL
C =
C =====
C
C 400 IF(SUC.GT.TABPRH(LAYER,1))GO TO 420
C      CONDOC=TABCON(LAYER,1)
C      GO TO 800
C
C 420 NT=NUMTAB(LAYER)
C      IF(SUC.LT.TABPRH(LAYER,NT))GO TO 440
C      CONDOC=TABCON(LAYER,NT)
C      GO TO 800
C
C

```

```

38
C
C 440 DD 460 I=2,NT
C      IPOS=1
C      IF(SUC.LT.TABPRH(LAYER,IPOS))GO TO 480
C      CONTINUE
C
C 460
C
C 4010 WRITE(6,4010)SUC,TABCON(LAYER,NT)
C      FORMAT(' ???77 Conductivity belonging to pressure head ',
C      * E11.3,' was not found. ',E11.3,' cm/day assumed ???77').
C      CONDOC=TABCON(LAYER,NT)
C      GO TO 800
C
C 480 IP1=IPOS-1
C      IF(INTERP.EQ.2)GO TO 500
C
C -----
C      LINEAR INTERPOLATION
C      CONDOC=TABCON(LAYER,IP1)+(SUC-TABPRH(LAYER,IP1))*
C      * (TABCON(LAYER,IPOS)-TABCON(LAYER,IP1))/
C      * (TABPRH(LAYER,IPOS)-TABPRH(LAYER,IP1))
C      GO TO 800
C
C -----
C      LOGARITHMIC INTERPOLATION
C      PRHLOG=ALOG10(ABS(TABPRH(LAYER,IP1)))
C      PRHLOGU=ALOG10(ABS(TABPRH(LAYER,IPOS)))
C      PRHLOG=ALOG10(ABS(SUC))
C      CONLOG=ALOG10(TABCON(LAYER,IP1))
C      CONLOGU=ALOG10(TABCON(LAYER,IPOS))
C
C      CONLOG=CONLOG+(CONLOGU-CONLOG)*(PRHLOG-PRHLOG)
C      * / (PRHLOG-PRHLOGU)
C      CONDOC=10.0**CONLOG
C
C 800 RETURN
C      END
C
C *****
C
C SUBROUTINE TABINF
C =====
C =
C = SUBROUTINE TO MAKE A TABLE AND A PRINTPLOT OF PRESSURE
C = HEADS BELONGING TO SOME HEIGHTS ABOVE THE GROUNDWATER
C = LEVEL IN CASE OF INFILTRATION AND SOME SPECIFIED FLUX
C = DENSITIES.
C =
C =====
C
C INTEGER PEAT
C LOGICAL CRACK, JUMP, BOUND(50), TXT(50), FILL
C CHARACTER DESCR, HEAD, PLCHAR(15), REGE(120), DOT, TEXT*10
C REAL MEDIAN, KSAT, KSATEF
C DIMENSION OUT(15), IOLPOS(15)
C COMMON/GPONEG/NFLNS, NFLNE, NFLPS, NFLPE
C COMMON/SDIL/THICK(10), THKLAY(10), GWL, DESCR(10,15)
C COMMON/INFIL/SUCINF(15,51), ZINF(51), NZINF
C COMMON/RISE/KSAT(10), PSIA(10), Z(15,54), H(54), FLUX(15),
C * METHOD, NFLUXS, NLAYER, LAYER, HEAD(80)
C COMMON/BLOEM/KSATEF(10), PSICOR(10), PSIEFF(10), PSIQ(10),
C * SLOPES(10), SLOPE(10), SLPCOR(10), F(10), REDUC(10),
C * DIFFER(10,15), SIZE(15), BULK(10), PEAT(10), HUMUS(10),
C * MEDIAN(10), NSIZES, CRACK(10)
C

```


[illegible]

43

```

END IF
BOUND(IGNEW)=.TRUE.
ITXT=(IGNEW+IGOLD)/2
TXT(ITXT)=.TRUE.
IGOLD=IGNEW
ILAY=ILAY+1
IF (ILAY.GT.NLAYER) GOTO 56

END IF
CONTINUE
51 ITXT=(50+IGOLD)/2
56 TXT(ITXT)=.TRUE.

C ----
C BUILDING THE LINES
57 ITEL=0
DO 80 IZ=IGML,ISTEP,-1*ISTEP
ITEL=ITEL+1
RZ=IZ*1.0
DO 52 I=1,100
REGE(I)=.
CONTINUE
FLX=.

C ----
C INSERTING BOUNDARIES AND TEXT
IF (BOUND(ITEL)) THEN
DO 53 I=1,100,2
REGE(I)=DOT
CONTINUE
END IF
IF (TXT(ITEL)) THEN
DO 54 I=1,15
REGE(I+2)=DESCR(IL,I)
CONTINUE
IL=IL+1
END IF

C ----
C DO 70 IFLUX=NFLPS,NFLPE
DO 55 ISUC=1,53
IF (Z(IFLUX,ISUC).GT.RZ) GOTO 60
CONTINUE
NOT FOUND
GOTO 70
60 POS=(RZ-Z(IFLUX,ISUC-1))/(Z(IFLUX,ISUC)-Z(IFLUX,ISUC-1))
*(H(ISUC)-H(ISUC-1))+H(ISUC-1)
IF (ABS(POS).LE.1E-6) GOTO 70
IPDS=INT(ALOG10(ABS(POS))*20+0.5)

C ----
C FILLING LARGE GAPS
IF (IOLPOS(IFLUX)-IPDS.GT.2.AND..NOT.EERSTE(IFLUX)) THEN
DO 63 I=IPDS+2,IOLPOS(IFLUX)-2,2
IF (REGE(I).EQ.' ' .OR. REGE(I).EQ.DOT) THEN
REGE(I)=PLCHAR(IFLUX)
ELSE
REGE(I)=**
END IF
CONTINUE
IOLPOS(IFLUX)=I
END IF

C ----
C INSERTING PLOTCHARACTERS
IF (REGE(IPDS).EQ.' ' .OR. REGE(IPDS).EQ.DOT) THEN
REGE(IPDS)=PLCHAR(IFLUX)

```

44

```

ELSE
REGE(IPDS)=**
END IF
IOLPOS(IFLUX)=IPDS
IF (EERSTE(IFLUX)) THEN
IF (IZ.EQ.IGML) THEN
TOP=.TRUE.
WRITE(6,13) (F5,3)',FLUX(IFLUX)
TOPFLX(6,13)=. cm/day.
ITOPOS=IPDS+3
ELSE
DO 65 I=IPDS+2,100,2
REGE(I)=PLCHAR(IFLUX)
CONTINUE
WRITE(FLX,(F5,3)')FLUX(IFLUX)
FLX(6,13)=. cm/day.
END IF
EERSTE(IFLUX)=.FALSE.
END IF
CONTINUE
IF (TOP.AND.12.EQ.IGML) THEN
DO 75 I=ITOPOS,ITOPOS+12
REGE(I)=TOPFLX(I-ITOPOS+1:I-ITOPOS+1)
CONTINUE
WRITE(10,1090)RZ,REGE
FORMAT(F6.0,T9,' ',100A1)
ELSE
WRITE(10,1100)RZ,REGE,FLX
FORMAT(F6.0,T9,' ',100A1,3X,A13)
END IF
CONTINUE
WRITE(10,1110)(IE0,IE1,IE2,IE3,IE4,IE5)
FORMAT(T9,5(' ',19('-')),' '/T6,5(E6,IE1,14X),E6,IE1,
//T50,';PRESSURE HEAD1 (cm)')
RETURN
END

```

45

```

65
70
75
1090
1100
80
1110
*
END

```