# Standardized ileal digestible lysine requirement for broilers

J.W. Spek

Wageningen Livestock Research

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Wageningen Livestock Research P.O. Box 338 6700 AH Wageningen The Netherlands

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### Preface

In 2017 a new Table has been introduced called; Table 'Standardized ileal digestibility of amino acids in feedstuffs for poultry' and has been described in the CVB Documentation report nr. 61. As a feed evaluation system has two pillars – the supply of nutrients by the diet on the one hand and the requirement for these nutrients by the animals on the other hand (both expressed in the same units) – it was also necessary to also update and express the amino acid requirements on a standardized ileal digestibility (SID) basis.

Therefore a large meta-analysis dataset was constructed from studies in which amino acid requirements in broilers were estimated. The SID amino acid concentrations of the diets used in these studies were recalculated based on the new CVB SID amino acid Table presented in CVB documentation report nr. 61 and the requirements for SID lysine were subsequently estimated. The results of this meta-analysis for standardized ileal digestible lysine (SID-LYS) are presented in the present CVB Documentation report. Compared to the former CVB apparent faecal digestible LYS recommendation for broilers described in CVB Documentation report nr. 18 and published in 1996 the present established SID-LYS amino acid recommendations for broilers are:

- 1. Based on a substantial larger dataset of requirement studies
- 2. Based on studies with modern broiler types in the period 1990 2017
- 3. Based on standardized ileal digestible amino acid values in feedstuffs instead of apparent faecal digestible amino acid values.

The in this report estimated requirement of SID-LYS will be incorporated in the Dutch CVB Tabellenboek Veevoeding Pluimvee 2018 and in the English version CVB Table Poultry Nutrition 2018.

This study was guided and assessed by the Technical Committee of CVB

Wageningen, June 2018

J.W. Spek

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G. van Duinkerken	Wageningen Livestock Research, Dept. Animal Nutrition, Wageningen
J.W. Spek	Wageningen Livestock Research, Dept. Animal Nutrition, Wageningen

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## Abbreviations

LYSLysineMEMetabolic energyMEbrMetabolic energy for broilersMEpoMetabolic energy for poultryMETMethionineM+CMethionine plus CysteineNNumberR²Coefficient of determinationReqRequirementSIDStandardized ileal tract digestibleStd. Dev.Standard deviationStd. Err.Standard errorTHRThreonineTRPTryptophanVALValine
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#### 1 Introduction

In 2012 a large meta-analysis was carried out by Veldkamp and others in order to determine the dietary requirements for standardized ileal tract digestible (SID) amino acids (AA) for broilers. This study resulted in a report published by Veldkamp et al. (2016). Before the start of this meta-analysis another large meta-analysis was carried out in order to determine the SID-AA levels for the various feed ingredients. This meta-analysis resulted in a CVB table with SID-AA concentrations for the various feed ingredients and this Table was used by Veldkamp et al. (2016) in order to recalculate the dietary SID-AA levels for the individual AA titration studies in order to estimate AA requirements. However, in 2017 this CVB Table has been updated with new data published in the years between 2012 and 2017 as there were questions about the SID cysteine digestibility value for sovbean meal. As a result, not only the SID-AA values for soybean meal have been updated but also for other feedstuffs. As a consequence it was necessary to recalculate all the diets used in the AA titration studies that Veldkamp et al. (2016) used to determine AA-requirements. In this study the results of estimated dietary SID lysine (SID-LYS: %) requirements based on the new Table values are presented. Furthermore, the dataset used by Veldkamp et al. has been extended with new studies that were not included in the study of Veldkamp et al.. This resulted in a dataset more than twice as large as the dataset used by Veldkamp. Furthermore, multiple models for estimation of SID-LYS requirements have been used and compared with each other in this study such as the exponential model as described and used by Veldkamp et al. (2016), a linear broken-line model and a quadratic broken-line model.

#### 2 Materials and Methods

Lysine titration studies were selected from literature (1990 – 2017) in which only the dietary LYS content was varied by means of addition of graded levels of dietary synthetic LYS. Furthermore, only those titration studies were selected in which non-test apparent digestible LYS levels of the basal diet (diet with the lowest LYS content) were less than 10% of the recommended CVB (2012) levels and where dietary digestible LYS levels of the basal diets where at least 20% below the recommended CVB (2012) level. Furthermore, performance characteristics such as body weight gain (BWG: g/d) and feed conversion ratio (FCR; g feed : g BWG) had to be recorded and information with respect to dietary composition, sex, age of the broilers and duration of the experiment had to be provided in the studies.

Requirements were estimated using three models, an exponential model, a linear broken-line model and a quadratic broken-line model.

The exponential model is as follows:

 $Y = a + b * (1 - e^{(-C * dx)})$ 

Where: Y = response value of BWG or FCR;

- a = estimated basal level (for dx=0) of the amino acid LYS;
- b<sub>i</sub> = difference between basal level and estimated asymptotic level for BWG or FCR response;
- C = rate parameter (for speed of curving);
- dx = difference in LYS concentration compared to the basal (non-supplemented) diet;

For each individual experiment the estimated requirement (Req) for the amino acid of interest was calculated as the amino acid concentration where 95% of the response (BWG and FCR) between intercept and asymptotic value was reached. The estimated amino acid requirement was calculated by the following mathematical equation:

 $\operatorname{Req} = \frac{\ln(0.05)}{-c} + \operatorname{MIN}(Xi)$ 

Where:

The linear broken-line model is as follows:

If (SID-LYS (g/kg) < R) then BWG or FCR = L + U × (R – SID-LYS); Else BWG or FCR = L + U × 0; Where: L = plateau value for BWG or FCR R = break-point value for SID-LYS (g/kg)

U = slope value, representing the increase in BWG or decrease in FCR per unit increase in dietary SID-LYS.

The quadratic broken-line model is as follows:

If (SID-LYS (g/kg) < R) then BWG or FCR = L + U × (R – SID-LYS)<sup>2</sup>; Else BWG or FCR = L + U × 0; Where: L = plateau value for BWG or FCR R = break-point value for SID-LYS (g/kg) U = slope value, representing the increase in BWG or decrease in FCR per unit increase in dietary SID-LYS.

For a number of titration studies a clear decrease in feed intake was observed after an initial increase in feed intake at increased levels of dietary LYS suggesting that the increase in dietary LYS after a certain optimum level resulted in a negative feedback on feed intake. This decrease in feed intake at increased LYS levels after a certain optimum LYS level for feed intake and performance has been achieved may affect the estimation of the optimal SID-LYS level. Therefore, SID-LYS requirements were also estimated after excluding the observations with these lower feed intakes. A lower feed intake was considered 'lower' as the feed intake of the two preceding dietary LYS levels were higher than the highest LYS level. However, in some cases this resulted in estimated 'extrapolated' SID-LYS requirements that were higher than the highest SID-LYS level. Therefore it was decided to only estimate SID-LYS requirements based on all the data.

Via the PROC MIXED procedure and the PROC NLMIXED procedures of SAS estimated SID-LYS requirements for BWG and FCR were regressed against factors such as age, sex, the dietary factors CP, ME and CP : ME ratio with study effect included as a random factor. Furthermore, the estimated SID-LYS requirement levels were also used to calculate ratios of other non-test SID-AA with the estimated requirement SID-LYS levels and it was checked whether some of the non-test SID AA were negatively affecting the estimated SID-LYS levels.

#### 3 Results and Discussion

In Table 1 a summary of the total dataset is given. The dataset consisted of 19 studies with in total 54 titration trials and 317 observations. In all 19 studies maize was the principal feed component.

	Ν	Mean	Std.	Minimum	Maximum
			Dev.		
MEpo Recalculated (kcal/kg)	317	3034	111.9	2635	3152
ME Publication (kcal/kg)	317	3168	128.8	2700	3370
CP Recalculated (%)	317	20.6	1.45	17.8	23.2
CP Publication (%)	317	20.4	1.55	17.2	23.6
Year	317	2006	4.3	1999	2012
Starting age (d)	317	11	9.5	1	35
Duration (d)	317	16	4.3	6	25
finishing age (d)	317	27	10.9	7	49
Mean age (d)	317	19	10.0	4	42
BWG (g/d)	317	52.7	30.52	15.8	189.3
FCR (g feed: g growth)	317	1.605	0.2425	1.029	2.644

In Appendix A for each titration trial the relationship between dietary SID-LYS supply and FCR and between dietary SID-LYS and BWG is presented graphically together with the estimated SID-LYS requirements for the exponential, linear broken-line and quadratic broken-line models. A visual analysis of these graphs show that in most cases the estimated SID-LYS requirements using the linear broken-line model is lower than the SID-LYS concentration at which maximum BWG or minimum FCR is observed and also that in a number of cases the estimated SID-LYS requirements using the exponential model is substantially overestimating the requirement for SID-LYS. Furthermore, the root of the squared difference between the estimated SID-LYS requirements and the observed SID-LYS requirements at which minimum FCR was observed or maximum BWG was observed was smallest for the quadratic broken-line model (the average squared root difference between estimated SID-LYS requirements and the observed SID-LYS requirements for FCR was an absolute 0.0677% for the quadratic broken-line model compared to absolute values of 0.124% and 0.113% for the exponential and linear broken-line models, respectively). Therefore it was decided to use the estimated SID-LYS requirements based on the quadratic broken-line model as the basis for deriving SID-LYS recommendations for BWG and FCR. In Appendix B the estimated quadratic broken-line model parameters for each titration trial is given.

For a number of titration trials (4 titration trials for FCR and 5 titration trials for BWG) it was not possible to estimate reliable or unique SID-LYS requirements using the quadratic brokenline procedure. Furthermore, there was only one study in which female and male chicken were mixed and it was observed that this was also the only study that resulted in estimated SID-LYS requirements for FCR and BWG that were outliers compared to the other observations. The results of this study with mixed sex therefore were not included in the further work of establishing relationships between estimated SID-LYS requirements for FCR/BWG and other factors such as age and sex of the broilers.

In Table 2 the dietary non-test SID-AA : estimated SID-LYS requirements ratios using the quadratic broken-line procedure for FCR and BWG are given together with the recommended CVB apparent fecal digestible (AFD) ratios. Results in Table 2 show that on average the estimated SID-LYS requirement estimates could not have negatively be impacted with limiting non-test AA levels although in some trials some non-test AA levels could have had a negative impact on estimated SID-LYS levels as a comparison between

recommended CVB ratios and minimal ratios for both FCR and BWG observed in this study show. However, a visual inspection of graphs in which the various ratios were plotted against estimated SID-LYS requirements did not show deviating SID-LYS requirement estimates at suboptimal low ratios.

**Table 2**. Dietary non-test SID-AA : estimated SID-LYS requirement ratios using the quadratic broken-line procedure for FCR and BWG and compared to the recommended (Rec.) CVB apparent faecal digestible (AFD) ratios.

	Rec.		FCR			BWG			
Ratio	CVB AFD ratio	Mean	Std. Dev.	Min	Max	Mean	Std. Dev.	Min	Max
MET: LYS	38	53	10.3	37	79	55	10.8	36	81
M+C:LYS	73	76	11.8	52	106	79	11.4	56	109
THR:LYS	65	67	6.6	57	84	70	7.7	60	88
TRP:YS	16	17	2.2	12	22	18	2.1	13	23
ILE:LYS	66	72	6.4	57	84	75	6.3	59	88
ARG:LYS	105	112	9.8	93	132	117	9.3	100	134
VAL:LYS	80	82	6.6	66	96	86	7.0	71	101

#### 3.1 Estimation of SID-LYS requirements for maximum BWG

It appeared that mean age was the factor that could explain most variation in estimated SID-LYS requirements for maximum BWG (Table 3). Factors such as sex, protein level and ME level were not significant when added as covariables next to mean age and mean age squared.

**Table 3**. Regression formula to estimate the SID-LYS requirement for maximum BWG (% in diet).

F.	Intercept	Mean age (d)	(Mean age (d))^2	R <sup>2</sup>
1	1.050±0.0196			0.000
2	1.153±0.0286	-0.00542±0.001284		0.324
3	1.261±0.0469	-0.01919±0.005086	0.000316±0.000115	0.438

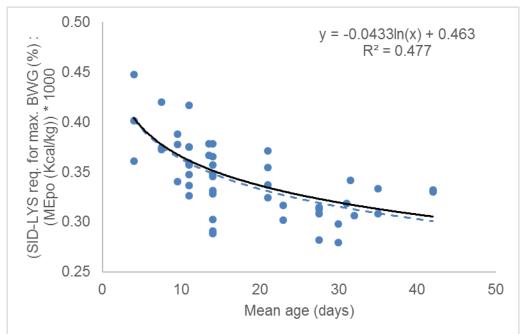
Although F.3 explains more variation in SID-LYS requirement for maximum BWG compared to F.2 (Table 3), the result is that after an initial decrease in SID-LYS requirement at increasing age the predicted SID-LYS requirement increases again as age increases. This is not logical from a physiological point of view and therefore it was chosen to fit a <u>natural</u> logarithmic relationship. This resulted in the formula presented in F.4:

F.4: SID-LYS req. for max BWG (% in diet) =  $1.280\pm0.03029 - 0.1394\pm0.04184 \times \log(\text{mean} \text{ age (d}))$ ; R<sup>2</sup> = 0.395.

Although dietary ME was not significant in explaining variation in estimated SID-LYS for BWG when it was added as a covariable to the model next to the factors mean age and mean age squared, when expressing the estimated SID-LYS requirements for maximum BWG relative to dietary ME content it resulted in a formula (F. 5) that explained substantial more variation compared to formula F.4:

F.5: SID-LYS req. for max BWG ((% est. SID LYS in diet for max. BWG : MEpo (Kcal))\*1000) =  $0.462\pm0.01971 - 0.0419\pm0.00696 \times \log(\text{mean age (d)}); R^2 = 0.477.$ 

Also it is from a physiological point of view logical to take the dietary ME content into consideration as an increase in dietary ME content enables a higher growth and protein retention per unit of feed consumed and thereby also necessitates a higher SID-LYS requirement per unit of feed consumed. In Figure 1 the relationship between mean age (days) and the SID-LYS req. for max BWG ((% SID LYS in diet : MEpo (Kcal/kg))\*1000) ratio is shown.



**Figure 1**. Relationship between mean age and the SID-LYS req. for max BWG ((% SID LYS in diet : MEpo (Kcal/kg))\*1000). The solid line represents formula F.5 and takes into account a study effect whereas the dashed line represents the formula shown in the Figure and does not take into account a study effect.

It is also possible to regress the model estimated SID-LYS requirements for maximum BWG against the model estimated plateau values of FCR and this type of regression formula might be useful in order to determine SID-LYS requirements for maximum BWG for deviating conditions such as birds with extremely low or high FCR. This resulted in the following regression formula for BWG:

F.6. SID-LYS req. for max BWG ((% est. SID LYS in diet for max. BWG : MEpo (Kcal/kg))\*1000) =  $0.560\pm0.0316 - 0.141\pm0.0206 \times FCR$  (g feed : g BWG); R<sup>2</sup> = 0.564

#### 3.2 Estimation of SID-LYS requirements for minimum FCR

In contrast to the estimation of the SID-LYS req. for maximum BWG less variation in SID-LYS req. for minimum FCR could be explained. It appeared that mean age was the factor that could explain most variation in SID-LYS requirement for minimum FCR (Table 4). Contrary to BWG there was no significant quadratic effect of mean age on SID-LYS req. for minimum FCR. Factors such as sex, protein level and ME level were not significant when added as covariables next to mean age and mean age squared.

**Table 4**. Regression formula to estimate the SID-LYS requirement for minimal FCR.

F.	Intercept	Mean age (d)	R <sup>2</sup>
7	1.083±0.0211		0.000
8	1.167±0.0338	-0.00414±0.001461	0.203

Although dietary energy was not significant in explaining variation in estimated SID-LYS for BWG when it was added as a covariable to the model next to the factor mean age, when expressing the estimated SID-LYS requirements for maximum BWG relative to dietary ME content it resulted in a formula (F.9) that explained more variation compared to formula F.8:

F.9: SID-LYS req. for min. FCR ((% est. SID LYS in diet for min. FCR : MEpo (Kcal))\*1000) =  $0.467\pm0.0257 - 0.0378\pm0.00907 \times \log(\text{mean age (d)}); R^2 = 0.287.$ 

It is also possible to regress the model estimated SID-LYS requirements for minimum FCR against the model estimated plateau value of FCR and this type of regression formula might be useful for extreme conditions such as birds with extremely low or high FCR. This resulted in the following regression formula for FCR:

F.10. SID-LYS req. for min. FCR ((% est. SID LYS in diet for min. FCR : MEpo  $(Kcal/kg))^{*1000} = 0.568 \pm 0.0349 - 0.135 \pm 0.0225 \times FCR (g feed : g BWG); R^{2} = 0.432$ .

#### 4 Conclusions

Based on the results of this study it is concluded that formula F.5 is most suited to predict SID-LYS recommendations for maximum BWG and formula F.9 to predict SID-LYS recommendations for minimum FCR. In Table 5 the SID-LYS requirements for BWG and FCR at the various growing periods are presented. These MEpo values are average MEpo values based on 2017 data from three Dutch compound feed companies.

Table 5. Estimated requirement levels for SID-LYS (g/kg) for BWG and FCR based on	
formula F.5 for BWG and F.9 for FCR.	

Growing period	MEpo (Kcal/kg)*	MEbr	SID-LYS (BWG)	SID-LYS (FCR)
		(Kcal/kg)**		
Week 1	2920	2840	12.0	12.3
Week 2	3020	2920	11.0	11.4
Weeks 3-4	3040	2940	10.2	10.7
Weeks >4	3100	3000	9.7	10.3

\*MEpo values are average MEpo values based on 2017 data from three Dutch compound feed companies.

\*MEbr was derived from MEpo by assuming a diet containing 40% wheat (with a STAam content of 58%), 20% maize, 30% soybean meal for all growing periods and inclusion of pure fat of, 2, 5, 5, and 5 percent for, respectively, the growing periods week 1, week 2, week 3 – 4 and week > 4.

#### List of studies included in the meta-analysis

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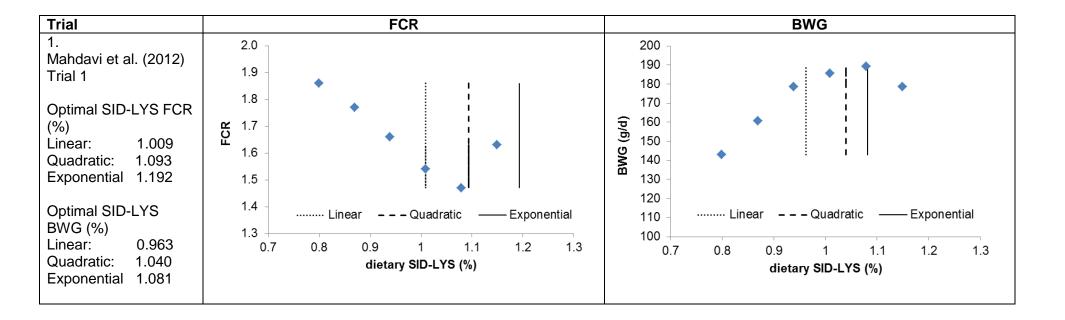
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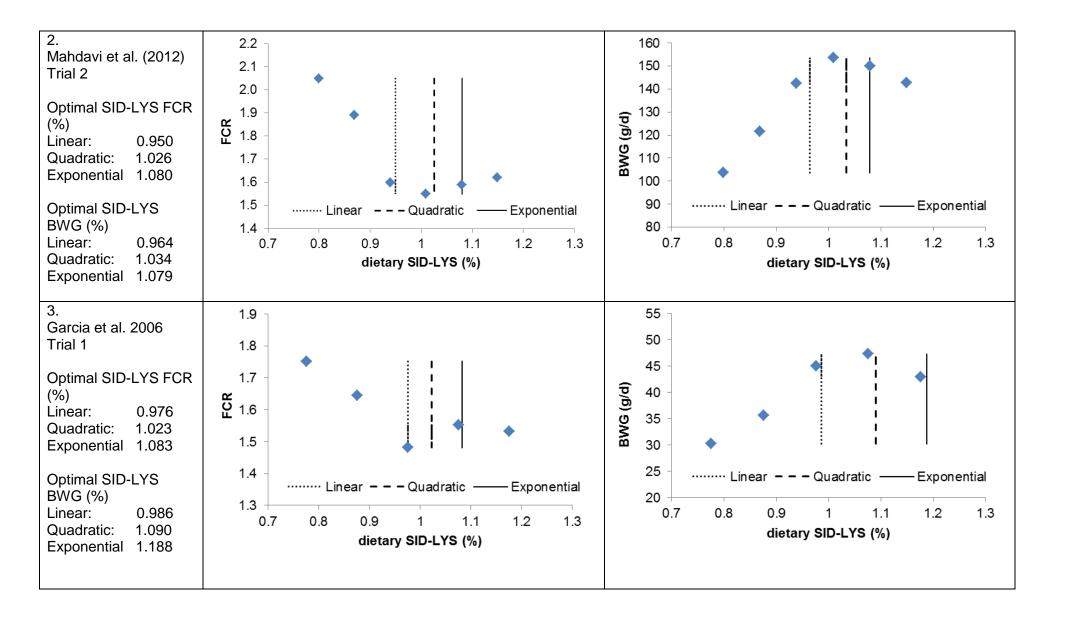
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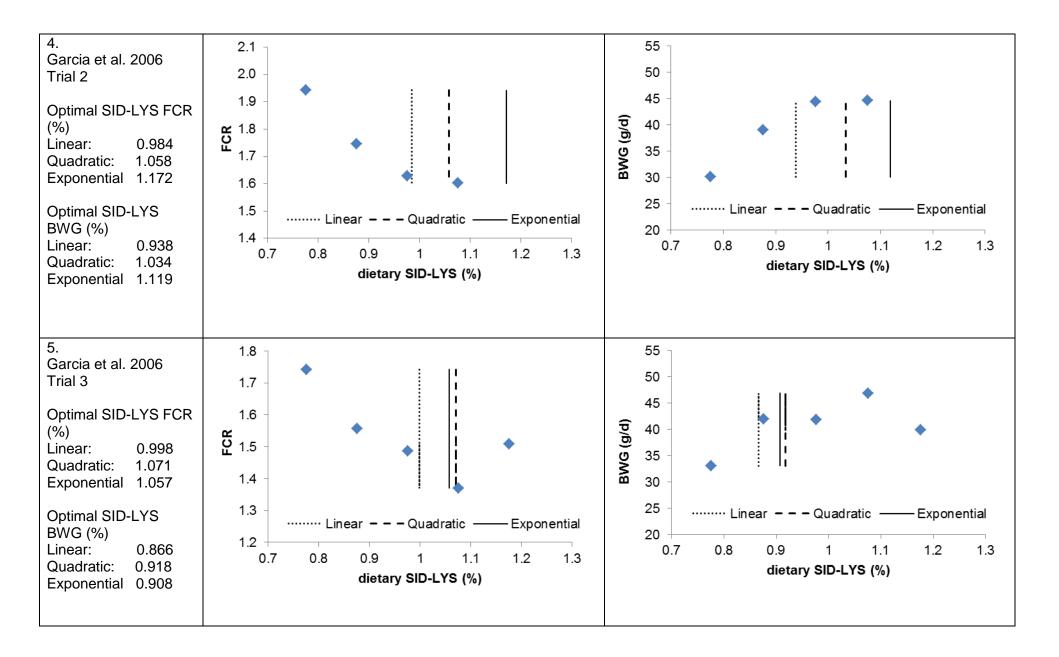
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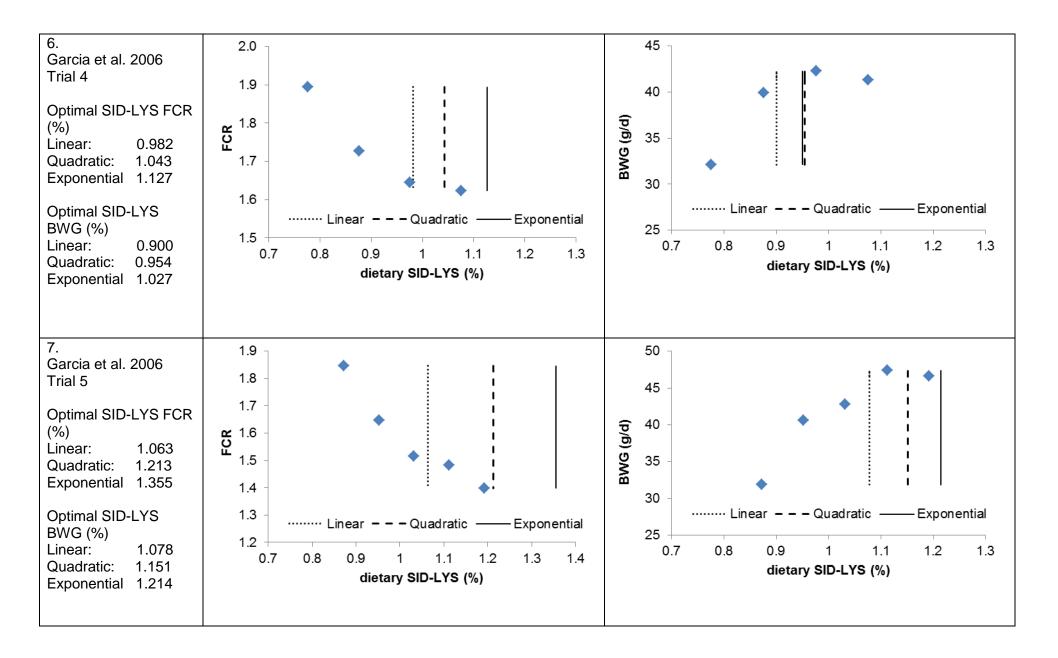
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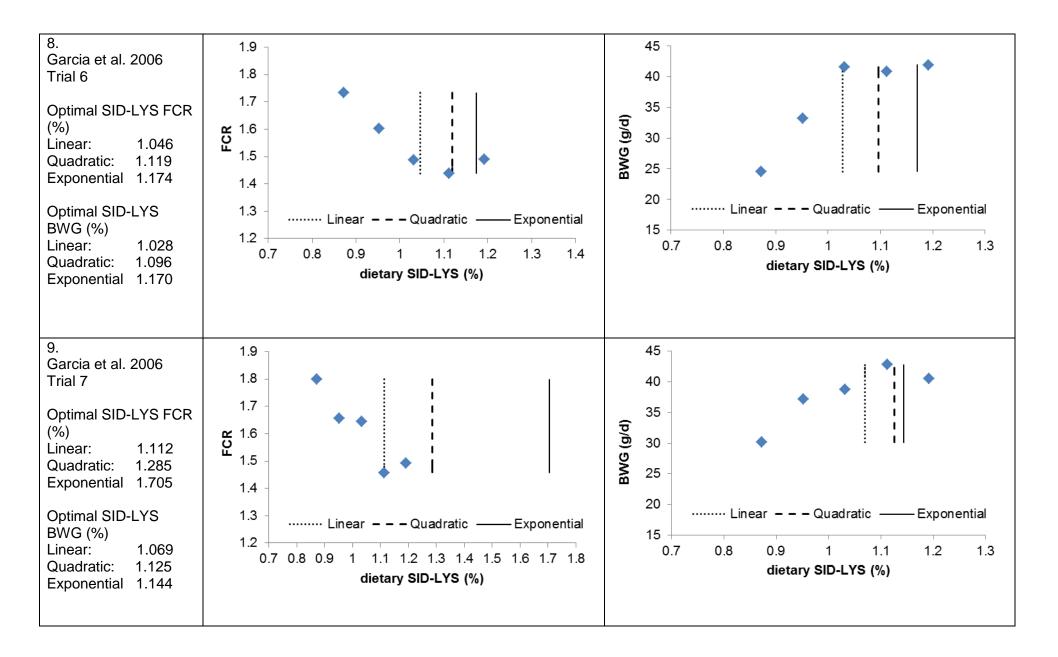
Appendix A. Relationship between dietary SID-LYS supply and performance parameters FCR and BWG for the various titration trials including the estimated SID-LYS requirements based on the linear broken-line model, the quadratic broken-line model and the exponential model.

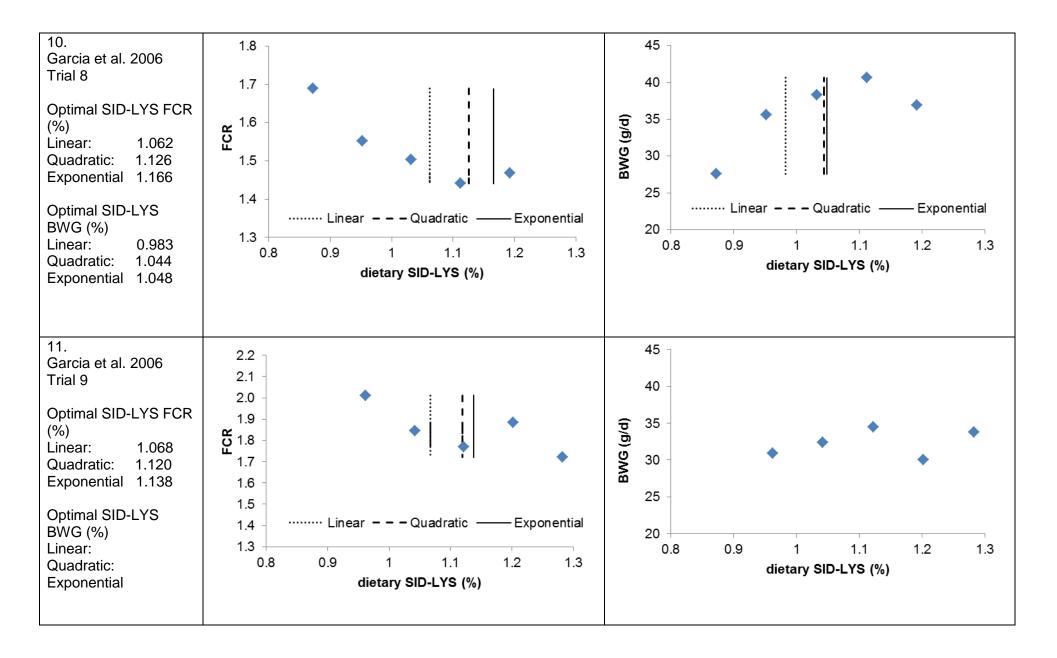


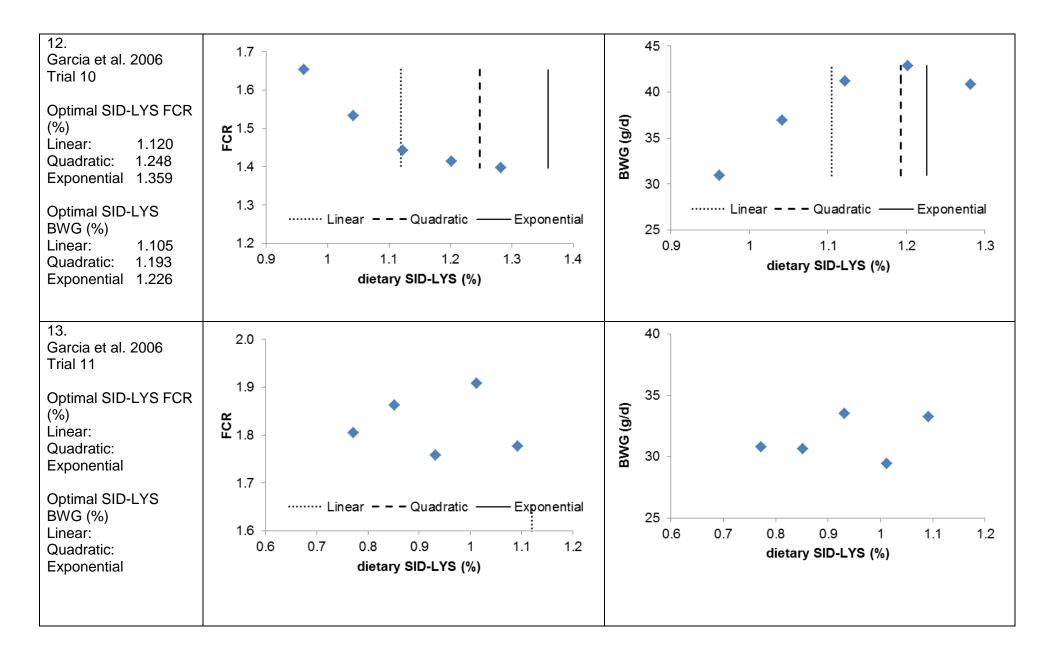


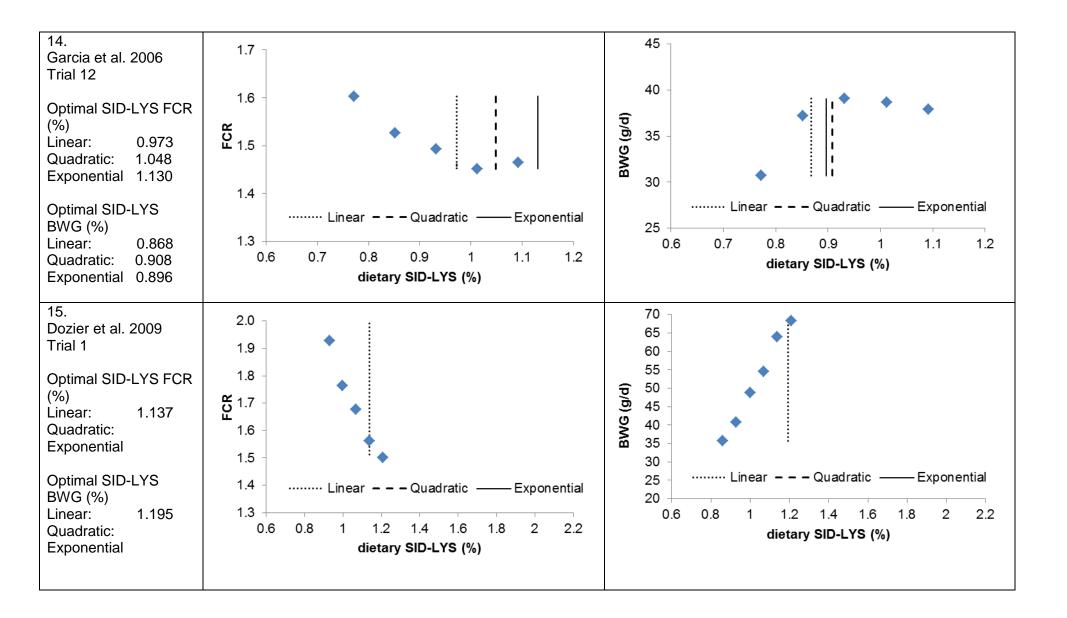


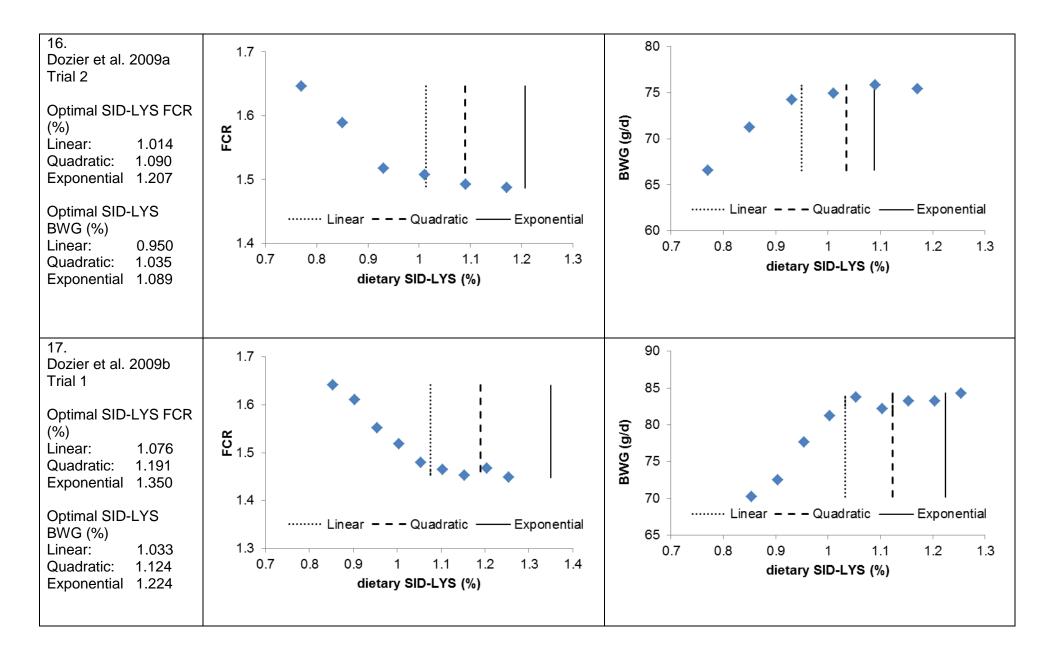


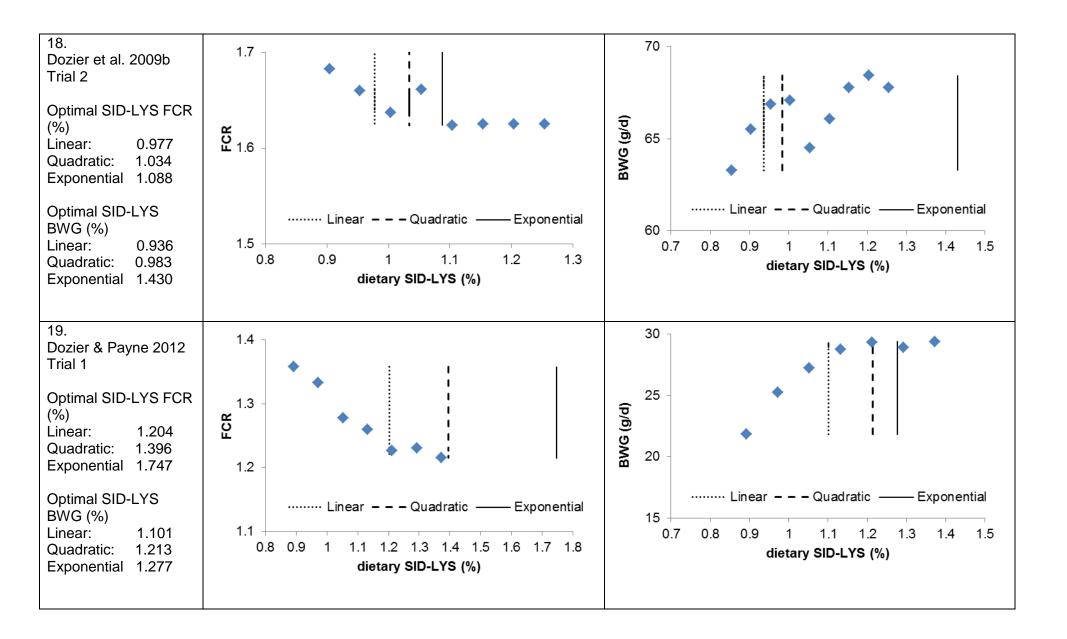


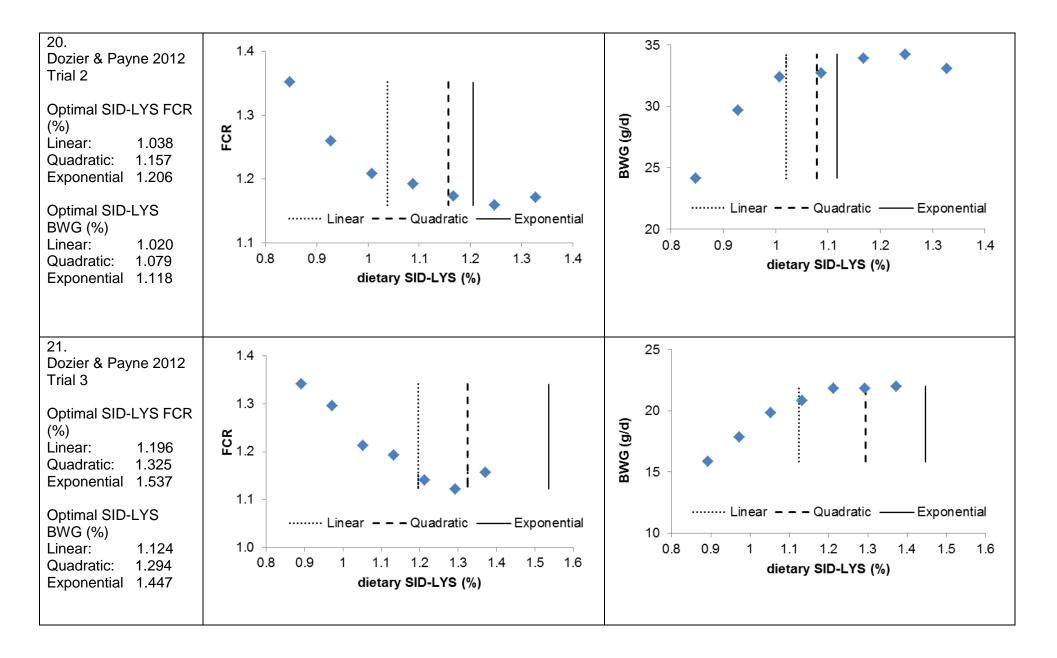


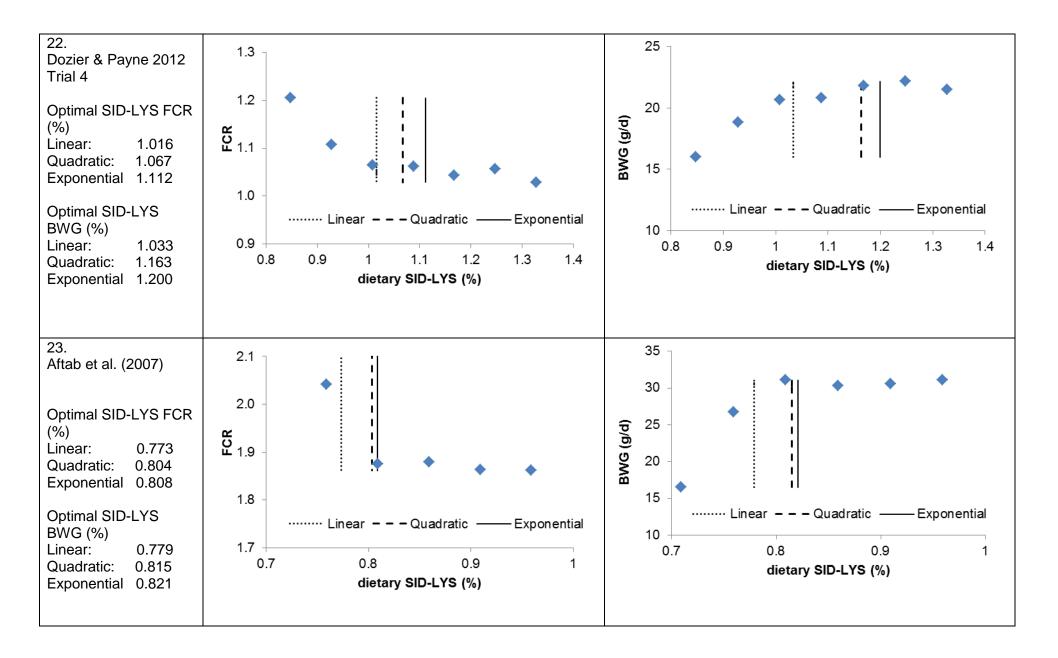


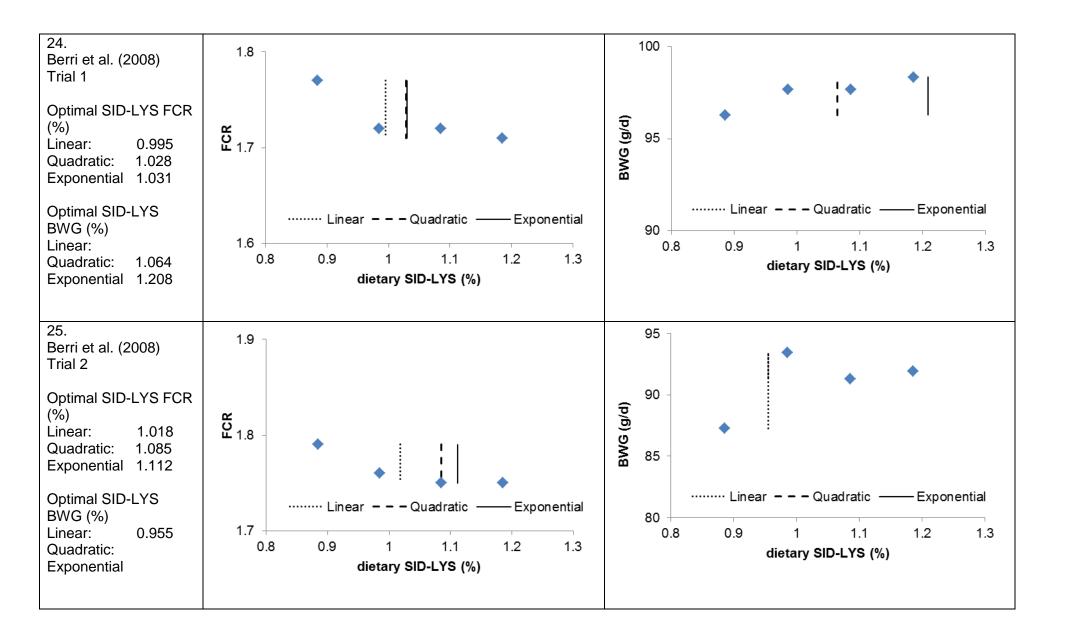


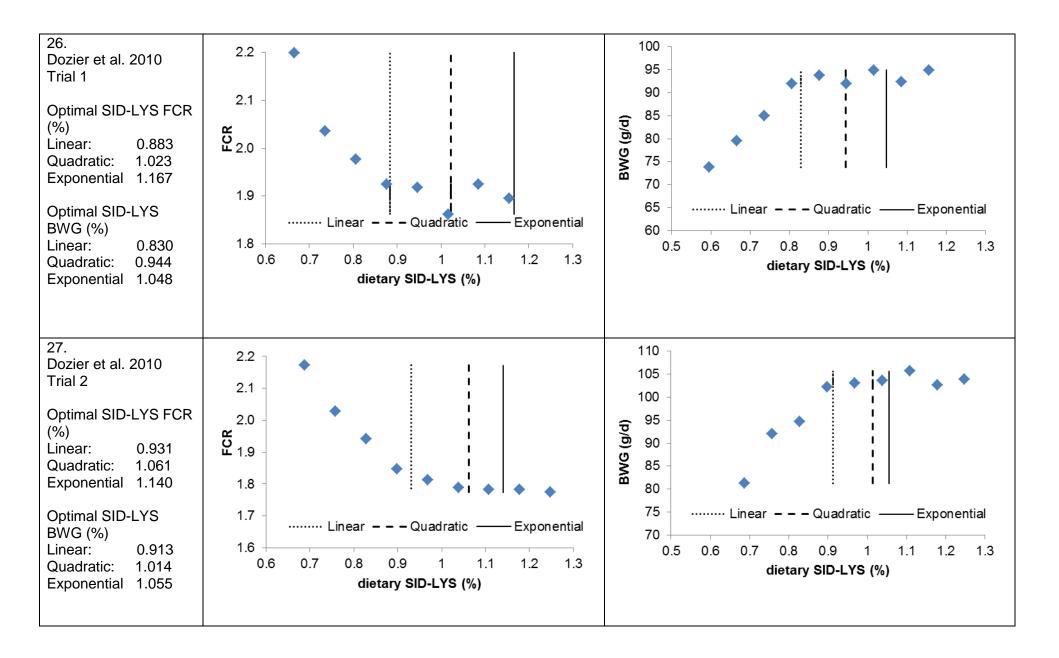


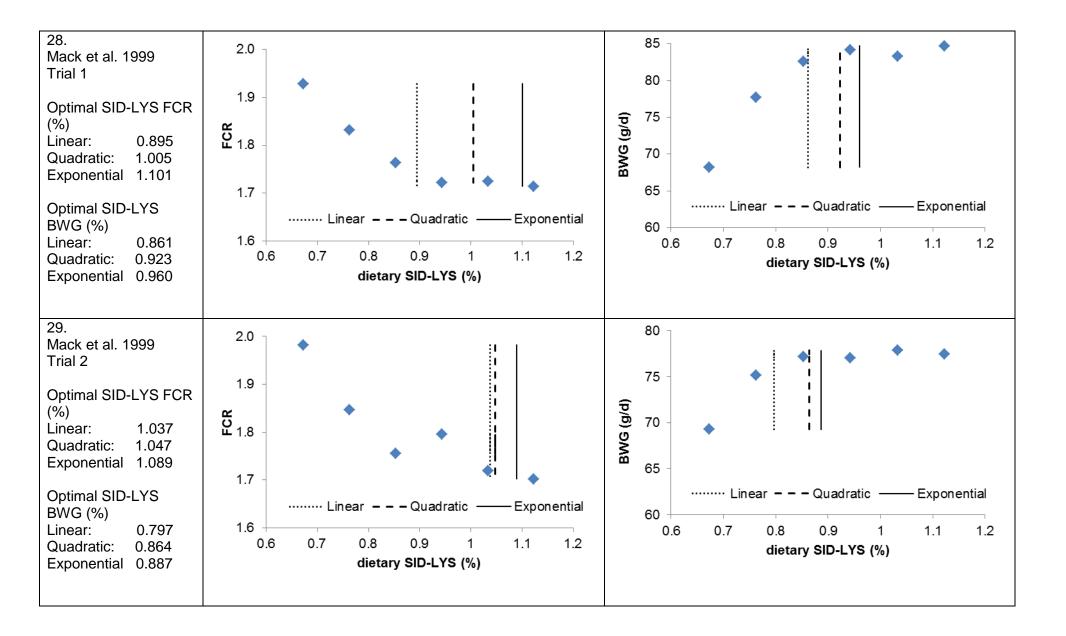


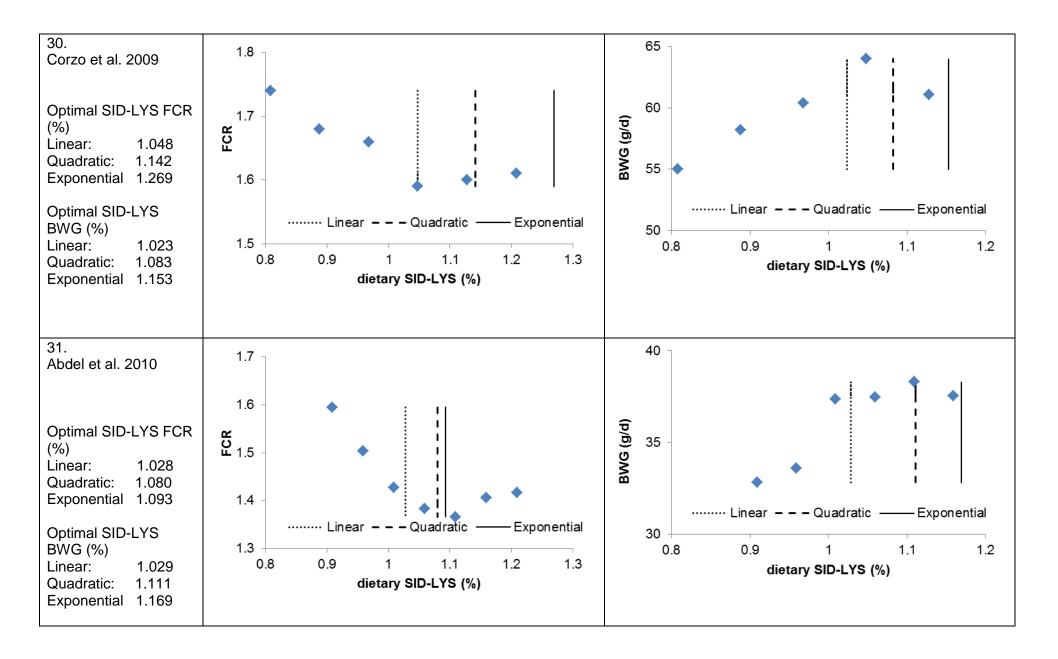


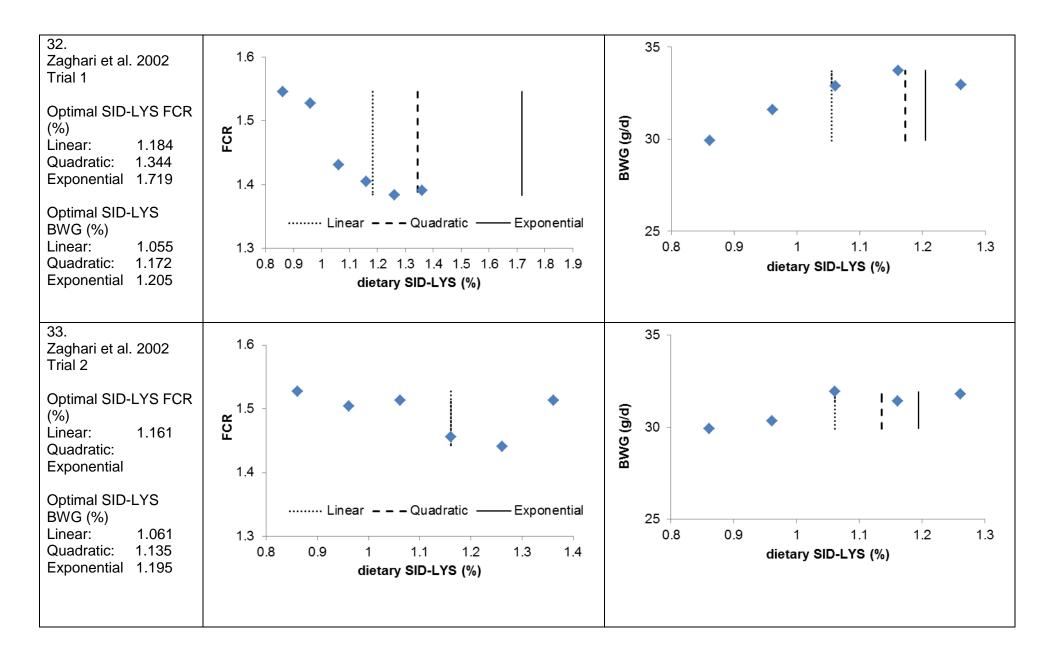


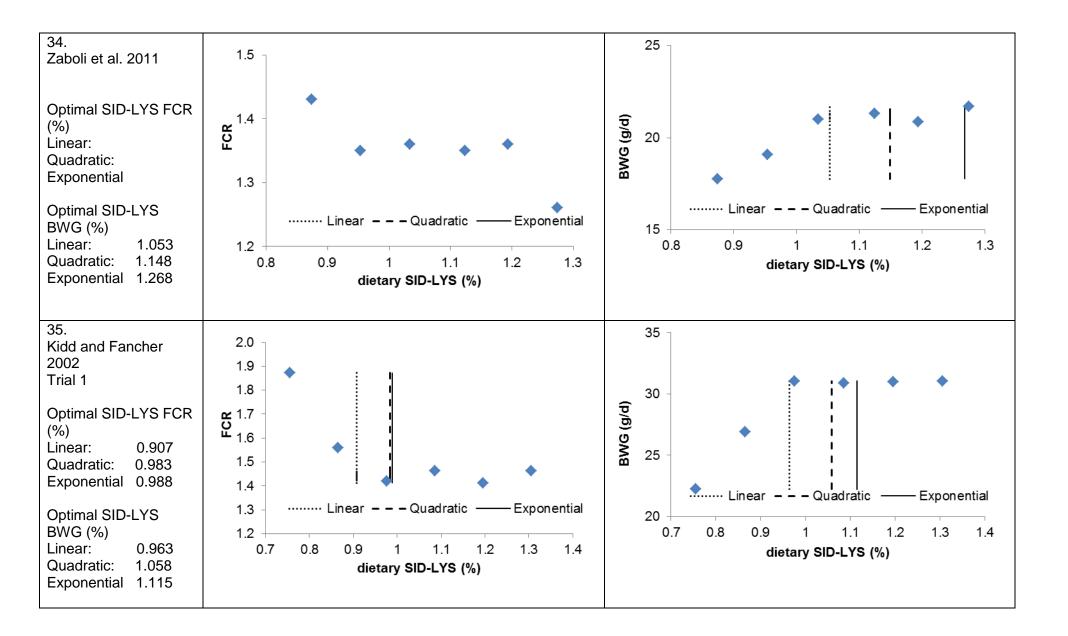


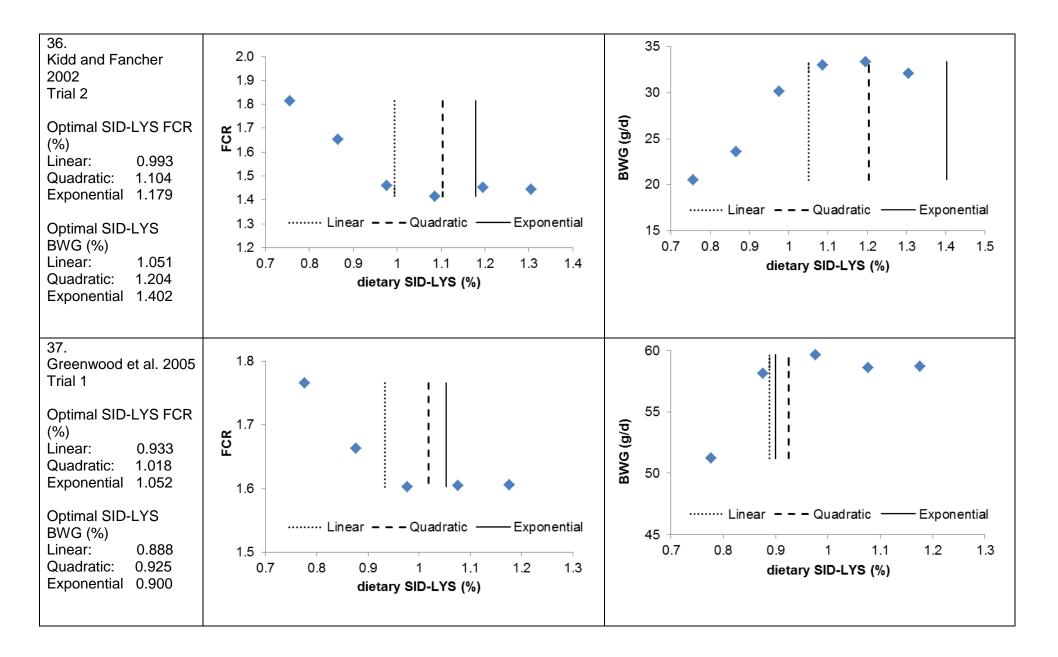


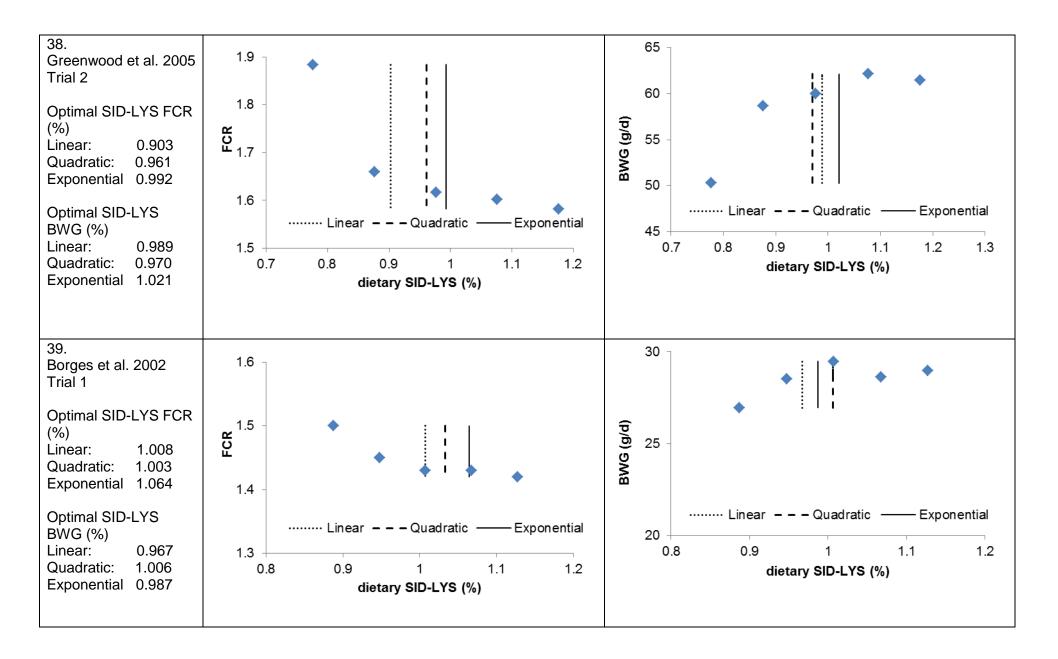


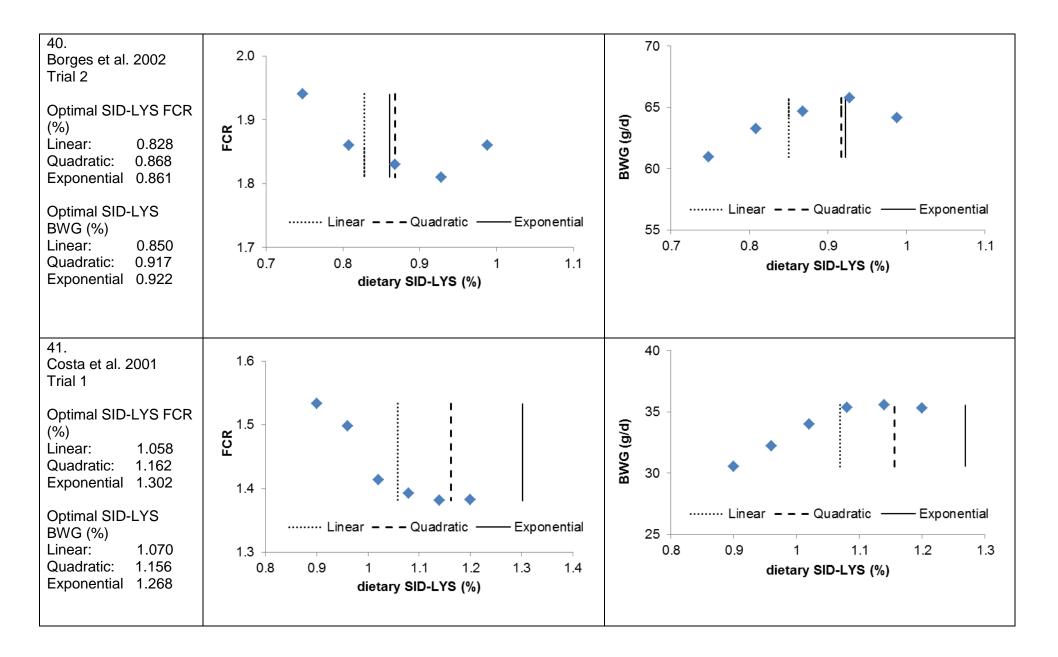


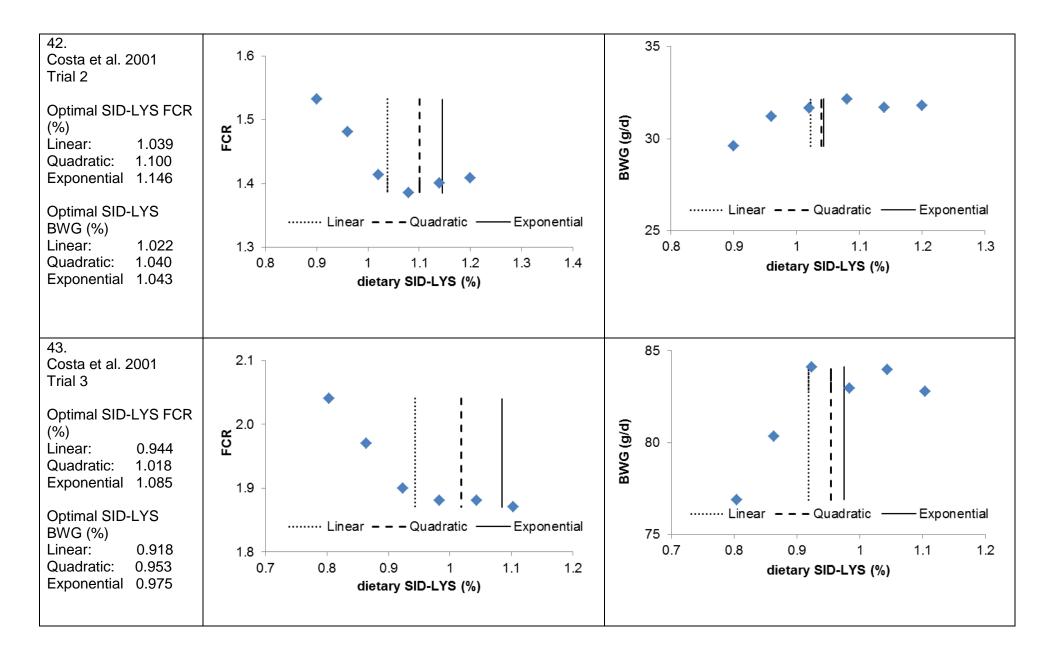


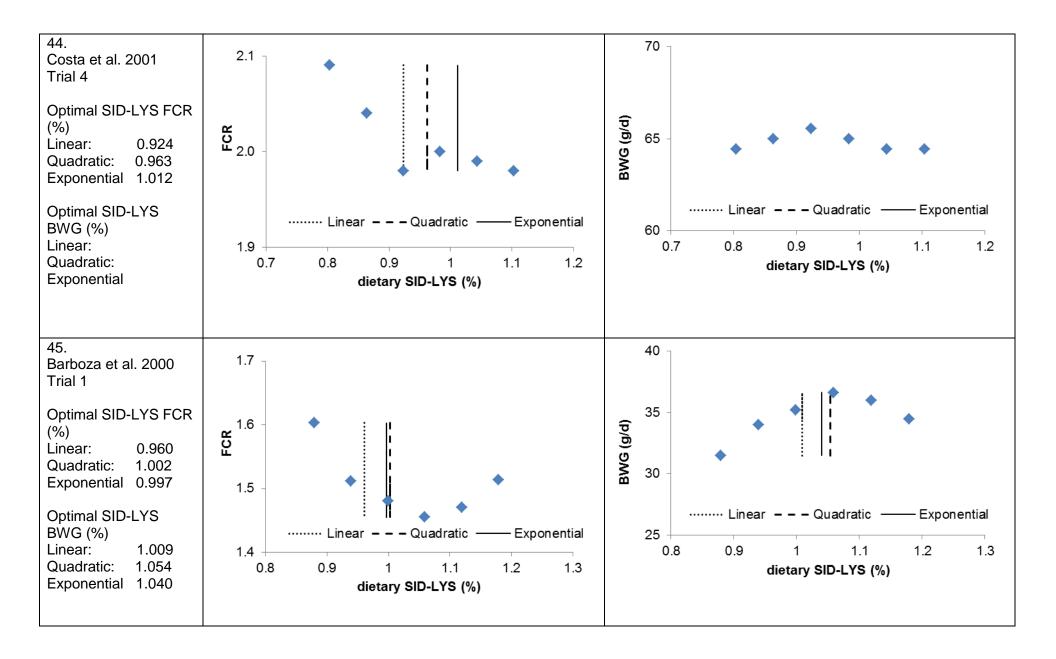


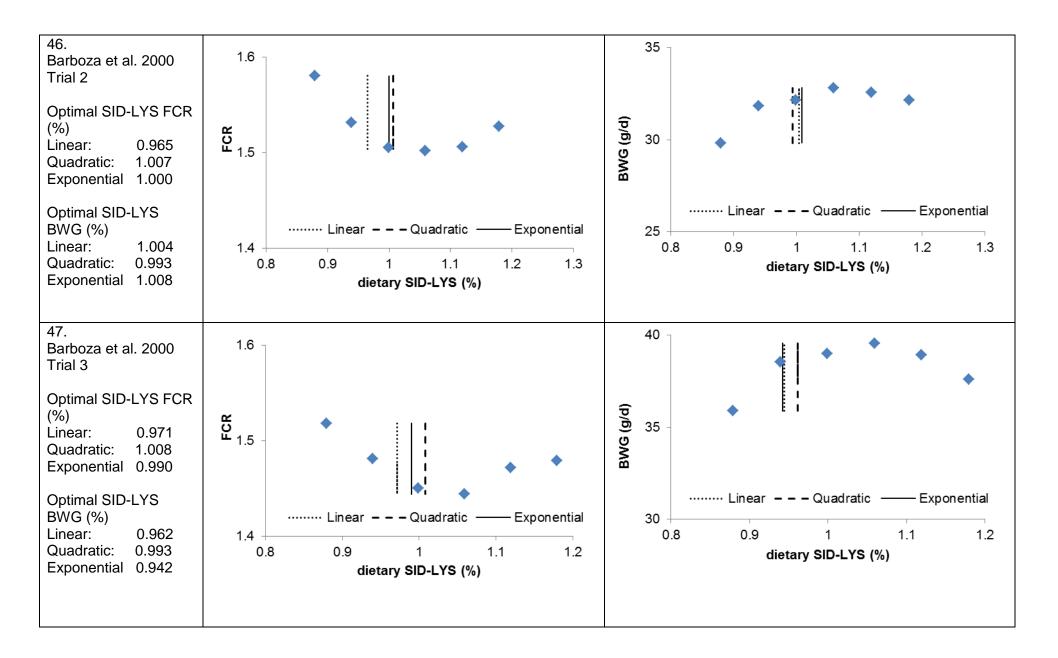


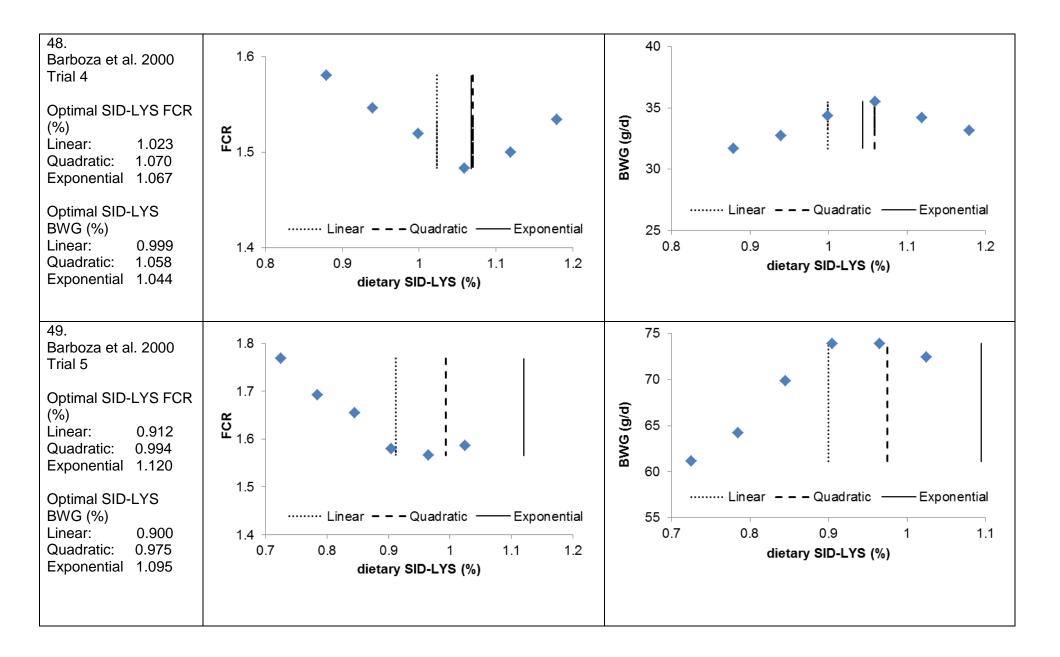


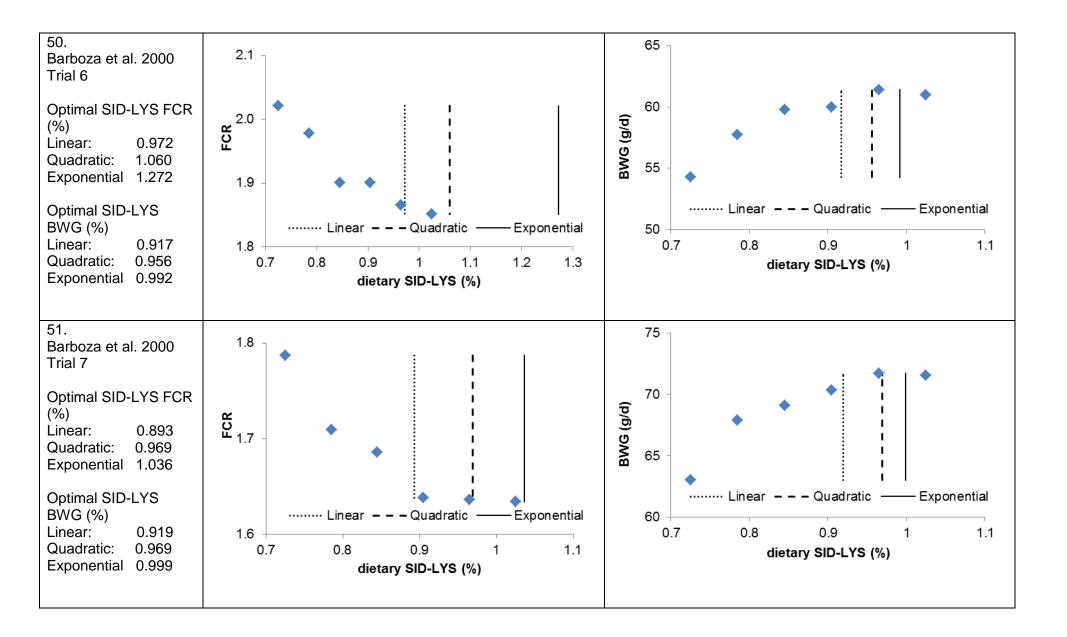


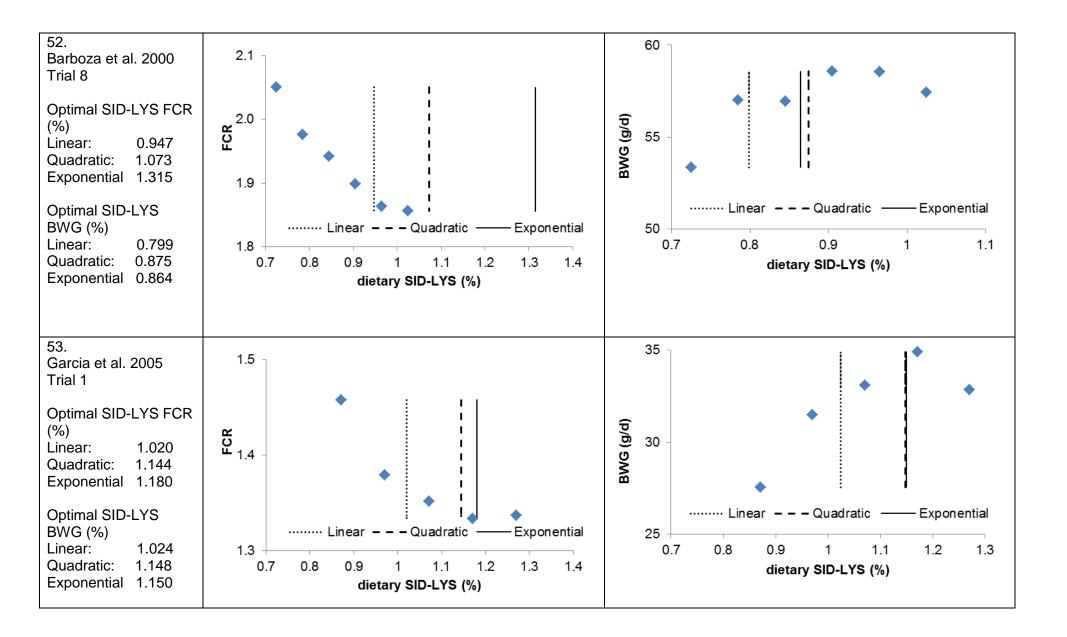


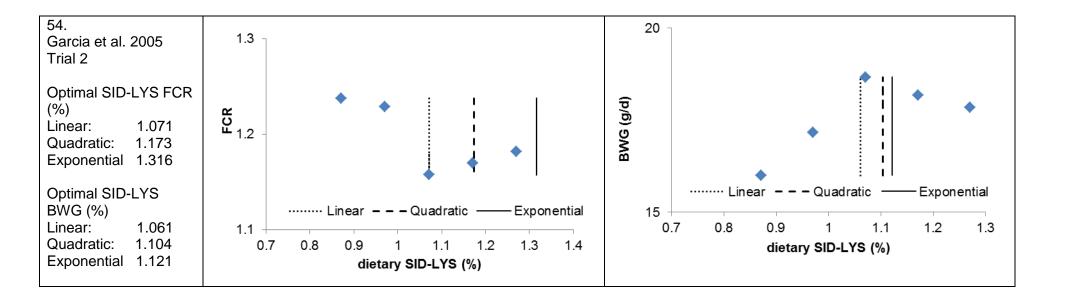












## Appendix B.

#### SID-LYS model estimates using the quadratic broken-line model for minimum FCR and maximum BWG

	-							
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Trial nr.	Estimate	Std. Err.	Estimate	Std. Err.	Estimate	Std. Err.	R <sup>2</sup>
2         1.58         0.038         1.023         0.1166         3.85         3.662         0.892           4         1.60         0.003         1.023         0.1166         3.85         3.662         0.892           4         1.60         0.003         1.023         0.1166         3.85         3.662         0.892           5         1.44         0.049         1.071         0.1455         3.40         3.419         0.865           6         1.62         0.004         1.043         0.0106         3.77         0.287         1.000           7         1.41         0.035         1.213         0.0636         3.66         1.244         0.971           9         1.46         0.015         1.128         0.3379         2.00         2.629         0.885           10         1.46         0.017         1.248         0.0196         3.10         0.413         0.997           14         1.46         0.007         1.248         0.0196         3.10         0.413         0.997           15         1.40         0.077         1.428         0.1028         1.74         0.306         0.986           18         1.63 <t< th=""><th><u> </u></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></t<>	<u> </u>							
3         1.53         0.033         1.023         0.1166         3.85         3.662         0.882           4         160         0.003         1.058         0.0053         4.29         0.153         1.000           5         1.44         0.049         1.071         0.1455         3.40         3.419         0.865           6         1.62         0.004         1.043         0.0106         3.77         0.287         1.000           7         1.41         0.032         1.213         0.06549         4.49         2.014         0.971           9         1.46         0.015         1.126         0.0485         3.53         1.347         0.979           11         1.79         0.048         1.120         0.1330         8.87         15.414         0.725           12         1.40         0.007         1.428         0.1005         2.06         0.521         0.997           14         1.46         0.006         1.91         0.0289         1.74         0.306         0.986           17         1.45         0.006         1.91         0.0289         1.74         0.309         0.986           18         1.63 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>								
41.600.0031.0580.00534.290.1531.00051.440.0491.0710.14553.403.4190.86561.620.0041.0430.01063.770.2871.00071.410.0351.2130.06363.661.2460.98581.460.0151.1260.04853.531.3470.97991.460.0151.1260.04853.531.3470.979111.790.0481.1200.13308.8715.4140.725121.400.0071.2480.01963.100.4130.997141.460.0071.0900.04041.560.4040.984151.400.0771.4280.10052.060.5210.986161.490.0061.0340.03943.441.6300.913191.220.0101.3960.07990.580.1710.978201.170.0061.1570.03441.860.3970.986211.140.0151.3250.07551.130.3910.965221.050.0071.0670.03633.251.1380.967231.870.0040.8040.002486.574.4841.000241.720.0051.0280.05212.681.8930.977251.750.1031.047<	2							
5         1.44         0.049         1.071         0.1455         3.40         3.419         0.865           6         1.62         0.004         1.043         0.0106         3.77         0.287         1.000           7         1.44         0.021         1.119         0.0549         4.49         2.014         0.971           9         1.46         0.015         1.126         0.0385         3.53         1.347         0.979           11         1.79         0.048         1.120         0.1330         8.87         15.414         0.725           12         1.40         0.007         1.248         0.0195         2.06         0.521         0.997           16         1.49         0.006         1.911         0.0289         1.74         0.306         0.886           18         1.63         0.006         1.911         0.0289         1.74         0.306         0.886           20         1.17         0.006         1.57         0.314         1.86         0.397         0.986           21         1.44         0.017         1.067         0.0363         3.25         1.138         0.967           22         1.05								
61.620.0041.0430.0106 $3.77$ 0.2871.00071.410.0351.2130.0636 $3.66$ 1.2460.98581.460.01511.2850.33792.002.6290.895101.460.01511.1260.0485 $3.53$ 1.3470.979111.790.0481.1200.13308.8715.4140.725121.400.0071.2480.0196 $3.10$ 0.4130.997141.460.0071.2480.10552.060.5210.985151.400.0771.4280.10052.060.5210.986161.490.0061.1910.02891.740.3060.986181.630.0061.0340.03943.441.6300.913191.220.0101.3960.07551.130.3970.986201.170.0061.1570.03141.860.3970.986211.140.0151.3250.05212.681.8930.977231.870.0040.8040.002486.574.4841.000241.720.0031.0050.01491.910.1750.998251.750.0031.0050.01491.910.1750.998261.720.0301.00470.12481.771.1870.906301.600.014<	4							
71.410.0351.2130.06363.661.2460.98581.460.0211.1190.05494.492.0140.97191.460.1511.2850.33792.002.6290.895101.460.0151.1260.04853.531.3470.979111.790.0481.1200.13308.8715.4140.725121.400.0071.2480.01963.100.4130.997141.460.0071.0900.04041.560.4040.984171.450.0061.1910.02891.740.3060.986181.630.0061.1940.03943.441.6300.913191.220.0101.3960.07990.580.1710.978201.170.0061.1570.03633.251.1380.967231.870.00071.0670.03633.251.1380.967241.720.0051.0280.05212.681.8930.977251.750.0001.0850.00651.950.6300.952271.780.0041.0610.01262.770.1990.998281.720.0031.0050.1481.771.1870.906301.600.0141.1420.08791.260.6700.339311.390.0111.08								
8         1.46         0.021         1.119         0.0549         4.49         2.014         0.971           9         1.46         0.151         1.285         0.3379         2.00         2.629         0.895           10         1.46         0.0151         1.126         0.1330         8.87         15.414         0.725           12         1.40         0.007         1.248         0.0196         3.10         0.413         0.997           14         1.46         0.0077         1.248         0.1005         2.06         0.521         0.997           16         1.49         0.0077         1.428         0.1005         2.06         0.521         0.997           16         1.49         0.007         1.428         0.1005         2.06         0.521         0.997           16         1.49         0.006         1.191         0.0289         1.74         0.306         0.986           17         1.45         0.006         1.157         0.314         1.86         0.397         0.986           21         1.17         0.006         1.028         0.0521         2.68         1.893         0.977           25         1.05								
9         1.46         0.151         1.285         0.3379         2.00         2.629         0.895           10         1.46         0.015         1.126         0.0485         3.53         1.347         0.979           11         1.79         0.048         1.120         0.1330         8.87         15.414         0.725           12         1.40         0.007         1.248         0.0196         3.10         0.413         0.997           14         1.46         0.007         1.428         0.1005         2.06         0.521         0.997           16         1.49         0.007         1.090         0.0404         1.56         0.404         0.986           17         1.45         0.006         1.034         0.0394         3.44         1.630         0.913           19         1.22         0.010         1.325         0.0755         1.13         0.391         0.986           21         1.14         0.015         1.325         0.0755         1.138         0.967           23         1.87         0.000         1.085         0.0001         1.000         2.68         1.893         0.977           25         1.75								
101.460.0151.1260.04853.531.3470.979111.790.0481.1200.13308.8715.4140.725121.400.0071.2480.01963.100.4130.997141.460.0091.0480.04551.870.6020.985151.400.0071.0900.04041.560.4040.984171.450.0061.1910.02891.740.3060.986181.630.0061.0340.03943.441.6300.913191.220.0101.3960.07990.580.1710.978201.170.0061.1570.03141.860.3970.986211.140.0151.3250.07551.130.3910.965221.050.0071.0670.03633.251.1380.967231.870.0040.8040.002486.574.4841.000241.720.0051.0280.05212.681.8930.977251.750.0001.0850.00001.000.0001.000261.890.0191.0230.06551.950.6300.952271.780.0041.0610.01262.770.1990.998281.720.0031.0050.01491.910.1750.998301.600.014								
111.79 $0.048$ 1.120 $0.1330$ $8.87$ $15.414$ $0.725$ 121.40 $0.007$ 1.248 $0.0196$ $3.10$ $0.413$ $0.997$ 141.46 $0.009$ 1.048 $0.0455$ $1.87$ $0.602$ $0.985$ 151.40 $0.077$ $1.428$ $0.1005$ $2.06$ $0.521$ $0.997$ 16 $1.49$ $0.007$ $1.090$ $0.0404$ $1.56$ $0.404$ $0.984$ 17 $1.45$ $0.006$ $1.191$ $0.0289$ $1.74$ $0.306$ $0.986$ 18 $1.63$ $0.006$ $1.157$ $0.0314$ $1.86$ $0.397$ $0.986$ 20 $1.17$ $0.006$ $1.157$ $0.0314$ $1.86$ $0.397$ $0.986$ 21 $1.144$ $0.015$ $1.325$ $0.0755$ $1.13$ $0.391$ $0.965$ 22 $1.05$ $0.007$ $1.067$ $0.0363$ $3.25$ $1.138$ $0.967$ 23 $1.72$ $0.005$ $1.028$ $0.0521$ $2.68$ $1.893$ $0.977$ 25 $1.75$ $0.004$ $1.061$ $0.0126$ $2.77$ $0.199$ $0.998$ 28 $1.72$ $0.003$ $1.0047$ $0.1248$ $1.77$ $1.187$ $0.906$ 30 $1.60$ $0.014$ $1.142$ $0.0879$ $1.26$ $0.670$ $0.939$ 31 $1.39$ $0.011$ $1.083$ $0.0320$ $7.06$ $2.787$ $0.958$ 32 $1.84$ $0.019$ $1.0223$ $8.36$	9	1.46	0.151	1.285	0.3379	2.00	2.629	0.895
121.40 $0.007$ $1.248$ $0.0196$ $3.10$ $0.413$ $0.997$ 141.46 $0.007$ $1.048$ $0.0455$ $1.87$ $0.602$ $0.985$ 151.40 $0.077$ $1.428$ $0.1005$ $2.06$ $0.521$ $0.997$ 16 $1.49$ $0.006$ $1.030$ $0.0404$ $1.56$ $0.404$ $0.984$ 17 $1.45$ $0.006$ $1.034$ $0.0394$ $3.44$ $1.630$ $0.913$ 19 $1.22$ $0.010$ $1.396$ $0.0799$ $0.58$ $0.171$ $0.978$ 20 $1.17$ $0.006$ $1.157$ $0.0314$ $1.86$ $0.397$ $0.986$ 21 $1.14$ $0.015$ $1.325$ $0.0755$ $1.13$ $0.391$ $0.965$ 22 $1.05$ $0.007$ $1.067$ $0.0363$ $3.25$ $1.138$ $0.967$ 23 $1.87$ $0.004$ $0.804$ $0.0024$ $86.57$ $4.484$ $1.000$ 24 $1.72$ $0.005$ $1.028$ $0.0521$ $2.68$ $1.893$ $0.977$ 25 $1.75$ $0.004$ $1.061$ $0.0126$ $1.77$ $0.199$ $0.998$ 26 $1.89$ $0.019$ $1.023$ $0.0655$ $1.95$ $0.630$ $0.952$ 27 $1.78$ $0.004$ $1.061$ $0.0126$ $2.77$ $0.199$ $0.998$ 28 $1.72$ $0.030$ $1.005$ $0.0323$ $8.66$ $2.467$ $0.985$ 32 $1.38$ $0.014$ $1.44$ $0.0320$ <td>10</td> <td>1.46</td> <td>0.015</td> <td>1.126</td> <td>0.0485</td> <td>3.53</td> <td>1.347</td> <td>0.979</td>	10	1.46	0.015	1.126	0.0485	3.53	1.347	0.979
121.40 $0.007$ $1.248$ $0.0196$ $3.10$ $0.413$ $0.997$ 141.46 $0.007$ $1.048$ $0.0455$ $1.87$ $0.602$ $0.985$ 151.40 $0.077$ $1.428$ $0.1005$ $2.06$ $0.521$ $0.997$ 16 $1.49$ $0.006$ $1.030$ $0.0404$ $1.56$ $0.404$ $0.984$ 17 $1.45$ $0.006$ $1.034$ $0.0394$ $3.44$ $1.630$ $0.913$ 19 $1.22$ $0.010$ $1.396$ $0.0799$ $0.58$ $0.171$ $0.978$ 20 $1.17$ $0.006$ $1.157$ $0.0314$ $1.86$ $0.397$ $0.986$ 21 $1.14$ $0.015$ $1.325$ $0.0755$ $1.13$ $0.391$ $0.965$ 22 $1.05$ $0.007$ $1.067$ $0.0363$ $3.25$ $1.138$ $0.967$ 23 $1.87$ $0.004$ $0.804$ $0.0024$ $86.57$ $4.484$ $1.000$ 24 $1.72$ $0.005$ $1.028$ $0.0521$ $2.68$ $1.893$ $0.977$ 25 $1.75$ $0.004$ $1.061$ $0.0126$ $1.77$ $0.199$ $0.998$ 26 $1.89$ $0.019$ $1.023$ $0.0655$ $1.95$ $0.630$ $0.952$ 27 $1.78$ $0.004$ $1.061$ $0.0126$ $2.77$ $0.199$ $0.998$ 28 $1.72$ $0.030$ $1.005$ $0.0323$ $8.66$ $2.467$ $0.985$ 32 $1.38$ $0.014$ $1.44$ $0.0320$ <td>11</td> <td></td> <td>0.048</td> <td></td> <td>0.1330</td> <td></td> <td>15.414</td> <td>0.725</td>	11		0.048		0.1330		15.414	0.725
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381.600.0100.9610.02538.292.3220.990391.430.0041.0330.02363.481.1370.986401.830.0150.8680.06337.418.0720.871411.380.0131.1620.05322.370.9540.965421.400.0091.1000.04183.471.4920.962431.870.0051.0180.01963.660.6840.992441.990.0080.9630.04174.182.2730.942451.480.0131.0020.05568.167.6790.866461.510.0061.0070.04704.323.2990.909471.460.0091.0080.86223.454.7870.750481.510.0131.0700.10972.072.4670.767491.570.0140.9940.04952.720.9810.972501.850.0211.0600.08841.530.7130.967511.630.0070.9690.03402.500.7060.982521.850.0131.0730.04581.620.3660.993531.340.0041.1440.03071.600.3630.992	37	1.60	0.003	1.018	0.0159	2.79		0.998
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511.630.0070.9690.03402.500.7060.982521.850.0131.0730.04581.620.3660.993531.340.0041.1440.03071.600.3630.992								
521.850.0131.0730.04581.620.3660.993531.340.0041.1440.03071.600.3630.992								
53 1.34 0.004 1.144 0.0307 1.60 0.363 0.992								
<u>54</u> 1.17 0.018 1.173 0.2150 0.80 1.158 0.757								
	54	1.17	0.018	1.173	0.2150	0.80	1.158	0.757

## SID-LYS model estimates using the quadratic broken-line model for minimum FCR

Trial an	Estimate	Std. Err.	Estimate	Std. Err.	Estimate	Std. Err.	R <sup>2</sup>
Trial nr.	L	L	R	R	U	U	
1	185	3.1	1.040	0.0549	-738	345.0	0.954
2	149	3.4	1.034	0.0547	-849	406.6	0.953
3	45	2.3	1.090	0.1312	-162	135.8	0.906
4	45	0.4	1.034	0.0208	-223	34.5	0.998
6	42	0.5	0.954	0.0310	-304	105.1	0.992
7	47	1.3	1.151	0.0635	-188	83.1	0.972
8	42	1.0	1.096	0.0390	-347	122.2	0.982
9	41	1.2	1.125	0.0816	-171	109.8	0.943
10	39	1.2	1.044	0.0678	-373	299.5	0.929
12	42	0.7	1.193	0.0451	-208	82.6	0.976
14	39	0.3	0.908	0.0232	-422	145.6	0.986
16	75	0.2	1.035	0.0217	-127	21.5	0.994
17	83	0.6	1.124	0.0351	-195	53.8	0.966
18	67	0.5	0.983	0.0891	-222	328.4	0.545
19	29	0.1	1.213	0.0161	-71	7.5	0.997
20	33	0.3	1.079	0.0304	-173	48.3	0.978
21	22	0.1	1.294	0.0180	-38	3.5	0.997
22	22	0.2	1.163	0.0438	-56	16.6	0.974
23	31	0.2	0.815	0.0067	-1273	166.8	0.997
24	98	0.3	1.064	0.1164	-54	69.5	0.900
26	94	0.8	0.944	0.0423	-172	45.2	0.969
27	104	0.7	1.014	0.0368	-208	50.8	0.974
28	84	0.3	0.923	0.0187	-252	39.2	0.995
29	77	0.2	0.864	0.0196	-222	47.3	0.992
30	62	0.9	1.083	0.0976	-100	72.8	0.896
31	38	0.5	1.111	0.0549	-135	77.2	0.907
32	33	0.2	1.172	0.0642	-35	15.0	0.962
33	32	0.3	1.135	0.1703	-23	29.6	0.737
34	21	0.3	1.148	0.0693	-49	25.6	0.945
35	31	0.3	1.058	0.0346	-99	23.7	0.988
36	33	1.0	1.204	0.0962	-66	28.7	0.957
37	59	0.3	0.925	0.0286	-351	133.9	0.986
38	61	0.6	0.970	0.0434	-291	134.1	0.974
39	29	0.2	1.006	0.0552	-146	140.2	0.896
40	65	0.6	0.917	0.0709	-140	118.9	0.902
41	35	0.2	1.156	0.0300	-78	18.3	0.988
42	32	0.1	1.040	0.0302	-114	50.6	0.965
43	83	0.5	0.953	0.0413	-298	170.0	0.940
45	36	0.5	1.054	0.0751	-135	121.6	0.849
46	32	0.2	0.993	0.0317	-199	115.0	0.944
47	39	0.4	0.962	0.0663	-426	682.1	0.765
48	34	0.6	1.058	0.1289	-86	129.4	0.664
49	73	1.1	0.975	0.0582	-211	98.8	0.952
50	61	0.4	0.956	0.0368	-122	39.7	0.976
51	71	0.5	0.969	0.0436	-134	48.6	0.970
52	58	0.5	0.875	0.0598	-200	164.4	0.882
53	34	0.7	1.148	0.0994	-81	58.7	0.927
54	18	0.3	1.104	0.1172	-41	41.9	0.886

SID-LYS model estimates using the quadratic broken-line model for maximum BWG