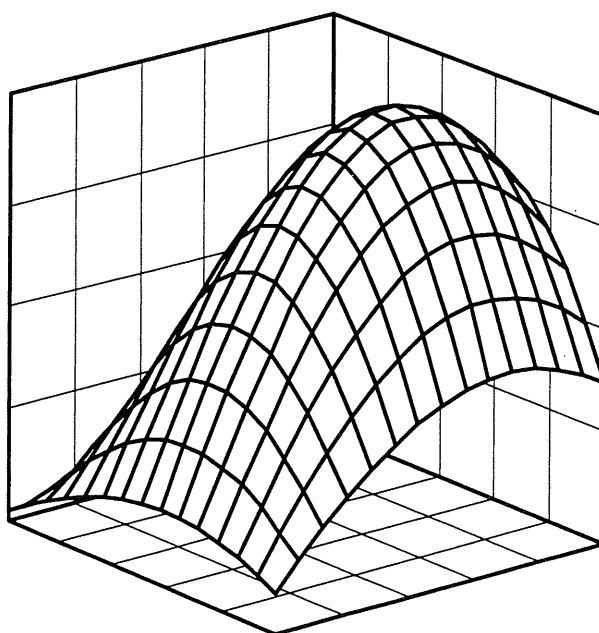


SUCROS97: Simulation of crop growth for potential and water-limited production situations

As applied to spring wheat



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E-mail: h.f.m.tenberge@ab.dlo.nl	E-mail: martin.vanittersum@staff.tpe.wau.nl

SUCROS97: Simulation of crop growth for potential and water-limited production situations

As applied to spring wheat

Editors H.H. van Laar*, J. Goudriaan* & H.van Keulen

PE ab-dlo

* Department of Theoretical
Production Ecology
Wageningen Agricultural University
P.O. Box 430
6700 AK Wageningen

CIP-DATA KONINKLIJKE BIBLIOTHEEK, DEN HAAG

Laar, H.H. van, J. Goudriaan & H. van Keulen

SUCROS97: Simulation of crop growth for potential and water-limited production situations. As applied to spring wheat.
Wageningen : DLO Research Institute for Agrobiological Sciences and Soil Fertility ; Wageningen : The C.T. de Wit Graduate School for Production Ecology. - (Quantitative approaches in systems analysis ; no. 14)
NUGI 835

Key words: simulation model, systems analysis, photosynthesis, water stress

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H. Terburg
AB-DLO

P.O. Box 14
NL-6700 AA Wageningen
Phone: (+) 31 317.475723
Fax: (+) 31 317.423110
E-mail: h.terburg@ab.dlo.nl

Th.H. Jetten
Secretariat C.T. de Wit Graduate School
for Production Ecology
Lawickse Allee 13
NL-6701 AN Wageningen
Phone: (+) 31 317.485116
Fax: (+) 31 317.484855
E-mail: theo.jetten@beleid.spp.wau.nl

Preface

This report describes the new 1997 versions of the models SUCROS1 and SUCROS2, which are improved and slightly modified versions of the models as they were described in our earlier report of 1992.

The units of the variables were streamlined into g m^{-2} for dry matter variables and to mm for water balance variables. The leaf assimilation rates were first expressed on a second basis, but integrated into daily values, so that daily growth rate and daily transpiration rates are expressed in $\text{g m}^{-2} \text{d}^{-1}$ and in mm d^{-1} , respectively.

The unit of air humidity was altered from mbar to kPa.

Over the past five years we were pointed to several errors and bugs in the 1992 version. We gratefully acknowledge such contributions of all our colleagues, but we would like to mention specifically Daniel van Kraalingen and Willem Stol who were most helpful in this respect.

The model SUCROS1 is for potential growth situations, whereas SUCROS2 is for water-limited situations. The results of SUCROS2 become identical to those of SUCROS1 when there is enough water to prevent any water shortage, and not so much as to cause water logging.

The modelling of the soil water balance is done by the 'tipping bucket' approach, with a daily time interval of integration. The soil depth was extended to 2 m, so that the number of soil layers had to be increased from three to four.

We added the major photosynthesis subroutine (MOMASSP) for the calculation of the current rate of canopy photosynthesis, as separately embedded within an FST program. Using this model it is possible to study the diurnal course of canopy photosynthesis as affected by leaf properties, LAI and environmental conditions. Although SUCROS does not provide this intra-diurnal time course, this model will show the underlying dynamics which is integrated within SUCROS by using Gaussian integration over the day.

The models and the Fortran Simulation Translator (FST) are available upon request. Information about distribution and costs can be obtained from:

Software Product Support, AB-DLO

P.O. Box 14, 6700 AA Wageningen, The Netherlands

E-mail: SPS@ab.dlo.nl

Abstract

Two versions of the simulation model for crop growth SUCROS (Simple and Universal CROp growth Simulator) are described, one for potential production (SUCROS1) and one when water is limiting (SUCROS2).

The model is applied to spring wheat, with ample supply of nutrients, and without pests, diseases and weeds. Radiation and temperature (and precipitation in SUCROS2), being the most important environmental factors, and crop characteristics determine growth and development. Crop growth and development are simulated based on underlying chemical, physiological and physical processes. Dry matter accumulation is calculated from daily crop CO_2 assimilation based on leaf CO_2 assimilation and taking into account the respiration costs and allocation of carbohydrates to different plant parts. Following the model listings, the statements are explained step by step.

In water-limited situations, the soil water balance is calculated according to the tipping-bucket system. The Penman-Monteith combination is used to calculate potential evapotranspiration. To account for the effect of water shortage, potential daily total gross CO_2 assimilation of the crop is multiplied by the ratio between actual transpiration rate and potential transpiration rate, and carbohydrate allocation is modified in favour of the roots.

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1. Crop growth model for potential production (SUCROS1)

J. Goudriaan, H. van Keulen & H.H. van Laar

1.1. Introduction

Former versions of the Simple and Universal CROp growth Simulator SUCROS were described by van Keulen *et al.* (1982) and Spitters *et al.* (1989). Most of the process descriptions included in SUCROS1 are explained in Goudriaan & van Laar (1994).

Crop growth is often described by empirical models, such as regression equations. Usually, environmental variables, such as radiation and rainfall, are incorporated in the regression, e.g. a simple approach is to relate yields measured at a given site or region to total seasonal rainfall (Le Houérou & Hoste, 1977; Lomas & Shashoua, 1974; Baier & Robertson, 1967). Such models can generate accurate yield predictions, provided the regression parameters are estimated on the basis of extensive sets of experimental data. The predictions, however, are restricted to the same environment and the same cultivar on which the regression is based. In addition, these empirical, descriptive models give little insight into the causes of the observed variation in yields.

SUCROS1 is a mechanistic model that explains crop growth on the basis of the underlying processes, such as CO₂ assimilation and respiration, as influenced by environmental conditions. The predictive ability of mechanistic models does not always live up to expectations. It should be realized, however, that each parameter estimate and process formulation has its own inaccuracy, and that errors may accumulate in the prediction of final yield. However, yield prediction is a secondary aim of these models. Their primary aim is to increase insight in the system studied by quantitatively integrating the present knowledge in a dynamic simulation model. By studying the behaviour of the model, better insight in the real system is gained.

Crop growth can be limited by various factors, such as shortage of water, or nutrients, and it can be reduced by pests and diseases. Therefore, different model versions have been developed to cope with the actual situation.

SUCROS1 simulates potential growth of a crop, i.e. its dry matter accumulation under ample supply of water and nutrients in a pest-, disease- and weed-free environment under the prevailing weather conditions. The rate of dry matter accumulation is a function of irradiation, temperature and crop characteristics. The basis for the calculation is the rate of CO₂ assimilation (photosynthesis) of the canopy. That rate is dependent on the radiant energy absorbed by the canopy, which is a function of incoming radiation and crop leaf area. From the absorbed radiation and the photosynthetic characteristics of individual leaves, the daily rate of gross CO₂ assimilation of the crop is calculated. These calculations are executed in a set of subroutines added to the model. For a detailed description, the reader is referred to Spitters (1986), Goudriaan (1986), Spitters *et al.* (1986) and Goudriaan & van Laar (1994). A submodel (MOMASSP.FST) that generates the diurnal course of gross assimilation for a specific set of conditions is included for separate study (Appendix I).

Part of the carbohydrates (CH₂O) produced is used to maintain the existing biomass. The remaining carbohydrates are converted into structural dry matter (plant organs). In the process of conversion, part of the weight is lost in growth respiration. The dry matter produced is partitioned among the various plant organs, using partitioning factors defined as a function of the phenological development stage of the crop. The dry weights of the plant organs are obtained by integration of their growth rates over time.

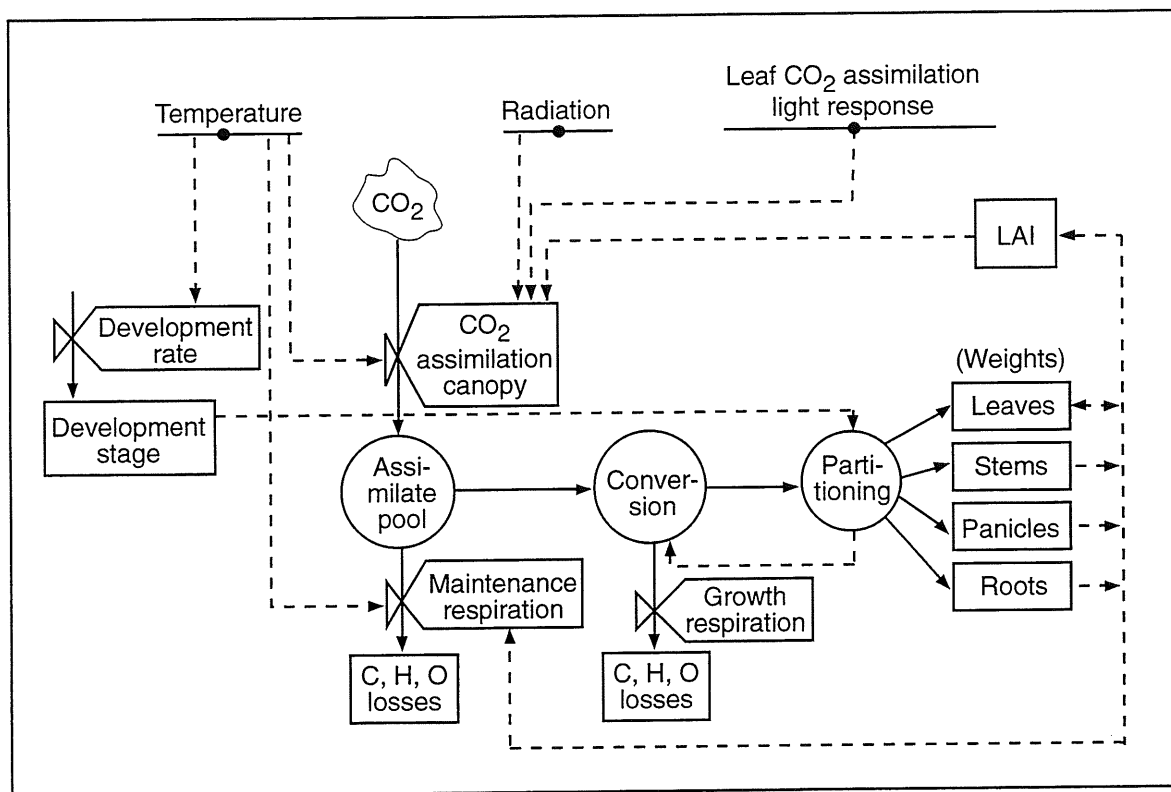


Figure 1.1 Relational diagram of SUCROS1. Boxes are state variables, valves are rate variables, circles are intermediate variables. Solid lines are flows of material, dotted lines are flows of information.
Source: ORYZA1 (SUCROS1 as applied for rice), Kropff et al., 1994.

SUCROS1 requires as input physiological properties of the crop and the actual weather conditions at the site, characterized by its geographical latitude, i.e. daily maximum and minimum temperatures and irradiation for each day of the year. A relational diagram is given in Figure 1.1.

SUCROS1 is written in FST, the FORTRAN Simulation Translator, a program developed by Rappoldt & van Kraalingen (1996). The model can be executed on VAX computers, IBM PC-AT's, or compatibles and Apple-Macintosh computers.

FST requires, before the program starts, a definition of the call for subroutines that are used in the program. All variables in the subroutine-call have to be defined as input or output variables. Following the definition of the subroutine-calls the program starts with the **TITLE** of the program.

```
DEFINE_CALL GLA      (INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, ...
                     INPUT, INPUT,      OUTPUT)
DEFINE_CALL SUBEAI (INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, OUTPUT)
DEFINE_CALL TOTASS (INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, ...
                  INPUT, INPUT,      OUTPUT, OUTPUT, OUTPUT)
```

```
TITLE Crop growth for potential production (SUCROS1)
*      Spring wheat, Version September 1997 (SUCROS1_97 V1.0)
```


1.2. Initial conditions

INITIAL

```
*   INCON ZERO      = 0.
    PARAMETER DOYEM = 90.
    INCON WLVI       = 0.5; WSTI = 0.3; WRTI = 0.8
    INCON WLVDI      = 0. ; WSOI = 0. ; ILAI = 0.012
    INCON IDVS       = 0. ; IEAI = 0.

* Initialization of TNASS: total CO2 equivalents initially available
  TNASSI = (WLVI*CFLV + WSTI*CFST + WRTI*CFRT) * 44./12.
```

Usually, the model SUCROS1 starts at the moment of crop emergence (DOYEM), the number 90 representing the day of the year.

The initial amounts of dry matter in leaves (WLVI, g DM m⁻²), stems (WSTI, g DM m⁻²), and roots (WRTI, g DM m⁻²) are set to their values at emergence; in this case ILAI=0.012 and SLA=0.022, so that WLVI becomes ca 0.5 g m⁻², from the partitioning tables the values of WSTI and WRTI can be found. Dead leaves (WLVDI, g DM m⁻²) and storage organs (WSOI, g DM m⁻²) at emergence are zero. The initial value for the leaf area index (ILAI, m² m⁻²) has been set at 0.012, assuming a plant density of 210 plants m⁻² and a leaf area per plant at emergence of 5.7×10^{-5} m² plant⁻¹. ILAI has a large effect on further growth. The initial values for development stage (IDVS, -) and ear area index (IEAI, m² m⁻²) are set to zero.

FST requires a variable as initial condition for an integral. If this integral starts at zero (e.g. summation of temperature) the variable ZERO is used.

1.3. Crop development

DYNAMIC

```
DVS      = INTGRL(IDVS, DVR)
DVR      = INSW(DVS-1., AFGEN(DVRVT, DAVTMP),...
               AFGEN(DVRRT, DAVTMP)) * EMERG
EMERG    = INSW(TIME-DOYEM, 0., 1.)
FUNCTION DVRVT = -10.,0., 0.,0., 30.,0.027
FUNCTION DVRRT = -10.,0., 0.,0., 30.,0.031
```

This part is described in more detail in Chapter 5 in Goudriaan & van Laar (1994). The pattern of dry matter distribution over the various plant organs is directly dependent on the phenological development stage of the crop. For many annual crops, the development stage (DVS) can be conveniently expressed in a dimensionless variable, having the value 0 at seedling emergence, 1 at flowering and 2 at maturity. The development stage is calculated as the integral of the development rate (DVR, d⁻¹).

The development rate is calculated separately for the period from emergence till flowering (pre-anthesis, DVRV), and from flowering till maturity (post-anthesis, grain filling, DVRR). Under temperate climatological conditions, temperature is the main environmental factor affecting the rate of development. So, DVRV and DVRR are defined as functions of average day temperature (DAVTMP, °C).

Phenological development starts at seedling emergence. The factor EMERG equals 0 before emergence and 1 after emergence. For explanation of the INSW function see Appendix II.

1.4. Leaf CO₂ assimilation

```

      AMAX      = AMX * AMDVS * AMTMP * EMERG
      AMDVS     = AFGEN(AMDVST, DVS)
      AMTMP     = AFGEN(AMTMPT, DDTMP)
PARAMETER AMX  = 1.11E-3
* 1.11 mg CO2/m2/s = 40 kg CO2/ha/h
FUNCTION AMDVST = 0.0,1.0, 1.0,1.0, 2.0,0.5, 2.5,0.0
FUNCTION AMTMPT = -10.,0.,0.,0.,10.,1.,25.,1.,35.,0.,50.,0.

```

This part is described in more detail in Chapter 8 in Goudriaan & van Laar (1994). The response of leaf CO₂ assimilation to light intensity is characterized by its slope at low light intensity and its maximum rate at light saturation (AMX , g CO₂ m⁻² s⁻¹). The temperature effect ($AMTMP$) is a function of the average temperature during daytime ($DDTMP$, °C) as given in the function $AMTMPT$.

The value of AMX used in the model, refers to the assimilation capacity of full-grown leaves at the top of the canopy, as these leaves absorb most of the radiation. The maximum CO₂ assimilation capacity of leaves varies with crop species and cultivar. If no firmly based value of AMX is available, a value of 1.11 mg CO₂ m⁻² s⁻¹ for C₃ species is, in general, a reasonable estimate.

The photosynthetic capacity of a leaf is also affected by its age: AMX reaches a maximum shortly after full expansion of the leaf, followed by a gradual decline with age (Rawson *et al.*, 1983; Dwyer & Stewart, 1986). The effect of ageing of the canopy is introduced by a multiplication factor ($AMDVS$) defined as a function of the development stage.

1.5. Daily gross CO₂ assimilation

```

      CALL TOTASS(DAY, LATT, DTR, SCP, AMAX, EFF, KDF, TAI, ...
                DAYL, DTGA, DS0)
PARAMETER EFF  = 12.5E-6
* 12.5 microgram CO2/J = 0.45 (kg CO2/ha/h)/(J/m2/s)
PARAMETER KDF  = 0.60
PARAMETER SCP  = 0.20
PARAMETER LATT = 52.

```

This part is described in more detail in Chapter 6 in Goudriaan & van Laar (1994). Daily gross crop CO₂ assimilation ($DTGA$, g CO₂ m⁻² d⁻¹) is calculated from the photosynthetically active radiation (PAR , J m⁻² s⁻¹) absorbed by the canopy and the CO₂ assimilation - light response of individual leaves. If radiation intensities averaged over the day and over the canopy were applied, daily canopy CO₂ assimilation would be seriously overestimated, because CO₂ assimilation responds to light intensity in a non-linear way. In the model, the temporal and spatial variation in radiation intensity over the leaves is, therefore, taken into account.

The computation is performed in the Subroutine $TOTASS$. This routine makes use of the Subroutines $ASTRO$ and $ASSIM$. $SUCROS1$ can be applied without a thorough understanding of these subroutines. Three parameters used in these subroutines, EFF , KDF and SCP , have to be specified and were derived from literature.

Detailed discussions are also given by Spitters *et al.* (1986) for the calculation of the diffuse and direct radiation fluxes above the canopy, by Spitters (1986) for the calculation of assimilation rates from these fluxes, and by Goudriaan (1986) for the Gaussian integration method used to integrate instantaneous assimilation rates over the canopy and over the day (see also Appendix II).

The only site characteristic required for the calculation of potential production is the latitude (LATT). In the given example, a latitude of 52° N for The Netherlands was used.

1.6. Carbohydrate production

$$GPHOT = DTGA * 30./44.$$

This part is described in more detail in Chapter 4 in Goudriaan & van Laar (1994). In the leaves, the absorbed CO₂ is reduced to carbohydrates (CH₂O) using the energy supplied by the absorbed light. For each g of CO₂ absorbed, 30/44 g of CH₂O is formed, the numerical values representing the molecular weights of CH₂O and CO₂, respectively.

1.7. Maintenance respiration

```

MAINT      = MAINTS * TEFF * MNDVS * EMERG
MAINTS     = MAINLV*WLVG + MAINST*WST + MAINRT*WRT + MAINSO*WSO
MNDVS      = WLVG / NOTNUL(WLV)
TEFF       = Q10**((DAVTMP-TREF)/10.)
PARAMETER Q10      = 2.;   TREF   = 25.
PARAMETER MAINLV   = 0.03; MAINST = 0.015
PARAMETER MAINRT   = 0.015; MAINSO = 0.01

```

This part is described in more detail in Chapter 4 in Goudriaan & van Laar (1994). Part of the carbohydrates formed is respired to provide energy for maintaining the existing biostructures. In the model, fixed coefficients (for a plant species dependent reference temperature) are used to calculate the maintenance requirements of the various organs (leaves, stems, roots and storage organs, i.e. grains, tubers etc.) of the crop. Higher temperatures accelerate the turnover rates in plant tissue and hence increase the costs of maintenance (TEFF). An increase in temperature of 10 °C increases maintenance respiration by a factor 2 (Penning de Vries & van Laar, 1982).

When the crop ages, its metabolic activity decreases and hence its maintenance requirements. This is mimicked in the model by assuming that maintenance respiration is proportional to the fraction of the accumulated leaf weight that is still green. The reduction factor, MNDVS, is also applied to maintenance respiration of the other organs as it is assumed that dying of stem tissue and roots, and dying of leaves proceed simultaneously. The NOTNUL function prevents division by zero (see Appendix II).

1.8. Dry matter partitioning

```

FSH        = AFGEN(FSHTB, DVS)
FRT        = 1. - FSH
FUNCTION FSHTB = 0.00,0.50, 0.10,0.50, 0.20,0.60, 0.35,0.78,...
               0.40,0.83, 0.50,0.87, 0.60,0.90, 0.70,0.93,...
               0.80,0.95, 0.90,0.97, 1.00,0.98, 1.10,0.99,...
               1.20,1.00, 2.50,1.00
FLV        = AFGEN(FLVTB, DVS)
FUNCTION FLVTB = 0.00,0.65, 0.10,0.65, 0.25,0.70, 0.50,0.50,...
               0.70,0.15, 0.95,0.00, 2.50,0.00

```

```

FST      = AFGEN(FSTTB, DVS)
FUNCTION FSTTB = 0.00,0.35, 0.10,0.35, 0.25,0.30, 0.50,0.50,...
               0.70,0.85, 0.95,1.00, 1.05,0.00, 2.50,0.00
FSO      = AFGEN(FSOTB, DVS)
FUNCTION FSOTB = 0.00,0.00, 0.95,0.00, 1.05,1.00, 2.50,0.00

ERRSH    = ABS(FLV + FST + FSO - 1.)
FINISH ERRSH > 1.E-6

```

This part is described in more detail in Chapter 5 in Goudriaan & van Laar (1994). The primary assimilates in excess of the maintenance costs are available for conversion into structural plant material. Occasionally, the combination of low radiation, high temperature and high biomass may cause a *shortage* rather than an *excess* of primary assimilates. For reasons of model simplicity and lack of empirical evidence, no alternative assimilate route was formulated for such a situation. This implies that structural plant material is then used to support maintenance. Partitioning over the various plant organs is described by fixed distribution factors, defined as a function of development stage. This partitioning occurs in two steps. Dry matter is first partitioned between shoots (FSH) and roots (FRT), followed by distribution of the shoot fraction among leaves (FLV), stems (FST) and storage organs (FSO). To avoid errors in the partitioning tables the variable ERRSH is introduced.

1.9. Growth of plant organs and translocation

```

ASRQ      = FSH * (ASRQLV*FLV+ASRQST*FST+ASRQSO*FSO) + ...
              ASRQRT*FRT

TRANSL    = INSW(DVS-1., 0., WST * DVR * FRTRL)

GTW       = (GPHOT - MAINT + CONVL*TRANSL*CFST*30./12.)/ASRQ
GRT       = FRT * GTW
GLV       = FLV * FSH * GTW
GST       = FST * FSH * GTW - TRANSL
GSO       = FSO * FSH * GTW

```

* The following values are calculated without

* the costs of nitrate reduction:

PARAMETER ASRQRT = 1.444; ASRQLV = 1.463

PARAMETER ASRQST = 1.513; ASRQSO = 1.415

PARAMETER FRTRL = 0.20 ; CONVL = 0.947

This part is described in more detail in Chapters 4 and 5 in Goudriaan & van Laar (1994). The overall value of assimilate requirement for conversion of carbohydrates into dry matter (ASRQ, g CH₂O g⁻¹ DM) for the crop as a whole is calculated as the weighted mean of the ASRQ's for the different plant organs. The assimilates required to produce a unit dry weight of a certain plant organ can be calculated from its chemical composition and the assimilate requirements of the various chemical compounds. Typical values for roots, leaves and stems are: 1.444, 1.463, and 1.513 g CH₂O g⁻¹ dry matter, respectively. Storage organs (grains, tubers, etc.) vary too much in composition among species to give one general value for their assimilate requirement. For wheat grains, it is 1.415 g CH₂O g⁻¹ dry matter (Penning de Vries & van Laar, 1982; Penning de Vries *et al.*, 1989 (Table 11)).

The growth rates of the various plant organs ($\text{g dry matter m}^{-2} \text{ d}^{-1}$) are obtained by multiplying the overall growth rate by the fractions allocated to the various organs.

After anthesis, about 20% of the stem weight, assumed to consist of reserve carbohydrates (Spiertz & Ellen, 1978), is eventually translocated to the storage organs. The translocation rate (TRANSL, $\text{g dry matter m}^{-2} \text{ d}^{-1}$) is introduced as a loss term in the rate of growth of stems (G_{ST}), and added to the assimilate flow that is available for growth (G_{TW}). Upon conversion to structural dry matter, these assimilates are subject to losses due to growth respiration and, therefore, divided by the assimilate requirement factor $ASRQ$. No distinction is made between assimilates originating from current photosynthesis (G_{PHOT}) and those derived from translocation. In addition, a small conversion loss occurs when stem reserves are remobilized presumably from starch to glucose (multiplication by a factor 0.947 (CONVL), Penning de Vries *et al.*, 1989, pg 61). The rate of translocation depends directly on development rate, and is proportional to a factor F_{TRTL} that expresses the fraction eventually translocated. The value of this factor should be determined by trial and error. It influences loss of stem weight in the grain filling period, and it will affect the final harvest index.

1.10. Leaf and ear development

```

TAI      = 0.5 * EAI + LAI
LAI      = INTGRL(ILAI, RLAI)
RLAI     = GLAI - DLAI
CALL GLA(TIME, DOYEM, DTEFF, DVS,           ...
          RGRL, DELT, SLA, LAI, GLV,         GLAI)
PARAMETER RGRL = 0.009
PARAMETER SLA  = 0.022

```

This part is described in more detail in Chapter 5 in Goudriaan & van Laar (1994). The area of green leaves is the major determinant for light absorption and CO_2 assimilation of the crop, but in wheat half of the Ear Area Index (EAI) also contributes. The Leaf Area Index (LAI , $\text{m}^2 \text{ m}^{-2}$) follows from the balance between growth rate ($GLAI$, $\text{m}^2 \text{ m}^{-2} \text{ d}^{-1}$), and senescence rate ($DLAI$, $\text{m}^2 \text{ m}^{-2} \text{ d}^{-1}$).

$GLAI$ is calculated, depending on the phenological development stage, in the Subroutine GLA . Before seedling emergence ($TIME < DOYEM$), GLA equals zero. After emergence, light intensity and temperature are the environmental factors influencing the rate of leaf area expansion.

During juvenile growth, temperature is the overriding factor, as the rate of leaf appearance and final leaf size are constrained by temperature through its effect on cell division and extension, rather than by the supply of assimilates. In these early stages, leaf area increases approximately exponentially over time. Examination of unpublished field data suggests that a safe approximation is to restrict the exponential phase to the situation where $LAI < 0.75$ and/or $DVS < 0.3$. Exponential leaf area development is described by:

$$LAI(t+DELT) = LAI(t) * \exp(RGRL * DTEFF * DELT)$$

so that the rate of increase in leaf area during juvenile growth is:

$$\begin{aligned}
 GLA &= LAI(t + DELT) - LAI(t) \\
 &= LAI(t) * (\exp(RGRL * DTEFF * DELT) - 1.) / DELT
 \end{aligned}$$

where $LAI(t)$ is the current leaf area, $RGRL$ is the relative growth rate of leaf area per degree-day ($^{\circ}\text{Cd}^{-1}$), $DELT$ is the time step of integration (d) and $DTEFF$ is the daily effective temperature ($^{\circ}\text{C}$).

In later development stages, leaf area expansion is increasingly restricted by assimilate supply. Branching and tillering generate an increasing number of sites per plant where leaf initiation can take place and mutual shading of plants further reduces the assimilate supply per growing point. During this stage ($LAI > 0.75$ and $DVS > 0.3$), the model calculates the growth of leaf area by multiplying the simulated increase in leaf weight (GLV) by the specific leaf area of new leaves (SLA , $m^2 g^{-1}$).

```

EAI          = INTGRL(IEAI, REAI)
CALL SUBEAI (DELT,DVS,EAR,TADRW,RDRDV,EAI, REAI)
PARAMETER EAR    = 0.63E-3

```

The ear area index (EAI , m^2 ears ($2 \times$ one-sided projection) m^{-2}) is set to zero for $DVS < 0.8$, and is calculated in the Subroutine SUBEAI. At $DVS = 0.8$, EAI is set to a fixed proportion, the Ear Area Ratio (EAR , m^2 ear g^{-1} dry matter) of the total above-ground dry matter ($TADRW$, $g m^{-2}$). Till $DVS = 1.3$, EAI remains at this value, and decreases subsequently.

```

DLAI         = LAI * RDR
RDR           = MAX(RDRDV, RDRSH)
RDRDV        = INSW(DVS-1.0, 0., DVR/(MAX(0.1, 2.-DVS))*FRDR)
RDRSH        = LIMIT(0., 0.03, 0.03 * (LAI-LAICR) / LAICR)
PARAMETER LAICR = 4.0 ; FRDR = 1.

```

The senescence rate of LAI ($DLAI$, $m^2 m^{-2} d^{-1}$) is described on the basis of a relative death rate (RDR , d^{-1}), set at the maximum of a relative death rate due to ageing ($RDRDV$) and one due to self-shading, $RDRSH$. The latter equals zero for LAI smaller than 4, and increases linearly with increasing LAI till a maximum value of 0.03 at $LAI = 8$ (the meaning of the `LIMIT` function in combination with $LAICR = 4.$, see Appendix II).

$RDRDV$ equals zero for $DVS < 1$ (pre-anthesis stage) and subsequently increases with DVS . The parameter $FRDR$ determines the rate at which RDR increases. For $FRDR = 1.$, LAI decreases linearly with DVS .

```

DLV          = WLVG * DLAI/NOTNUL(LAI)

```

The death rate of leaves (DLV , $g m^{-2} d^{-1}$) is defined as the relative senescence rate of LAI times the weight of the green leaves ($WLVG$), the `NOTNUL` function prevents division by zero.

1.11. Dry matter production

```

WRT          = INTGRL(WRTI, GRT)
WLVG         = INTGRL(WLVI, RWLVG)
RWLVG        = GLV - DLV
WLVD         = INTGRL(WLVDI, DLV)
WST          = INTGRL(WSTI, GST)
WSO          = INTGRL(WSOI, GSO)

```

Dry weights of the various plant organs (roots (WRT , $g m^{-2}$), green leaves ($WLVG$, $g m^{-2}$), dead leaves ($WLVD$, $g m^{-2}$), stems (WST , $g m^{-2}$), storage organs (WSO , $g m^{-2}$)) are obtained through integration of the respective growth rates.

```

WLV      = WLVG  + WLVD
TADRW    = WLV   + WST  + WSO
TDRW     = TADRW + WRT

```

Some totals of dry matter production are calculated and included in the output.

```

HI      = WSO / NOTNUL(TADRW)

```

The harvest index (HI) is the weight of the grains divided by total above-ground biomass.

1.12. Weather data

```

DTR      = AFGEN(DTRT, DAY) * 1.E06

```

This part is described in more detail in Chapter 3 and Appendix 5 in Goudriaan & van Laar (1994). Actual daily total global radiation (DTR , $J\ m^{-2}\ d^{-1}$, the factor 1.E06 converts MJ into J) is read from the function $DTRT$ which contains measured values for solar radiation (400 - 2000 nm) in $MJ\ m^{-2}\ d^{-1}$ for all days of the year.

```

DTMAX    = AFGEN(TMAXT, DAY)
DTMIN    = AFGEN(TMINT, DAY)
DAVTMP   = 0.5 * (DTMAX + DTMIN)
DDTMP    = DTMAX - 0.25 * (DTMAX-DTMIN)

```

Daily maximum and minimum temperatures ($DTMAX$ and $DTMIN$, respectively, °C) are read from the functions $TMAXT$ and $TMINT$ containing measured values for all days of the year. For daytime temperature ($DDTMP$) we use an approximate formula (see also Chapter 3 in Goudriaan & van Laar, 1994). Weather data are read from tables with 365 data pairs each. The independent variable is the current day number of the year (DAY).

```

DTEFF    = MAX(0., DAVTMP-TBASE)
PARAMETER TBASE = 0.

```

Since many growth processes are temperature dependent above a certain threshold temperature, an effective temperature ($DTEFF$) is calculated. For spring wheat, the threshold value is 0 °C. Weather data given in the model are monthly averages (defined at the middle of each month) for Wageningen (The Netherlands), averaged over the years 1951 - 80.

```

FUNCTION DTRT = 15., 2.1, 46., 4.4, 74., 7.8, 105.,13.0,...
               135.,16.3, 166.,17.5, 196.,15.6, 227.,13.8, 258.,10.0,...
               288., 5.8, 319., 2.7, 349., 1.7
FUNCTION TMAXT = 15., 4.3, 46., 5.4, 74., 8.9, 105.,12.4,...
               135.,17.3, 166.,20.5, 196.,21.4, 227.,21.5, 258.,18.9,...
               288.,14.3, 319., 8.6, 349., 5.5
FUNCTION TMINT = 15., -0.7, 46.,-0.6, 74., 1.2, 105., 3.3,...
               135., 7.3, 166.,10.3, 196.,12.2, 227.,12.0, 258., 9.7,...
               288., 6.5, 319., 2.9, 349., 0.6

```

When weather data are read from the AB/TPE standard weather files, the following specifications are given (the 'weather' variable names are reserved names in FST, see Rappoldt & van Kraalingen, 1996):

```
WEATHER WTRDIR='C:\SYS\WEATHER\' , CNTR='NLD' , ISTN=1, IYEAR=1990
* Reading weather data from the weather file:
* RDD      Daily global radiation          J/m2/d
* TMMN      Daily minimum temperature      degree C
* TMMX      Daily maximum temperature      degree C
* LAT       Latitude of the site           degree
* DOY       Daynumber of year              d
```

Behind the WEATHER keyword, assignments should be written for the directory of the weather data files (WTRDIR='directory'), the country code (CNTR='country code'), the station number within the country (ISTN=number) and the year to which the weather data pertain (IYEAR=year). The following adaptations have to be made:

```
DTR      = RDD
DTMAX     = TMMX
DTMIN     = TMMN
```

NOTE: From the weather file the latitude (LAT) and day of year (DOY) are generated, so the variables LATT and DAY have to be taken out of the model. Replace DAY by DOY and LATT by LAT (see call for TOTASS).

1.13. Carbon balance check

The Carbon Balance Check compares the amount of carbon present in all organs at any point in time, with the integral of net carbon assimilation rate (TNASS). This rate consists of gross assimilation (DTGA), minus maintenance respiration (MAINT), minus losses due to growth respiration. These growth respiratory losses are defined as the organ growth rates times their CO₂ production factors (CO2RT, CO2LV, etc.), and in addition the loss (a fraction 1 – CONVL) that occurs during remobilization of stem carbohydrates into glucose.

In practice, the two terms CHKIN and CHKFL should never differ by more than a fraction [10⁻⁶]. A larger relative deviation (mostly of the order of a few per cent) will be a sure signal of omission of a term somewhere in the program (CHKDIF), and the simulation will stop.

```
CHKIN      = WLV*CFLV + WST*CFST + ...
            WRT*CFRT + WSO*CFSO
CHKFL      = TNASS * (12./44.)
TNASS      = INTGRL(TNASSI, RTNASS)
RTNASS     = ((GPHOT - MAINT)*44./30.) - ...
            (GRT*CO2RT + GLV*CO2LV + ...
            (GST+TRANSL)*CO2ST + GSO*CO2SO + ...
            (1.-CONVL)* TRANSL*CFST*44./12.)
CO2RT      = 44./12. * (ASRQRT*12./30. - CFRT)
CO2LV      = 44./12. * (ASRQLV*12./30. - CFLV)
```



```
CO2ST      = 44./12. * (ASRQST*12./30. - CFST)
CO2SO      = 44./12. * (ASRQSO*12./30. - CFSO)
```

```
CHKDIF     = (CHKIN-CHKFL)/NOTNUL(CHKIN)
```

```
FINISH CHKDIF > 0.001
```

```
PARAM CFLV=0.459; CFST=0.494; CFRT=0.467; CFSO=0.471
```

The parameters CFLV, CFST, CFRT and CFSO ($\text{g C g}^{-1} \text{ DM}$) represent the C-contents of leaves, stems, roots and storage organs, respectively.

1.14. Run control

```
DAY        = 1. + AMOD(TIME-1., 365.)
```

(If weather data are read from the AB/TPE standard weather files this statement should be omitted.) In the given example, seedling emergence is at day of the year number 90, i.e. 31 March (PARAMETER DOYEM=90.). Simulation may start earlier and is specified in the TIMER statement (STTIME).

```
FINISH DVS      > 2.
```

The simulation stops when the crop is mature, i.e. at development stage 2.

```
TIMER STTIME    = 80., FINTIM = 300., DELT = 1., PRDEL = 5.
TRANSLATION_GENERAL DRIVER='EUDRIV'
```

Simulation is executed with time steps of one day ($\text{DELT} = 1.$), with rectilinear integration of the rates ($\text{DRIVER} = \text{'EUDRIV'}$). Output is produced every fifth day ($\text{PRDEL} = 5.$). To make sure that the simulation does not continue endlessly due to a mistake (or error) in model formulation, the finish time (FINTIM) is set about 50 days later than the expected maturation date.

```
PRINT DAY,DTR,DVS,TDRW,TADRW,WLVG,WLVD,WLV,WST,...
      WSO,WRT,LAI,EAI,HI,GPHOT,DAYL,...
      DSO,TRANSL,CHKIN,CHKFL,CHKDIF,ERRSH,MAINT
```

In this line any variable can be specified. Values occur for every print interval (PRDEL) in the output file.

```
END           completes the specifications of the model.
STOP          hereafter the subroutines are invoked.
```

```
(SUBROUTINES)
```

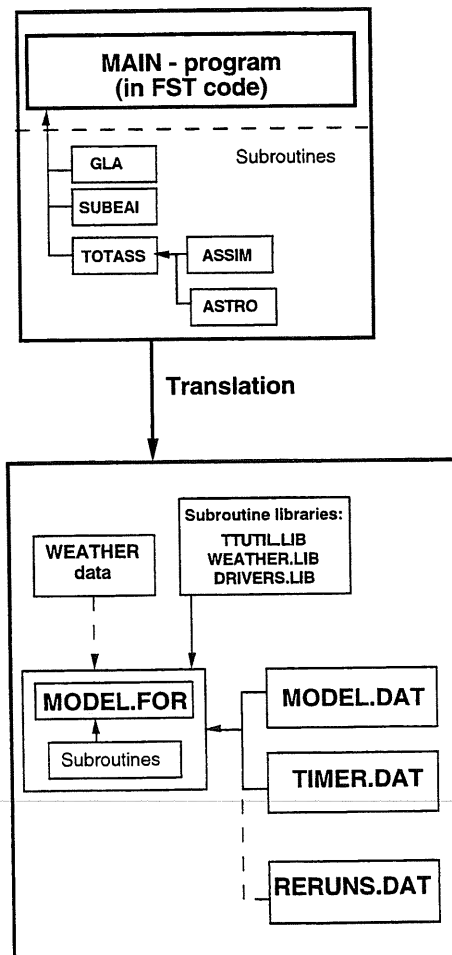
1.15. Subroutines

Subroutines are invoked following the STOP statement.

-
- * Subroutine GLA
- * computes daily increase in leaf area index (LAI, $\text{m}^2 \text{ leaf m}^{-2} \text{ ground d}^{-1}$)
-
- * Subroutine SUBEAI
- * calculates ear area index (EAI)
-
- * Subroutine ASTRO
- * computes daylength and daily extra-terrestrial radiation from day number and latitude
-
- * Subroutine TOTASS
- * computes daily total gross CO_2 assimilation rates (DTGA, $\text{g CO}_2 \text{ m}^{-2} \text{ d}^{-1}$)
-
- * Subroutine ASSIM
- * calculates instantaneous assimilation rates (FGROS, $\text{g CO}_2 \text{ m}^{-2} \text{ s}^{-1}$)
-

The structure of the model:

FST Source
with Subroutines in
FORTRAN77



1.16. Listing of the model SUCROS1

```

DEFINE_CALL GLA      (INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, ...
INPUT, OUTPUT)
DEFINE_CALL SUBEAL (INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, OUTPUT)
DEFINE_CALL TOTASS (INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, ...
OUTPUT, OUTPUT, OUTPUT)

TITLE Crop growth for potential production (SUCROS1)
* Spring wheat, Version September 1997 (SUCROS1_97 V1.0)

* 1.1 INTRODUCTION
*****
* This model for potential crop growth (example: spring wheat)
* is described in:
* J. Goudriaan & H.H. van Laar, 1994. Modelling Potential Crop
* Growth Processes. Textbook with Exercises. Kluwer Academic
* Publishers, Dordrecht, The Netherlands, 238 pp.
*
* Earlier versions of the model are described in:
* H. van Keulen, F.W.T. Penning de Vries & E.M. Drees, 1982.
* A summary model for crop growth. In: Simulation of plant
* growth and crop production. Eds F.W.T. Penning de Vries &
* H.H. van Laar, Simulation Monographs, Pudoc, Wageningen,
* pp. 87-97.
*
* Spitters, C.J.T., H. van Keulen & D.W.G. van Kaaalangen, 1989.
* A simple and universal crop growth model: SUCROS87. In:
* Simulation and systems management in crop protection.
* Eds R. Rabbinge, S.A. Ward & H.H. van Laar, Simulation
* Monographs, Pudoc, Wageningen, pp. 147-181.
*****

* 1.2 INITIAL CONDITIONS
INITIAL
* INCON ZERO = 0.
PARAMETER DOYEM = 90.
INCON WLVI = 0.5; WSTI = 0.3 ; WRTI = 0.8
INCON WLVDI = 0. ; WSOI = 0. ; ILAI = 0.012
INCON IDVS = 0. ; IEAI = 0.

* Initialization of TNASS: total CO2 equivalents initially available
TNASSI = (WLVI*CFLV + WSTI*CFST + WRTI*CFRT) * 44./12.

* 1.3 CROP DEVELOPMENT
DYNAMIC
DVS
DVR = INTGRL(IDVS, DVR)
= INSW(DVS-1., AFGEN(DVRVT, DAVTMP), ...
EMERG = AFGEN(DVRVT, DAVTMP)) * EMERG
FUNCTION DVRVT = -10., 0., 0., 30., 0.027
FUNCTION DVRRT = -10., 0., 0., 30., 0.031

* 1.4 LEAF CO2 ASSIMILATION
AMAX = AMX * AMDVS * AMTMP * EMERG
AMDVS = AFGEN(AMDVST, DVS)
AMTMP = AFGEN(AMTMPT, DDTMP)
PARAMETER AMX = 1.11E-3

* 1.11 milligram CO2/m2/s = 40 kg CO2/ha/h
FUNCTION AMDVST = 0.0, 1.0, 1.0, 1.0, 2.0, 0.5, 2.5, 0.0
FUNCTION AMTMPT = -10., 0., 0., 0., 10., 1., 25., 1., 35., 0., 50., 0.

* 1.5 DAILY GROSS CO2 ASSIMILATION
CALL TOTASS(DOY, LAT, DTR, SCP, AMAX, EFF, KDF, TAI, ...
DAYL, DTGA, DS0)
PARAMETER EFF = 12.5E-6
* 12.5 microgram CO2/J = 0.45 kg (CO2/ha/h)/(J/m2/s)
PARAMETER KDF = 0.60
PARAMETER SCP = 0.20
*PARAMETER LATT = 52.

* 1.6 CARBOHYDRATE PRODUCTION
GPHOT = DTGA * 30./44.

* 1.7 MAINTENANCE RESPIRATION
MAINT = MAINTS * TEFF * MNDVS * EMERG
MAINTS = MAINIV*WLVG + MAINST*WST + MAINRT*WRT + MAINSO*WSO
MNDVS = WLVG / NOTMUL(WLV)
TEFF = Q10**((DAVTMP-TREF)/10.)
PARAMETER Q10 = 2.; TREF = 25.
PARAMETER MAINIV = 0.03; MAINST = 0.015
PARAMETER MAINRT = 0.015; MAINSO = 0.01

* 1.8 DRY MATTER PARTITIONING
FSH = AFGEN(FSHTB, DVS)
FRT = 1. - FSH
FUNCTION FSHTB = 0.00, 0.50, 0.10, 0.50, 0.20, 0.60, 0.35, 0.78, ...
0.40, 0.83, 0.50, 0.87, 0.60, 0.90, 0.70, 0.93, ...
0.80, 0.95, 0.90, 0.97, 1.00, 0.98, 1.10, 0.99, ...
1.20, 1.00, 2.50, 1.00

FLV = AFGEN(FLVTB, DVS)
FUNCTION FLVTB = 0.00, 0.65, 0.10, 0.65, 0.25, 0.70, 0.50, 0.50, ...
0.70, 0.15, 0.95, 0.00, 2.50, 0.00

FST = AFGEN(FSTTB, DVS)
FUNCTION FSTTB = 0.00, 0.35, 0.10, 0.35, 0.25, 0.30, 0.50, 0.50, ...
0.70, 0.85, 0.95, 1.00, 1.05, 0.00, 2.50, 0.00

FSO = AFGEN(FSOTB, DVS)
FUNCTION FSOTB = 0.00, 0.00, 0.95, 0.00, 1.05, 1.00, 2.50, 1.00

ERRSH = ABS(FLV+FST+FSO - 1.)
FINISH ERRSH > 1.E-6

* 1.9 GROWTH OF PLANT ORGANS AND TRANSLOCATION
ASRQ = FSH * (ASRQLV*FLV + ASRQST*FST + ASRQSO*FSO) + ...
ASRQST*FRT
TRANSL = INSW(DVS-1., 0., WST * DVR * FRTRL)

```

```

GTW      = (GPHOT - MAINT + CONVL*TRANSL*CFST*30./12.) / ASRQ
GRT      = FRT * GTW
GLV      = FLV * FSH * GTW
GST      = FST * FSH * GTW - TRANSL
GSO      = FSO * FSH * GTW

* The following values are calculated without
* the costs of nitrate reduction:
PARAMETER ASRORT = 1.444; ASROLV = 1.463
PARAMETER ASRGST = 1.513; ASRQSO = 1.415
PARAMETER FRTSL = 0.20; CONVL = 0.947

* 1.10 LEAF AND EAR DEVELOPMENT

TAI      = 0.5 * EAI + LAI
LAI      = INTGRL(ILAI, RLAI)
RLAI     = GLAI - DLAI
CALL GLA(TIME, DOYEM, DTEFF, DVS, GLAI)
PARAMETER RGRL = 0.009
PARAMETER SLA  = 0.022

EAI      = INTGRL(IEAI, REAI)
CALL SUBEAI(DELT,DVS,EAR,TADRW,RDRDV,EAI, REAI)
PARAMETER EAR  = 0.63E-3

DLAI     = LAI * RDR
RDR      = MAX(RDRDV, RDRSH)
RDRDV   = INSM(DVS-1.0, 0., DVR/(MAX(0.1, 2.-DVS)))*FRDR)
RDRSH   = LIMIT(0., 0.03, 0.03 * (LAI-LAICR) / LAICR)
PARAMETER LAICR = 4.0; FRDR = 1.

DLV      = WLVG * DLAI/NOTNUL(LAI)

* 1.11 DRY MATTER PRODUCTION

WRT      = INTGRL(WRTL, GRT)
WLVG     = INTGRL(WLVL, RWLVG)
RWLVG    = GLV - DLV
WLVD     = INTGRL(WLVDI, DLV)
WST      = INTGRL(WSTI, GST)
WSO      = INTGRL(WSOI, GSO)

WLW      = WLVG + WLVD
TADRW    = WLW + WST + WSO
TDRW     = TADRW + WRT
HI       = WSO / NOTNUL(TADRW)

* 1.12 WEATHER DATA

WEATHER WTRDIR='C:\SYS\WEATHER\';CNTR='NLD';ISTN=1;IYEAR=1990
* Reading weather data from the weather file:
* RDD      Daily global radiation      J/m2/d
* TMN      Daily minimum temperature  degree C
* TMMX     Daily maximum temperature  degree C
* LAT      Latitude of the site        degree
* DOY      Daynumber of year           d

DTR      = RDD
DAVTMP   = 0.5 * (TMMX + TMN)
DDTMP    = TMMX - 0.25 * (TMMX - TMN)
DTEFF    = MAX(0., DAVTMP - TBASE)
PARAMETER TBASE = 0.

* If weather data are not available in AB-TPE format:
* DTR      = AFGEN(DTRT, DAY) * 1.E06
* DTMX     = AFGEN(TMAX, DAY)
* DTMIN    = AFGEN(TMIN, DAY)
* DAVTMP   = 0.5 * (DTMX + DTMIN)
* DDTMP    = DTMX - 0.25 * (DTMX - DTMIN)
* Average weather data for the Netherlands
* FUNCTION DTRT = 15., 2.1, 46., 4.4, 74., 7.8, 105., 13.0, ...
* 135., 16.3, 166., 17.5, 196., 15.6, 227., 13.8, 258., 10.0, ...
* 288., 5.8, 319., 2.7, 349., 1.7
* FUNCTION TMAX = 15., 4.3, 46., 5.4, 74., 8.9, 105., 12.4, ...
* 135., 17.3, 166., 20.5, 196., 21.4, 227., 21.5, 258., 18.9, ...
* 288., 14.3, 319., 8.6, 349., 5.5
* FUNCTION TMIN = 15., -0.7, 46., -0.6, 74., 1.2, 105., 3.3, ...
* 135., 7.3, 166., 10.3, 196., 12.2, 227., 12.0, 258., 9.7, ...
* 288., 6.5, 319., 2.9, 349., 0.6

* 1.13 CARBON BALANCE CHECK

CHKIN    = WLW * CFLV + WST * CFST + ...
WRT      = CFRT + WSO * CFST
CHKFL    = TNASS * (12./44.)
TNASS    = INTGRL(TNASSI, RTNASS)
RTNASS   = ((GPHOT - MAINT)*44./30.) - ...
          (GRT*CO2RT + GLV*CO2LV + ...
          (GST+TRANSL)*CO2ST + GSO*CO2SO + ...
          (1.-CONVL)*TRANSL*CFST*44./12.)
CO2RT    = 44./12. * (ASRQRT*12./30. - CFRT)
CO2LV    = 44./12. * (ASROLV*12./30. - CFLV)
CO2ST    = 44./12. * (ASRQST*12./30. - CFST)
CO2SO    = 44./12. * (ASRQSO*12./30. - CFST)
CHKDIF   = (CHKIN - CHKFL) / NOTNUL(CHKIN)

FINISH   = 0.001
PARAM CFLV=0.459; CFST=0.494; CFRT=0.467; CFSTO=0.471

* 1.14 RUN CONTROL

DAY      = 1. + AMOD(TIME-1., 365.)

FINISH DVS > 2.
TIMER STTIME = 80.; FINTIM = 300.; DELT = 1.; PRDEL = 5.
TRANSLATION_GENERAL DRIVER='EUDRIV'

PRINT DOY,DTR,DVS,TDRW,WLVG,WLVD,WST,...
WSO,WRT,LAI,EAI,HI,GPHOT,DAYL,...
DSO,TRANSL,CHKIN,CHKFL,CHKDIF,ERRSH,MAINT

END
STOP

```

```

* 1.15 SUBROUTINES
*
*-----
* SUBROUTINE GLA
* Purpose: This subroutine computes daily increase of leaf area index
*          (m2 leaf/ m2 ground/ d)
* Version: September 1997 (SUCROS97 V1.0)
*
* FORMAL PARAMETERS: (I=input,O=output,C=control,IN=init,T=time)
* name type meaning units class
*-----
* TIME R4 Time in simulation d T
* DOYEM R4 Day number of crop emergence d T
* DTEFF R4 Daily effective temperature oc I
* DVS R4 Development stage of the crop oc-1 d-1 I
* RGRL R4 Relative leaf growth rate d T
* DELT R4 Time step of integration d T
* SLA R4 Specific leaf area m2 g-1 I
* LAI R4 Leaf area index m2 m-2 I
* GLV R4 Growth rate of the leaves g m-2 d-1 I
* GLAI R4 Growth rate of leaf area index m2 m-2 d-1 O
*
* SUBROUTINE GLA (TIME,DOYEM,DTEFF,DVS,RGRL,DELT,SLA,LAI,GLV,
* $ IMPLICIT REAL (A-Z)
*
*-----growth during maturation stage
* GLAI = SLA * GLV
*
*-----growth during juvenile stage
* IF ((DVS.LT.0.3).AND.(LAI.LT.0.75)) THEN
* GLAI = (LAI * (EXP(RGRL*DTEFF*DELT)-1.))/DELT
* ENDLF
*
*-----growth before seedling emergence
* IF (TIME.LE.DOYEM) GLAI = 0.
*
* RETURN
* END
*
*-----
* SUBROUTINE SUBEAI
* Purpose: This subroutine calculates ear area index
* Version: September 1997 (SUCROS97 V1.0)
*
* FORMAL PARAMETERS: (I=input,O=output,C=control,IN=init,T=time)
* name type meaning units class
*-----
* DELT R4 Time step of integration d T
* DVS R4 Development stage of the crop - I
* EAR R4 Ear area/weight ratio g m-2 I
* TADRW R4 Total above-ground dry weight g m-2 I
* RDR R4 Relative death rate d-1 I
* EAI R4 Ear area index m2 m-2 I
* REAI R4 Growth rate ear area index m2 m-2 d-1 O
*
* SUBROUTINE SUBEAI (DELT,DVS,EAR,TADRW,RDRDV,EAI, REAI)
* IMPLICIT REAL(A-Z)

```

```

IF (DVS.LT.0.8) REAI = 0.
IF (DVS.GE.0.8 .AND. EAI.EQ.0.) THEN
  REAI = (EAR * TADRW)/DELT
ELSE
  REAI = 0.
ENDIF
IF (DVS.GE.1.3) REAI = -RDRDV * EAI
RETURN
END
*
*-----
* SUBROUTINE ASTRO
* Purpose: This subroutine calculates astronomic daylength,
*          diurnal radiation characteristics such as the daily
*          integral of sine of solar elevation and solar constant.
* Version: September 1997 (SUCROS97 V1.0)
*
* FORMAL PARAMETERS: (I=input,O=output,C=control,IN=init,T=time)
* name type meaning units class
*-----
* DOY R4 Daynumber (Jan 1st = 1) - T
* LAT R4 Latitude of the site degrees I
* SC R4 Solar constant J m-2 s-1 O
* DS0 R4 Daily extraterrestrial radiation J m-2 d-1 O
* SINLD R4 Seasonal offset of sine of solar height - O
* COSLD R4 Amplitude of sine of solar height - O
* DAYL R4 Astronomic daylength (base = 0 degrees) h O
* DSINB R4 Daily total of sine of solar height s O
* DSINBE R4 Daily total of effective solar height s O
*
* FATAL ERROR CHECKS (execution terminated, message)
* Condition: LAT > 67, LAT < -67
*
* SUBROUTINE ASTRO (DOY, LAT,
* $ SC, DS0, SINLD, COSLD, DAYL, DSINB, DSINBE)
* IMPLICIT REAL (A-Z)
*
*-----PI and conversion factor from degrees to radians
* PI = 3.141592654
* RAD = PI/180.
*
*-----check on input range of parameters
* IF (LAT.GT.67.) STOP 'ERROR IN ASTRO: LAT> 67'
* IF (LAT.LT.-67.) STOP 'ERROR IN ASTRO: LAT<-67'
*
*-----declination of the sun as function of daynumber (DOY)
* DEC = -ASIN (SIN (23.45*RAD)*COS (2.*PI*(DOY+10.)/365.))
*
*-----SINLD, COSLD and AOB are intermediate variables
* SINLD = SIN (RAD*LAT)*SIN (DEC)
* COSLD = COS (RAD*LAT)*COS (DEC)
* AOB = SINLD/COSLD
*
*-----daylength (DAYL)
* DAYL = 12.0*(1.+2.*ASIN (AOB)/PI)
*
* DSINB = 3600.*(DAYL*SINLD+24.*COSLD*SQRT (1.-AOB*AOB)/PI)
* DSINBE = 3600.*(DAYL*(SINLD+0.4*(SINLD*SINLD+COSLD*COSLD*0.5))+)

```

```

      &      12.0*COSLD*(2.0+3.0*0.4*SINLD)*SQRT (1.-AOB*AOB)/PI)
*-----solar constant (SC) and daily extraterrestrial radiation (DS0)
SC = 1370.*(1.+0.033*COS (2.*PI*DOY/365.))
DS0 = SC*DSINB
      RETURN
      END

*-----SUBROUTINE TOTASS
* Purpose: This subroutine calculates daily total gross
* assimilation (DTGA) by performing a Gaussian integration
* over time. At three different times of the day,
* radiation is computed and used to determine assimilation
* whereafter integration takes place.
* Version: September 1997 (SUCROS97 V1.0)
* FORMAL PARAMETERS: (I=input,O=output,C=control,IN=init,T=time)
* name type meaning units class
*-----
DOY R4 Day number (January 1 = 1) - T
LAT R4 Latitude of the site degrees I
DTR R4 Daily total of global radiation J/m2/d I
SCP R4 Scattering coefficient of leaves for visible I
AMAX R4 Assimilation rate at light saturation g CO2/ m2 leaf/s
EFF R4 Initial light conversion factor g CO2/J I
KDF R4 Extinction coefficient diffuse flux leaves - I
LAI R4 Leaf area index as used for photosynthesis m2/m2 I
      Note: This can involve stem, flower or
      ear area index!!
DAYL R4 Astronomic daylength (base = 0 degrees) h O
DTGA R4 Daily total gross assimilation g CO2/m2/d O
DS0 R4 Daily extraterrestrial radiation J/m2/s O
*-----SUBROUTINES called : ASTRO, ASSIM
*-----
SUBROUTINE TOTASS (DOY, LAT, DTR, SCP, AMAX, EFF, KDF, LAI,
& DAYL, DTGA, DS0)
      IMPLICIT REAL(A-Z)
      REAL XGAUSS(3), WGAUSS(3)
      INTEGER I1, IGAUSS
      DATA IGAUSS /3/
      DATA XGAUSS /0.112702, 0.500000, 0.887298/
      DATA WGAUSS /0.277778, 0.444444, 0.277778/
      PI = 3.141592654
      CALL ASTRO(DOY,LAT,SC,DS0,SINLD,COSLD,DAYL,DSINB,DSINBE)
*-----assimilation set to zero and three different times of the day (HOUR)
DTGAS = 0.
      DO 10 I1=1, IGAUSS
*-----at the specified HOUR, radiation is computed and used to compute

```

```

*      assimilation
      HOUR = 12.0*DAYL*0.5*XGAUSS(I1)
*-----sine of solar elevation
      SINB = MAX (0., SINLD+COSLD*COS (2.*PI*(HOUR+12.)/24.))
*-----diffuse light fraction (PRDF) from atmospheric
      transmission (ATWTR)
      PAR = 0.5*DTR*SINB*(1.+0.4*SINB)/DSINBE
      ATWTR = PAR/(0.5*SC*SINB)
      IF (ATWTR.LE.0.22) THEN
        PRDF = 1.
      ELSE IF (ATWTR.GT.0.22 .AND. ATWTR.LE.0.35) THEN
        PRDF = 1.-6.4*(ATWTR-0.22)**2
      ELSE
        PRDF = 1.47-1.66*ATWTR
      END IF
      PRDF = MAX (PRDF, 0.15+0.85*(1.-EXP (-0.1/SINB)))
*-----diffuse PAR (PARDF) and direct PAR (PARDR)
      PARDF = PAR * PRDF
      PARDR = PAR - PARDF
      CALL ASSIM (SCP,AMAX,EFF,KDF,LAI,SINB,PARDR,PARDF,FGROS)
*-----integration of assimilation rate to a daily total (DTGA)
      DTGAS = DTGAS+FGROS*WGAUSS(I1)
10 CONTINUE
      DTGA = DTGAS * DAYL * 3600.
      RETURN
      END
*-----SUBROUTINE ASSIM
* Purpose: This subroutine performs a Gaussian integration over
* depth of canopy by selecting five different LAI's and
* computing assimilation at these LAI levels. The
* integrated variable is FGROS.
* Version: September 1997 (SUCROS97 V1.0)
* FORMAL PARAMETERS: (I=input,O=output,C=control,IN=init,T=time)
* name type meaning units class
*-----
SCP R4 Scattering coefficient of leaves for visible g CO2/ I
AMAX R4 Assimilation rate at light saturation m2 leaf/s I
EFF R4 Initial light conversion factor g CO2/J I
KDF R4 Extinction coefficient diffuse flux leaves - I
LAI R4 Leaf area index as used for photosynthesis m2/m2 I
      Note: This can involve stem, flower or
      ear area index!!
SINB R4 Sine of solar height I
PARDR R4 Instantaneous flux of direct radiation (PAR) W/m2 I
PARDF R4 Instantaneous flux of diffuse radiation (PAR) W/m2 I
FGROS R4 Instantaneous assimilation rate of g CO2/ O

```

```

*          whole canopy          m2 soil/s          *
*-----*-----*-----*
SUBROUTINE ASSIM (SCP, AMAX, EFF, KDF, LAI, SINB, PARDR, PARDF,
& IMPLICIT REAL(A-Z)
REAL XGAUSS(5), WGAUSS(5)
INTEGER I1, I2, IGAUSS

*-----Gauss weights for five point Gauss
DATA IGAUSS /5/
DATA XGAUSS /0.0469101,0.2307534,0.5,0.7692465,0.9530899/
DATA WGAUSS /0.1184635,0.2393144,0.2844444,0.2393144,0.1184635/

*-----reflection of horizontal and spherical leaf angle distribution
SQV = SQRT(1.-SCP)
REFH = (1.-SQV)/(1.+SQV)
REFS = REFH*2./(1.+2.*SINB)

*-----extinction coefficient for direct radiation and total direct flux
CLUSTF = KDF / (0.8*SQV)
KBL = (0.5/SINB) * CLUSTF
KDRT = KBL * SQV

*-----selection of depth of canopy, canopy assimilation is set to zero
FGROS = 0.

DO 10 I1=1, IGAUSS
  LAIC = LAI * XGAUSS(I1)

  *-----absorbed fluxes per unit leaf area: diffuse flux, total direct
  * flux, direct component of direct flux.
  VISDF = (1.-REFH)*PARDF*KDF *EXP (-KDF *LAIC)
  VIST = (1.-REFS)*PARDR*KDRT *EXP (-KDRT *LAIC)
  VISD = (1.-SCP) *PARDR*KBL *EXP (-KBL *LAIC)

  *-----absorbed flux (J/M2 leaf/s) for shaded leaves and assimilation of
  * shaded leaves
  VISSHD = VISDF + VIST - VISD
  IF (AMAX.GT.0.) THEN
    FGRSH = AMAX * (1.-EXP(-VISSHD*EFF/AMAX))
  ELSE
    FGRSH = 0.
  END IF

  *-----direct flux absorbed by leaves perpendicular on direct beam and
  * assimilation of sunlit leaf area
  VISPP = (1.-SCP) * PARDR / SINB
  FGRSUN = 0.
  DO 20 I2=1, IGAUSS
    VISSUN = VISSHD + VISPP * XGAUSS(I2)
    IF (AMAX.GT.0.) THEN
      FGRS = AMAX * (1.-EXP(-VISSUN*EFF/AMAX))
    ELSE
      FGRS = 0.
    END IF
    FGRSUN = FGRSUN + FGRS * WGAUSS(I2)
  20 CONTINUE

  *-----fraction sunlit leaf area (FSLLA) and local assimilation

```

```

*          rate (FGL)
FSLLA = CLUSTF * EXP(-KBL*LAIC)
FGL = FSLLA * FGRSUN + (1.-FSLLA) * FGRSH

*-----integration of local assimilation rate to canopy
* assimilation (FGROS)
FGROS = FGROS + FGL * WGAUSS(I1)

10 CONTINUE
FGROS = FGROS * LAI
RETURN
END

```


2. Crop growth model for water-limited conditions (SUCROS2)

H. van Keulen, J. Goudriaan, L. Stroosnijder, E.A. Lantinga & H.H. van Laar

2.1. Introduction

SUCROS2 describes production (here applied to spring wheat) under water-limited conditions by including water balances of crop and soil in the SUCROS1 model (see Figure 2.1). Conditions are still optimal with respect to other growth factors, i.e. ample nutrients and a pest-, disease- and weed-free environment. With the SUCROS2 model, effects of temporary water shortage and options for soil and water conservation can be studied. The crop / soil water balances in SUCROS2 are based on earlier versions documented by Stroosnijder (1982) and Penning de Vries *et al.* (1989). SUCROS2 only allows for effects of water stress that are mediated through a) photosynthesis and b) altered root/shoot partitioning. Other, possibly important, effects remain to be included such as increased leaf senescence and abscission, changes in harvest index and suppressed tillering.

SUCROS2 can only be understood on the basis of SUCROS1, the crop growth model for potential production described in Chapter 1. The effect of inadequate moisture supply is transmitted through two variables, one acting on daily gross CO₂ assimilation and the other on root-shoot partitioning.

In Sections 2.2-2.22 of this report, the explanatory text follows as closely as possible the computer listing of the model, i.e. each section starts with a number of lines copied from this listing. In the following texts, the acronyms are explained and the units of all variables and data are treated. Another feature is that parameter and function values are defined directly after they are used for the first time. In this way, it is indicated where the model depends on user-specified input, emphasizing that the accuracy of model results not only depends on correct understanding and description of the processes involved, but also on availability and quality of the input data. The way in which SUCROS2

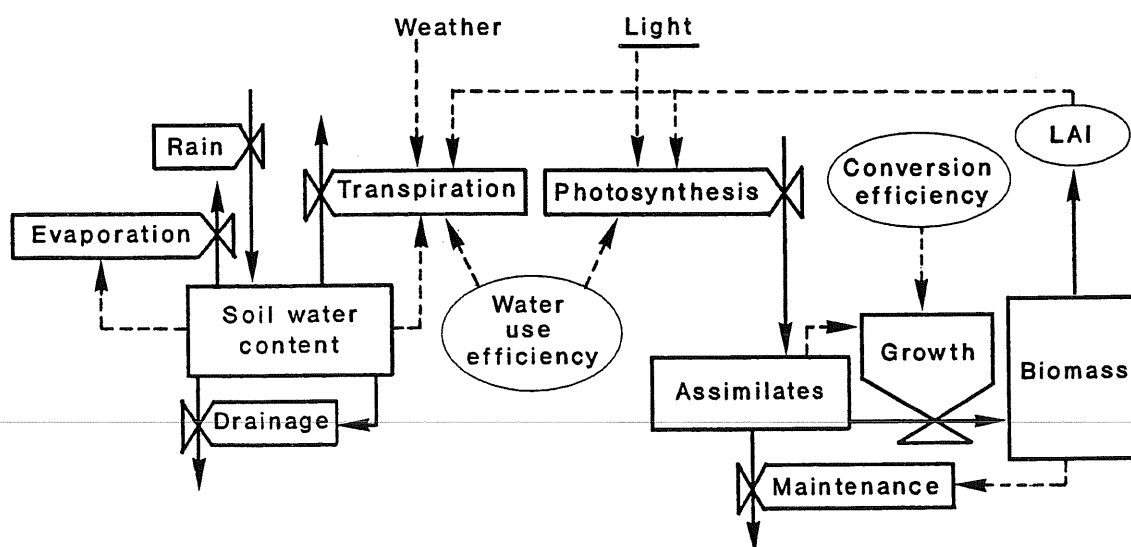


Figure 2.1. Relational diagram of a system, where water is limiting crop growth at least part of the growing season.

is presented here, is different from the modular structure of most current models in which separate data blocks for soil, crop and climate are added at the end of a main program.

In Sections 2.2-2.12, only differences between SUCROS2 and SUCROS1 will be discussed.

FST requires, before the program starts, a definition of the call for subroutines that are used in the program. All variables in the subroutine-call have to be defined as input or output variables. In addition to SUCROS1 the subroutines SUBGRT and SUBFR are needed in SUCROS2.

```
DEFINE_CALL GLA      (INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, ...
                     INPUT,          OUTPUT)
DEFINE_CALL SUBEAI (INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT,  OUTPUT)
DEFINE_CALL TOTASS (INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, ...
                     OUTPUT, OUTPUT, OUTPUT)
DEFINE_CALL SUBGRT (INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, ...
                     INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT,  OUTPUT)
DEFINE_CALL SUBFR  (INPUT, INPUT, INPUT, INPUT, INPUT, INPUT, INPUT,  OUTPUT)
```

TITLE Crop growth for water-limited production (SUCROS2)

* Spring wheat, Version September 1997 (SUCROS2_97 V1.0)

2.2. Initial conditions

INITIAL

```
INCON ZERO      = 0.
PARAMETER DOYEM = 90.
INCON WLVI      = 0.5;   WSTI = 0.3; WRTI = 0.8
INCON WLVDI     = 0. ;   WSOI = 0. ; ILAI = 0.012
INCON IDVS      = 0. ;   IEAI = 0.

INCON ZRTI      = 5.
      WL1I      = WCLI1 * TKL1
      WL2I      = WCLI2 * TKL2
      WL3I      = WCLI3 * TKL3
      WL4I      = WCLI4 * TKL4
PARAM WCLI1     = 0.2;   WCLI2 = 0.2; WCLI3 = 0.2; WCLI4 = 0.2
PARAM TKL1      = 200.; TKL2  = 400.; TKL3  = 600.; TKL4  = 800.
      TKLT      = TKL1 + TKL2 + TKL3 + TKL4
      WCUMI     = WL1I + WL2I + WL3I + WL4I

INCON IDSLR     = 1.
PARAM MDRATE    = 50.
```

ZRTM = MIN(ZRTMC, ZRTMS, TKLT)

PARAMETER ZRTMS = 1200.

PARAMETER ZRTMC = 1200.

* Initialization of TNASS: total CO2 equivalents initially available

TNASSI=(WLVI*CFIV + WSTI*CFST + WRTI*CFRT) * 44./12.

In addition to the statements explained in SUCROS1, a number of additional initial conditions are specified.

ZRTI (in mm) is the rooted depth (Section 2.15) at emergence (i.e. DOYEM). WCLI1, WCLI2, WCLI3 and WCLI4 are the initial moisture contents ($\text{cm}^3 \text{cm}^{-3}$) in the four soil layers distinguished in this model (Section 2.14). Model results are rather sensitive to these initial values because they define the available moisture reserves in the soil. It is, therefore, advisable to start model execution well before the emergence date (in (semi-)arid regions before the onset of the rainy season), so that realistic values for initial moisture conditions can be defined. If measured values at emergence are available, they can be directly incorporated.

In the given example, where the total depth of the soil profile (sum of TKL1, TKL2, TKL3 and TKL4) is 2000 mm (Subsection 2.14.1), the amount of stored water (WCUMI) is 400 mm. When all layers are at wilting point (Sections 2.14 and 2.18) the profile contains 150 mm of water. Hence, at the start of the simulation, the profile contains 250 mm (400-150) crop available water.

The model takes for the maximum rooted depth (ZRTM) the minimum of the values set by soil properties (ZRTMS, mm), crop characteristics (ZRTMC, mm), or total soil depth defined in the model (TKLT, mm), see also Subsection 2.15.3.

2.3. Crop development

DYNAMIC

```
DVS          = INTGRL(IDVS, DVR)
DVR          = INSW(DVS-1., AFGEN(DVRVT, DAVTMP), ...
                  AFGEN(DVRRT, DAVTMP)) * EMERG
EMERG        = INSW(TIME-DOYEM, 0., 1.)
FUNCTION DVRVT = -10.,0., 0.,0., 30.,0.027
FUNCTION DVRRT = -10.,0., 0.,0., 30.,0.031
```

For explanation see page 3.

2.4. Leaf CO₂ assimilation

```
AMAX         = AMX * AMDVS * AMTMP * EMERG
AMDVS        = AFGEN(AMDVST, DVS)
AMTMP        = AFGEN(AMTMPT, DDTMP)
PARAMETER AMX = 1.11E-3
* 1.11 milligram CO2/m2/s = 40 kg CO2/ha/h
FUNCTION AMDVST = 0.0,1.0, 1.0,1.0, 2.0,0.5, 2.5,0.0
FUNCTION AMTMPT = -10.,0., 0.,0., 10.,1., 25.,1., 35.,0., 50.,0.
```

For explanation see page 4.

2.5. Daily gross CO₂ assimilation

```
CALL TOTASS(DOY, LAT, DTR, SCP, AMAX, EFF, KDF, TAI, ...
            DAYL, DTGA, DS0)
PARAMETER EFF = 12.5E-6
```

```
* 12.5 microgram CO2/J = 0.45 (kg CO2/ha/h) / (J/m2/s)
PARAMETER KDF      = 0.60
PARAMETER SCP      = 0.20
*PARAMETER LATT    = 52.
```

For explanation see page 4.

2.6. Carbohydrate production

```
GPHOT      = DTGA * PCEW * 30./44.
```

PCEW is a factor that accounts for reduced photosynthesis due to water stress; its value is calculated in Section 2.18.

For more explanation see page 5.

2.7. Maintenance respiration

```
MAINT      = MAINTS * TEFF * MNDVS * EMERG
MAINTS     = MAINLV*WLVG + MAINST*WST + MAINRT*WRT + MAINSO*WSO
MNDVS      = WLVG / NOTNUL(WLV)
TEFF       = Q10**((DAVTMP-TREF)/10.)
PARAMETER Q10 = 2.;    TREF = 25.
PARAMETER MAINLV = 0.03; MAINST = 0.015
PARAMETER MAINRT = 0.015; MAINSO = 0.01
* Maintenance parameters are expressed in g glucose per g dry matter per day
```

For explanation see page 5.

2.8. Dry matter partitioning

```
FSHP       = AFGEN(FSHTB, DVS)
FSH        = (FSHP * CPEW) / (1. + (CPEW-1.) * FSHP)
FRT        = 1. - FSH
FUNCTION FSHTB = 0.00,0.50, 0.10,0.50, 0.20,0.60, 0.35,0.78,...
               0.40,0.83, 0.50,0.87, 0.60,0.90, 0.70,0.93,...
               0.80,0.95, 0.90,0.97, 1.00,0.98, 1.10,0.99,...
               1.20,1.00, 2.50,1.00

FLV        = AFGEN(FLVTB, DVS)
FST        = AFGEN(FSTTB, DVS)
FSO        = AFGEN(FSOTB, DVS)
FUNCTION FLVTB = 0.00,0.65, 0.10,0.65, 0.25,0.70, 0.50,0.50,...
               0.70,0.15, 0.95,0.00, 2.50,0.00
FUNCTION FSTTB = 0.00,0.35, 0.10,0.35, 0.25,0.30, 0.50,0.50,...
               0.70,0.85, 0.95,1.00, 1.05,0.00, 2.50,0.00
```

```
FUNCTION FSOTB = 0.00,0.00, 0.95,0.00, 1.05,1.00, 2.50, 1.00
```

```
ERRSH = ABS (FLV + FST + FSO - 1.)
FINISH ERRSH > 1.E-6
```

CPEW is a factor accounting for the effect of water stress on dry matter partitioning, leading to higher investments in the root; its value is calculated in Section 2.18 (Subsection 2.18.3).

For more explanation see page 6.

2.9. Growth of plant organs and translocation

```
ASRQ = FSH * (ASRQLV*FLV + ASRQST*FST + ASRQSO*FSO) + ...
      ASRQRT*FRT
```

```
TRANSL = INSW(DVS-1., 0., WST * DVR * FRTRL)
```

```
GTW = (GPHOT - MAINT + CONVL*TRANSL*CFST*30./12.) / ASRQ
GRT = FRT * GTW
GLV = FLV * FSH * GTW
GST = FST * FSH * GTW - TRANSL
GSO = FSO * FSH * GTW
```

* The following values are calculated without
* the costs of nitrate reduction:

```
PARAMETER ASRQRT = 1.444; ASRQLV = 1.463
PARAMETER ASRQST = 1.513; ASRQSO = 1.415
PARAMETER FRTRL = 0.20 ; CONVL = 0.947
```

For explanation see page 6.

2.10. Leaf and ear development

```
TAI = 0.5 * EAI + LAI
LAI = INTGRL(ILAI, RLAI)
RLAI = GLAI - DLAI
CALL GLA (TIME, DOYEM, DTEFF, DVS, ...
          RGRL, DELT, SLA , LAI, GLV, GLAI)
PARAMETER RGRL = 0.009
PARAMETER SLA = 0.022

EAI = INTGRL(IEAI, REAI)
CALL SUBEAI (DELT, DVS, EAR, TADRW, RDRDV, EAI, REAI)
PARAMETER EAR = 0.63E-3

DLAI = LAI * RDR
RDR = MAX (RDRDV, RDRSH)
```

```

RDRDV      = INSW(DVS-1.0, 0., DVR/(MAX(0.1, 2.-DVS))*FRDR)
RDRSH      = LIMIT(0., 0.03, 0.03 * (LAI-LAICR) / LAICR)
PARAMETER LAICR = 4.0 ; FRDR = 1.

```

```
DLV        = WLVG * DLAI/NOTNUL(LAI)
```

For explanation see pages 7 and 8.

2.11. Dry matter production

```

WLVG       = INTGRL(WLVI, RWLVG)
RWLVG      = GLV - DLV
WLVD       = INTGRL(WLVDI, DLV)
WST        = INTGRL(WSTI, GST)
WRT        = INTGRL(WRTI, GRT)
WSO        = INTGRL(WSOI, GSO)

```

```

WLW        = WLVG + WLVD
TADRW      = WLW + WST + WSO
TDRW       = TADRW + WRT

```

```
HI         = WSO / NOTNUL(TADRW)
```

For explanation see page 8.

2.12. Weather data

```
WEATHER WTRDIR='C:\SYS\WEATHER\';CNTR='NLD';ISTN=1;IYEAR=1990
```

* Reading weather data from the weather file:

```

* RDD      Daily global radiation      J/m2/d
* TMMN     Daily minimum temperature   degree C
* TMMX     Daily maximum temperature   degree C
* VP       Vapour pressure             kPa
* WN       Wind speed                  m/s
* RAIN     Precipitation               mm/d
* LAT      Latitude of the site         degree
* DOY      Daynumber of year = TIME     d

```

```
DTR        = RDD
```

```
DAVTMP     = 0.5 * (TMMX + TMMN)
```

```
DDTMP      = TMMX - 0.25 * (TMMX-TMMN)
```

```
DTEFF      = MAX(0., DAVTMP-TBASE)
```

```
PARAMETER TBASE = 0.
```

```
AVP        = VP
```

```
WDS        = WN
```

RRAIN = RAIN

TRAIN = INTGRL(ZERO, RRAIN)

In addition to the variables explained in SUCROS1 (see page 9), actual vapour pressure (AVP, kPa; daily averaged), wind speed (WDS, m s^{-1}) and rainfall (RAIN, mm) are read from the AB/TPE standard weather file NLD1.990. Actual vapour pressure is read in kPa (1 mbar = 100 Pa). Total rainfall (TRAIN) is computed to be included in the output and in the water balance check (Subsection 2.14).

2.13. Penman-Monteith combination equation

2.13.1. Introduction

Strictly speaking, transpiration is the loss of water from the plants, and evaporation is the loss of water from the soil or from a free-water surface. Evapotranspiration covers both transpiration and evaporation.

The principal driving force for evapotranspiration is the gradient of vapour pressure from the evaporating surface to the surrounding air. The vapour pressure at the evaporating surface is assumed to be equal to the saturated vapour pressure at the prevailing temperature of that surface. The vapour pressure in the air is a meteorological variable. The rate of evapotranspiration depends also on the diffusion resistance between the evaporating surface and the air, which is strongly related to wind speed. The two environmental variables, air humidity and wind speed combined determine the 'evaporative demand' of the air or 'drying power' of the air.

The problem in the approach above is that the temperature of the evaporating surface is usually not known from standard meteorological observations. Evapotranspiration of a 1 mm layer of water requires 2.4 MJ m^{-2} of energy and can, therefore, be described through quantification of an energy balance. The energy dissipation required for evapotranspiration leads to cooling of the evaporating surface which reduces the vapour gradient. Hence, a source of power is required to maintain the corresponding surface temperature, and the vapour pressure gradient. This energy is supplied by solar radiation. The net radiation received by the canopy/soil is, therefore, the driving force for evapotranspiration.

Net radiation is the balance between incoming (short-wave) radiation from the sun, corrected for reflection and outgoing (long-wave) radiation. Heat supplied by moving air (advection) is another source of energy, but this is usually negligible, except in situations where the vegetation is surrounded by extensive bare areas (oasis). Only 1% of incoming radiation is dissipated in photosynthesis, which is, therefore, disregarded here. Respiration yields an insignificant amount of energy. To simplify the treatment of evapotranspiration, it is considered to be governed by two factors: radiation and drying power.

Penman (1948) was the first to describe evapotranspiration in physical-mathematical terms. He calculated evapotranspiration from free-water surfaces, bare soil and low grass swards for 10-day periods. There is ongoing discussion in the literature whether his formulae are also applicable if daily values are used. If used with daily values, 24 hour average values should be used. For large day/night differences (e.g. in wind speed), Doorenbos & Kassam (1979) suggested the use of correction factors.

The value calculated according to the Penman equations is the potential evapotranspiration (ET), i.e. without limitations with respect to the supply of liquid water to the evaporating surface. This ET (Penman) value is often used as a reference value, to which actual crop water demand is related.

To translate ET into crop water requirements, so-called crop factors are used (e.g. Doorenbos & Pruitt, 1977; Feddes, 1987). In the model, the following set of equations is used:

$$PENMAN = EVAPR + EVAPD$$

The Penman reference value for potential evapotranspiration ($PENMAN$, mm d^{-1} or $\text{kg H}_2\text{O m}^{-2} \text{d}^{-1}$) is calculated as the sum of two terms, a radiation term ($EVAPR$) and a drying power term ($EVAPD$).

2.13.2. Radiation term

$$\begin{aligned} EVAPR &= (1./LHVAP) * (SLOPE/(SLOPE+PSYCH)) * NRAD \\ SLOPE &= 4158.6 * SVP / (DAVTMP + 239.)^{**2} \\ SVP &= 0.611 * \exp(17.4 * DAVTMP / (DAVTMP + 239.)) \\ \text{PARAMETER LHVAP} &= 2.4E6 \\ \text{PARAMETER PSYCH} &= 0.067 \end{aligned}$$

The radiation term depends on net radiation ($NRAD$, $\text{J m}^{-2} \text{d}^{-1}$), the latent heat of evaporation ($LHVAP$ equal to $2.4 \times 10^6 \text{ J kg}^{-1}$ at 30°C with only a small temperature dependence) and a weighting factor ($SLOPE/(SLOPE+PSYCH)$) in which $SLOPE$ ($\text{kPa } ^\circ\text{C}^{-1}$) is the tangent of the relation between saturated vapour pressure (kPa) and temperature ($^\circ\text{C}$) and $PSYCH$ ($0.067 \text{ kPa } ^\circ\text{C}^{-1}$ at 0 meter elevation) the psychrometer constant (Monteith, 1965).

$SLOPE$ and SVP can be found in look-up tables (check for the correct units!) but here parameterized equations are used.

2.13.3. Net radiation

$$\begin{aligned} NRAD &= (1.-ALB) * DTR - RLWN \\ ALB &= ALBS * \exp(-0.5 * LAI) + 0.25 * (1.-\exp(-0.5 * LAI)) \\ ALBS &= 0.25 * (1.-0.5 * WCL1/WCST1) \end{aligned}$$

Net radiation depends on incoming short-wave radiation (measured DTR , $\text{J m}^{-2} \text{d}^{-1}$), the reflection or albedo value (ALB , unitless), and net outgoing long-wave radiation.

The albedo for the canopy/soil is composed of that for the soil ($ALBS$) and that for the canopy (0.25). The relative contributions of both albedos depend on the shading of the soil by the crop and is calculated on the basis of the leaf area index (LAI). An extinction coefficient (for short-wave radiation penetrating the crop) of 0.5 is used here.

The soil's albedo depends on its surface color and moisture content. Albedo values for dry soil vary from 0.15 (clay) to 0.40 (dune sand). Here, an average value of 0.25 is used. The dependence on soil moisture is described in relation to the average water content of the top soil layer (ten Berge, 1989).

2.13.4. Net long-wave radiation

$$\begin{aligned} RLWN &= BBRAD * FVAP * FCLEAR * 86400. \\ BBRAD &= BOLTZM * (DAVTMP+273.)^{**4} \\ \text{PARAMETER BOLTZM} &= 5.668E-8 \end{aligned}$$


```

FVAP      = 0.56-0.079*SQRT(AVP*10.)
FCLEAR    = 0.1+0.9*CLEAR
CLEAR     = LIMIT(0., 1., ((DTR/DS0)-A)/B)
PARAMETER A = 0.25; B=0.45

```

Net long-wave radiation ($RLWN$, $J\ m^{-2}\ d^{-1}$) is approximated by three semi-empirical functions, (Penman, 1956; derived from the original Brunt (1932) formula), accounting for temperature ($BBRAD$, $J\ m^{-2}\ s^{-1}$), vapour pressure in the atmosphere ($FVAP$, unitless) and sky clearness ($FCLEAR$, unitless). Note that the parameters used in these functions are not unitless so that in the literature a large number of values exist leading to a lot of confusion about the 'Penman' formula. Penman's original sky clearness factor ($CLEAR$, unitless) contains n/N , in which n is the actual sunshine duration ($h\ d^{-1}$), as measured with a Campbell-Stokes solarimeter, and N is the maximum possible sunshine duration (dependent on latitude and time of the year). If n is not available, but DTR instead, the ratio n/N can be estimated from the atmospheric transmission ratio $DTR/DS0$ using the Ångström formula:

$$n/N = (DTR/DS0 - A) / B$$

where A and B are empirical constants (see Table 2.1) and $DS0$ is the extra-terrestrial radiation, i.e. the radiation intensity at the top of the atmosphere, also called Angot's value. Its value depends on location on earth (latitude) and time of the year. Values are usually tabulated (in look-up tables), but can also be calculated using a set of equations as in one of the model's subroutines. The actual vapour pressure (AVP , kPa (daily average)) is read from the meteorological input data. If its value is not known, $FVAP$ can be replaced by the Swinbank equation (Swinbank, 1963), which uses temperature alone. This equation is:

$$FVAP = 1. - 9.35E-6 * (DAVTMP + 273.)^{**2}$$

Table 2.1. Indicative values for empirical constants in the Ångström formula in relation to latitude and climate used by the FAO (Frère & Popov, 1979).

	A	B
Cold and temperate zones	0.18	0.55
Dry tropical zones	0.25	0.45
Humid tropical zones	0.29	0.42

2.13.5. Drying power term

```

WDF      = 2.63 * (1.0 + 0.54 * WDS) * PSYCH
DRYP     = (SVP-AVP) * WDF
EVAPD    = DRYP / (SLOPE+PSYCH)

```

The numerical values in the equation for $DRYP$ ($mm\ d^{-1}\ kPa\ ^\circ C^{-1}$) are not unitless and, therefore, depend on the units of wind speed (WDS) and the vapour pressures, SVP and AVP . The numerical values applied here refer to WDS in $m\ s^{-1}$, measured at a standard height of 2 meter, and SVP and AVP expressed in kPa. The wind function (WDF , $mm\ d^{-1}\ ^\circ C^{-1}$) estimates the conductance for transfer of

latent and sensible heat from the surface to the standard height and depends on roughness of the surface and atmospheric stability. In this model, the wind function for short, closed grass crops is used (Penman, 1956).

2.13.6. Output variables

```

TPENM      = INTGRL(ZERO, PENMAN)
TEVAPR     = INTGRL(ZERO, EVAPR)
TEVAPD     = INTGRL(ZERO, EVAPD)

```

Cumulative potential evapotranspiration since the start of the simulation (TPENM, mm) is computed as well as the cumulative values for the radiation and drying power terms, respectively.

2.14. The soil water balance

The soil water balance is modelled in a simplified way. For a discussion on parametric versus deterministic modelling of the soil water balance reference is made to Stroosnijder (1982). The water balance processes considered are interception, runoff, infiltration, redistribution, external drainage, waterlogging, evaporation and transpiration.

2.14.1. Soil compartments and soil physical characteristics

The root system is usually in contact with various parts of the soil profile that may differ in texture, density and water content. Most soil water balance processes are more intensive near the surface. To take this into account, the soil profile is divided into four layers, called soil compartments. Thickness and physical characteristics of each layer are inputs to the model. The upper layer (TKL1) is set at 200 mm thick, the second (TKL2) at 400 mm, the third (TKL3) at 600 mm, and the fourth (TKL4) at 800 mm. Their sum (TKLT, mm) should at least exceed the maximum rooting depth. The model can easily be extended to account for more heterogeneous situations by increasing the number of compartments and defining specific characteristics for each of them.

For parametric simulation, four specific points of the soil water content - water potential relation (soil moisture characteristic or pF-curve) are needed: the volumetric water contents ($\text{cm}^3 \text{H}_2\text{O cm}^{-3}$ soil) at saturation (WCST), at field capacity (WCFC), at wilting point (WCWP) and when air dry (WCAD).

Soil water content at saturation (WCST) is assumed equal to soil porosity, though some 'entrapped' air may occupy a small part of the pore space. 'Field capacity' is the volumetric water content of the soil after wetting and initial (1 - 3 days) redistribution (Veihmeyer & Hendrickson, 1931). It is often treated as a soil characteristic (van Keulen, 1975; Stroosnijder, 1982; Driessen, 1986; Jansen & Gosseye, 1986), although it also depends on boundary conditions. Field capacity is usually defined as the volumetric water content at a soil moisture suction of 10 kPa or pF 2.0.

As the soil dries out, it becomes increasingly difficult for plants to extract water. At high soil water suctions (the actual value depending on environmental conditions), plants may wilt during the day and recover at night when evaporative demand is low. Above a certain value of moisture suction, plants do not recover at night and wilt permanently. The soil moisture suction then usually has a value of about 1600 kPa or pF 4.2; the value varies among plant species. The volumetric water content at this suction value is called the permanent wilting point (or simply wilting point) of the soil. Its value varies strongly among soil types.

The amount of water available for uptake by the crop is the total amount in the soil, minus that retained at permanent wilting point. The soil water content when air dry is one third or less of that at wilting point. This concept is physically not well-defined, but simulation results are not sensitive to the value of this characteristic. The soil moisture suction of an air dry soil is assumed to be 10^7 mbar or pF 7.0 (van Keulen, 1975).

2.14.2. Interception

```

AINTC      = MIN(RRAIN, INTC*LAI)
PARAMETER INTC = 0.25

```

The amount of rainfall intercepted by the canopy (A_{INTC} , mm d^{-1}) equals the interception capacity per layer of leaves (I_{NTC} , mm d^{-1}) times the leaf area index (LAI). Obviously, this amount can only be intercepted if rainfall intensity (R_{RAIN}) is higher, hence the use of the `MIN` function (Appendix II).

2.14.3. Runoff

```

RNOFF      = MAX(0., 0.15*(RRAIN-AINTC-10.), ...
              RRAIN-AINTC-(WCST1*TKL1-WL1)/(2.*DELT))

```

Not all the water that reaches the surface infiltrates into the soil, especially not during heavy rain. Runoff from a field can be up to 20% of precipitation, and even higher on unfavourable surfaces (Stroosnijder & Koné, 1982) or with large and intense showers. Runoff may be reduced by proper soil management or specific anti-erosion measures such as terracing or ridging. Runoff occurs when the rate of water supply at the soil surface exceeds the infiltration capacity and the excess water accumulated at the soil surface exceeds the surface storage capacity. Infiltration capacity is a function of the water content of the top soil layer. In the model these processes are not described explicitly, because of lack of information, and alternatively an empirical relation between runoff and rainfall is used.

2.14.4. Infiltration

```

WLFL1      = RRAIN-AINTC-RNOFF

```

The infiltration rate (WL_{FL1} , mm d^{-1}) is equal to precipitation minus interception and runoff.

2.14.5. Redistribution

```

WLFL2      = MAX(0., MIN(WL1-WCFC1*TKL1, ...
                          WCST2*TKL2-WL2)/(2.*DELT))
WLFL3      = MAX(0., MIN(WL2-WCFC2*TKL2, ...
                          WCST3*TKL3-WL3)/(2.*DELT))
WLFL4      = MAX(0., MIN(WL3-WCFC3*TKL3, ...
                          WCST4*TKL4-WL4)/(2.*DELT))
WLFL5      = MAX(0., MIN((WL4-WCFC4*TKL4)/(2.*DELT), MDRATE))

```

PARAMETER WCFC1 = 0.23; WCFC2 = 0.23; WCFC3 = 0.23; WCFC4 = 0.23

PARAMETER WCST1 = 0.40; WCST2 = 0.40; WCST3 = 0.40; WCST4 = 0.40

Redistribution of water in the soil can be simulated by using the Richards equation, but the problem is then the small time coefficient, especially near water saturation. In SUCROS2, this problem is circumvented by applying the 'tipping bucket' approach, with a time step of one day. For optimal numerical stability, a drainage coefficient of 0.5 is used. Which means that each day half the surplus water in excess of field capacity is drained to the adjacent lower layer, i.e. WLFL2, WLFL3, WLFL4, WLFL5 (mm d^{-1} , positive in downward direction).

2.14.6. External drainage

DRAIN = WLFL5

If more water enters the deepest layer than can be retained at field capacity, the excess is either drained below the root zone (DRAIN) or fills up the soil compartments above field capacity causing buildup of a perched water table. Drainage is limited by the maximum drainage rate of the subsoil (MDRATE, mm d^{-1}). A high value implies perfect drainage. A low value implies restricted drainage and waterlogged conditions may occur during wet periods. A zero value means no drainage at all (impermeable layer).

Water that cannot drain, fills up the soil layers till saturation. This occurs first in the deepest layer simulating the formation of a perched groundwater table. If still more excess water is to be stored in the soil profile overlying compartments are successively filled up till saturation as well. If the whole soil profile is saturated, water flows over the surface. This parametric way to account for waterlogged conditions will not always be satisfactory. Mechanistic (this parametric method is also dynamic) simulation of waterlogging can be done with a model named SAWAH (ten Berge *et al.*, 1992) when the transport characteristics of the soil are known.

2.14.7. Evaporation and transpiration

The rate of water extraction due to evaporation (EVSU1-4, mm d^{-1}) and transpiration (TRWL1-4, mm d^{-1}) for each of the four layers is calculated later in the model (Sections 2.17 and 2.16, respectively).

2.14.8. Calculation of soil water content

RWL1 = WLFL1 - WLFL2 - EVSW1 - TRWL1

RWL2 = WLFL2 - WLFL3 - EVSW2 - TRWL2

RWL3 = WLFL3 - WLFL4 - EVSW3 - TRWL3

RWL4 = WLFL4 - WLFL5 - EVSW4 - TRWL4

WL1 = INTGRL(WL1I, RWL1)

WL2 = INTGRL(WL2I, RWL2)

WL3 = INTGRL(WL3I, RWL3)

WL4 = INTGRL(WL4I, RWL4)

WCL1 = WL1 / TKL1

WCL2 = WL2 / TKL2

$$\begin{aligned}
WCL3 &= WL3 / TKL3 \\
WCL4 &= WL4 / TKL4 \\
RWCL1 &= (WCL1 - WCWP1) / (WCFC1 - WCWP1) \\
RWCL2 &= (WCL2 - WCWP2) / (WCFC2 - WCWP2) \\
RWCL3 &= (WCL3 - WCWP3) / (WCFC3 - WCWP3) \\
RWCL4 &= (WCL4 - WCWP4) / (WCFC4 - WCWP4)
\end{aligned}$$

First, the amount of water ($WL1-4$, mm) in each of the layers is tracked by integration of all water fluxes into and out of the layers. Then the volumetric water content is computed by dividing the amount of water by the thickness of the respective layers.

Finally the 'relative amount' of crop available water in each of the compartments ($RWCL1-4$, -) is calculated (S in Subsection 2.18.1). These values are used in the calculation of actual transpiration (Subsection 2.16.3).

2.14.9. Output variables

$$\begin{aligned}
TDRAIN &= \text{INTGRL}(\text{ZERO}, \text{DRAIN}) \\
TAINTC &= \text{INTGRL}(\text{ZERO}, \text{AINTC}) \\
TRNOFF &= \text{INTGRL}(\text{ZERO}, \text{RNOFF})
\end{aligned}$$

A number of output variables are computed. Total drainage since the start of the simulation ($TDRAIN$, mm), total interception ($TAINTC$, mm) and total runoff ($TRNOFF$, mm). These variables are also used in the calculation of the water balance of the system.

2.14.10. Checking the balances

$$\begin{aligned}
WCUM &= WL1 + WL2 + WL3 + WL4 \\
CHECK &= \text{TRAIN} + WCUMI - \text{TAINTC} - \text{TRNOFF} - \text{TDRAIN} - \text{WCUM} - \dots \\
&\quad \text{TATRAIN} - \text{TAEVAP}
\end{aligned}$$

Finally, some check values are computed, the total amount of water in the soil profile ($WCUM$, mm) and a check on the water balance ($CHECK$, mm). Ideally, the latter should be zero. For $TATRAIN$ and $TAEVAP$ see Subsections 2.16.5 and 2.17.5, respectively.

2.15. Rooted depth

2.15.1. Introduction

$$ZRT = \text{INTGRL}(ZRTI, EZRT)$$

The rooted depth (ZRT , mm) is defined as the maximum depth from which the crop effectively extracts water. A root density of 0.10 cm root length per cm^3 of soil volume may be adopted as the lower density limit. This is a low value as water is mobile and flows relatively easily to roots. The rooted depth is computed as the integral of the rate of root elongation ($EZRT$, mm d^{-1}) with the initial value of the integral, i.e. rooted depth at emergence ($ZRTI$, mm), defined in the initial section of the model.

2.15.2. Elongation rate of roots

$EZRT = EZRTC * WSERT * AMTMP$

* Temperature effect included, same as for AMAX (AMTMP)

```
CALL SUBGRT (ZRT,ZRTM,DVS,TKL1,TKL2,TKL3,TKL4,WCL1,WCL2,WCL3,WCL4, ...
            WCWP1,WCWP2,WCWP3,WCWP4, WSERT)
```

PARAMETER EZRTC = 12.

The length of fibrous roots can vary enormously without much relation to root weight. Hence, rooted depth is calculated independently of the growth of the root mass. Rooted depth ($EZRTC$) can increase at a maximum rate of 10 - 30 mm d⁻¹, but it is affected by soil physical, soil chemical and biological factors, i.e. for spring wheat a value of 12 mm d⁻¹ is taken (van Keulen & Seligman, 1987).

Root growth generally stops around flowering or earlier if the maximum rooted depth ($ZRTM$) is reached. These limitations are introduced through the function value of $WSERT$.

Low soil temperatures reduce root growth. For conditions with average daytime temperatures between 20 - 30 °C, there is no temperature effect on $EZRT$.

It is assumed that root extension ceases when the root tip reaches a soil compartment with a moisture content at or below wilting point, as described in the self-defined FORTRAN function $WSRT$.

2.15.3. Maximum depth of roots

Roots grow to a certain maximum depth ($ZRTM$, see also Section 2.2) if they are not restricted by soil conditions. The maximum depth depends on plant species ($ZRTMC$) and ranges from 0.5 - 1.5 m or more. Significant differences among cultivars for this characteristic have been reported (Teare & Peet, 1983).

A very dense soil offers mechanical resistance which hampers root extension and reduces the maximum attainable depth. An obvious case is where shallow soil overlies bedrock. High soil densities can also be found at depths of 0.3 - 0.8 m in deep soils, particularly just below the plough layer (hardpan). Its creation may be intentional, such as during soil preparation in irrigated rice where a hardpan is needed to reduce drainage. A compacted layer can also develop unintentionally, such as when harvesting crops with heavy machinery. A physical limitation to rooting depth is approximated by specification of a maximum depth as a soil characteristic ($ZRTMS$).

Sensitivity analysis has established that the maximum rooting depth is an important characteristic, though little is known about it in field crops. Maximum rooting depth should be determined around flowering, i.e. by using root observation tubes (Vos & Groenwold, 1983), or indirectly by monitoring (with neutron probes) the depths from which water is withdrawn in the absence of drainage.

2.16. Transpiration

2.16.1. Introduction

In the model, potential transpiration rate (P_{TRANS} , mm d⁻¹) is calculated on the basis of the Penman-Monteith combination equation. Under ample soil moisture supply, the rate of water uptake follows

this potential rate very closely. However, if insufficient water is available in the soil, uptake cannot meet the demand, i.e. actual transpiration ($ATRANS$, mm d^{-1}) is below the potential and stomata close as a consequence. Transpiration then follows the rate of water uptake.

Water in the crop provides only a small buffer between daily uptake and daily transpiration loss and their daily totals can be considered equal. The ratio $ATRANS/PTRANS$ is an indicator for the degree of water stress under which the crop grows.

Maximum available water in the soil (i.e. all water held between field capacity and wilting point) varies from 0.5 - 2.5 mm water per cm rooted depth for different soils. This implies that, if soil evaporation could be avoided, a C_3 crop could produce 17 - 80 g m^{-2} total dry matter on the water stored in each 10 cm of rooted depth and a C_4 crop about twice as much. Obviously, water stored in the soil provides an important buffer in periods with deficient rainfall. Dry season cropping is, in fact, possible in many climates, provided that at the start there is a wet soil profile and at least 0.5 - 0.7 m of rootable soil profile.

A crop may die from water stress even before the lower soil layer reaches wilting point. The rate at which water is extracted near wilting point is so low that photosynthesis provides insufficient energy for maintenance respiration and the crop dies.

2.16.2. Potential canopy transpiration

$$PTRANS = (1. - \exp(-0.5 \cdot LAI)) \cdot EVAPR + EVAPD \cdot \dots \\ \min(2.0, LAI) - 0.5 \cdot AINTC$$

Only part of the radiation term ($EVAPR$) of potential evapotranspiration will be used by the crop, if not all radiation is intercepted by the canopy, which is exponentially related to leaf area. Radiation not intercepted by the canopy will reach the soil and contribute to potential soil evaporation. The average extinction coefficient for visible and near infrared radiation is about 0.5.

The drying power of the air is only effective up to a cumulative leaf area index of 2. Lower leaves do not contribute much to transpiration because little light penetrates deep into the canopy, hence their stomatal resistance is high. Also air humidity is higher and wind speed is reduced. Potential transpiration is reduced by half (as the average of values 0.3 - 1.0 as reported by Singh & Szeicz (1979)) the amount of interception.

2.16.3. Actual transpiration

```
FUNCTION EDPTFT = -.50,0., -.05,0., 0.,.15, .15,.6, ...
               .3,.8, .5,1., 2.,1.
ERLB          = ZRT1*AFGEN(EDPTFT, RWCL1) +...
               ZRT2*AFGEN(EDPTFT, RWCL2) +...
               ZRT3*AFGEN(EDPTFT, RWCL3) +...
               ZRT4*AFGEN(EDPTFT, RWCL4)
TRRM          = PTRANS/NOTNUL(ERLB)
TRWL1         = TRRM*WSE1*ZRT1*AFGEN(EDPTFT, RWCL1)
TRWL2         = TRRM*WSE2*ZRT2*AFGEN(EDPTFT, RWCL2)
TRWL3         = TRRM*WSE3*ZRT3*AFGEN(EDPTFT, RWCL3)
TRWL4         = TRRM*WSE4*ZRT4*AFGEN(EDPTFT, RWCL4)
ZRT1          = LIMIT(0., TKL1, ZRT)
ZRT2          = LIMIT(0., TKL2, ZRT-TKL1)
```

```

ZRT3      = LIMIT(0.,TKL3,ZRT-TKL1-TKL2)
ZRT4      = LIMIT(0.,TKL4,ZRT-TKL1-TKL2-TKL3)

ATRANS    = TRWL1+TRWL2+TRWL3+TRWL4

```

Uptake of water takes place from the rooted soil volume. To simulate water uptake in semi-arid regions, van Keulen (1975) assumed that soil moisture uptake is evenly distributed over the rooted depth, in a uniformly wetted profile. This implies that the major resistance to water flow is assumed in the soil and not in the roots.

Usually under field conditions, soil water content is not uniform. In the model, each layer is treated separately. Compensatory effects can be accommodated, so that when part of the root system is in dry soil compartments, those parts that are in wetter compartments, will take up more water (cf. Lawlor, 1973). The root activity coefficient ($EDPTFT$) varies between 0 and 1 and is inversely related to the relative amount of available water in a soil compartment (van Keulen & Seligman, 1987, Figure 31). The effect of this factor is to decrease potential uptake per unit depth of root penetration for that part of the root system that is in dry soil compartments, thus allowing increased uptake by roots in wetter compartments. Effective root length for each soil layer is obtained by multiplying the root penetration depth with the root activity coefficient.

The potential rate of water uptake ($TRRM$, $\text{mm mm}^{-1} \text{d}^{-1}$) per millimeter of effective rooted depth is calculated by dividing the potential transpiration rate of the canopy ($PTRANS$) by the cumulative effective root length.

The uptake per compartment ($TRWL1-4$) is equal to the potential uptake rate per millimeter of effective rooted depth ($TRRM$) multiplied by a factor accounting for the effect of low soil moisture contents ($WSE1-4$), and by the effective root length per soil compartment. Total water uptake ($ATRANS$) is the sum of water withdrawn from the individual soil compartments.

The multiplication factors for moisture uptake due to low soil moisture contents (between 1 and 0) for the individual soil compartments ($WSE1-4$) are discussed in Subsection 2.18.1.

2.16.4. Output variables

```

TPTRAN    = INTGRL(ZERO, PTRANS)
TATRAN    = INTGRL(ZERO, ATRANS)

```

Total potential canopy transpiration since the start of the simulation ($TPTRAN$, mm) and total water uptake (actual transpiration, $TATRAN$, mm) are computed.

2.17. Evaporation

Soil evaporation is important under incomplete soil cover, but is much lower than transpiration under a well developed crop canopy. Evaporation continues, albeit at a decreasing rate, until the soil is air-dry.

2.17.1. Potential soil evaporation

```

PEVAP     = EXP(-0.5*LAI) * (EVAPR + EVAPD)

```


Shading (also by dead leaves) is accounted for in this computation; the extinction coefficient for short-wave radiation (together with near infrared radiation) in the crop canopy is about 0.5.

2.17.2. Effect of soil dryness

```

DSLRL      = INTGRL(IDSLR, RDSLRL)
RDSLRL     = INSW(RRAIN-0.5, 1., -(DSLRL-1.)/DELT)

```

Actual evaporation rate depends on the water content of the top soil compartments. The latter cannot be correctly predicted by the model since a thin top layer cannot be simulated using time steps of one day. Therefore, an alternative formulation has been selected, based on the number of days since the last rain ($DSLRL$), the value of $IDSLR$ has a minimum of 1. and is reset to 1. when it rains (Stroosnijder, 1982). Days with less than 0.5 mm of rain are not taken into account.

2.17.3. Actual evaporation

```

AEVAP      = INSW(RRAIN-0.5, EVSD, EVSH)
EVSH       = MIN(PEVAP, (WL1-WCAD1*TKL1)/DELT+WLFL1)
PARAMETER WCAD1 = 0.025; WCAD2 = 0.025; WCAD3 = 0.025; WCAD4 = 0.025

```

In calculating actual evaporation ($AEVAP$, mm d^{-1}) a distinction is made (using the value of $DSLRL$) between days with rain ($EVSH$, mm d^{-1}) and days without rain ($EVSD$, mm d^{-1}). The former is set equal to the potential evaporation rate ($PEVAP$, mm d^{-1}) under the limiting condition that the top soil layer cannot be depleted beyond the air-dry water content ($WCAD$). For days without rain the evaporation rate ($EVSD$) is below the potential rate, and calculated as:

```

EVSD       = MIN(PEVAP, 0.6*PEVAP*(SQRT(DSLRL+1.)-...
                SQRT(DSLRL))+WLFL1)

```

The evaporation rate decreases as the top soil starts drying. The reduction in potential evaporation rate during drying is approximated using the experimental field observation that cumulative evaporation is proportional to the square root of time (Stroosnijder, 1982, 1987). The proportionality factor ($\text{mm}(\sqrt{\text{d}})^{-1}$) is assumed to be equal to 60% of the potential evaporation rate. Rainfall below 0.5 mm is too small to trigger the resetting of days since the last rain and is added to evaporation. This small amount of rainfall is assumed to evaporate without soil wetting.

2.17.4. Extraction of 'evaporation water' from soil layers

```

FEVL1      = MAX(WL1-WCAD1*TKL1, 0.1)*EXP(-EES*(0.5*TKL1))
FEVL2      = MAX(WL2-WCAD2*TKL2, 0.1)*EXP(-EES*(TKL1+...
                (0.5*TKL2)))
FEVL3      = MAX(WL3-WCAD3*TKL3, 0.1)*EXP(-EES*(TKL1+TKL2+...
                (0.5*TKL3)))
FEVL4      = MAX(WL4-WCAD4*TKL4, 0.1)*EXP(-EES*(TKL1+TKL2+TKL3+...
                (0.5*TKL4)))
PARAMETER EES = 0.002

```

Partitioning parameters (FEVL1-4) are computed for the four layers. In this way, redistribution of water due to developing potential gradients is mimicked by extracting water for evaporation from all compartments with a water content above air dryness. This is achieved through the use of a soil-specific extinction coefficient (EES , mm^{-1}) (van Keulen, 1975). Weighting also accounts for the depth and thickness of layers (TKL) and their water content. The extinction coefficient, that in principle has to be determined on the basis of experimental data, is approximately 10^{-2} mm^{-1} for heavy (clay) soils and $3 \times 10^{-2} \text{ mm}^{-1}$ for light (sandy) soils.

$$\begin{aligned} FEVLT &= FEVL1 + FEVL2 + FEVL3 + FEVL4 \\ EVSW1 &= AEVAP * (FEVL1 / FEVLT) \\ EVSW2 &= AEVAP * (FEVL2 / FEVLT) \\ EVSW3 &= AEVAP * (FEVL3 / FEVLT) \\ EVSW4 &= AEVAP * (FEVL4 / FEVLT) \end{aligned}$$

Finally, the contribution from the individual layers ($EVSW1-4$, mm d^{-1}) is computed by multiplying the actual evaporation rate ($AEVAP$) by the weighing factor for each compartment.

2.17.5. Output variables

$$\begin{aligned} TPEVAP &= \text{INTGRL}(\text{ZERO}, PEVAP) \\ TAEVAP &= \text{INTGRL}(\text{ZERO}, AEVAP) \end{aligned}$$

Cumulative potential soil evaporation since the start of the simulation ($TPEVAP$, mm) and cumulative actual soil evaporation ($TAEVAP$, mm) are computed.

2.18. Effects of water stress

2.18.1. Effect of soil water content on water uptake

Both water and air must be present in sufficient amounts in the soil for optimal uptake of soil water by roots. Since water content (WCL , θ) and air content are complementary (soil porosity), the dependence of actual water uptake rate on soil water content shows an optimum (Feddes et al., 1978). Starting from wilting point (θ_{wp}), water uptake rate first rises linearly with increasing soil water content until it reaches the potential transpiration rate (the evaporative demand, T_m). The water content at which this occurs is called the critical soil water content θ_c . Transpiration rate remains at its potential level over a range of water contents reaching to well over field capacity. At some point beyond field capacity (θ_{fc}), transpiration is hampered again. The shape of this response curve is depicted in Figure 2.2, where the actual transpiration rate T is given scaled to the potential transpiration rate T_m . In contrast to Feddes et al. (1978), not soil water potential, but soil water content is chosen as the independent variable (Gollan et al., 1986; Schulze, 1986). In the computational procedure (Subroutine SUBFR), the current value of water content determines which linear segment must be used.

It is convenient to scale water content in the lower dry part as a fraction of the range $\theta_{fc} - \theta_{wp}$, to the so-called *reduced water content* (Bresler, 1991):

$$S = \frac{(\theta - \theta_{wp})}{(\theta_{fc} - \theta_{wp})}$$

Table 2.2. Characteristic potential transpiration rates (see text for explanation for five crop groups according to Driessen (1986). (Source: Doorenbos *et al.*, 1978).

Crop group	$T_{S=0.5}$ (mm d ⁻¹)	Crops (example)
1	1.8	leaf vegetables
2	3	clover, carrot
3	4.5	pea, potato
4	6	groundnut
5	9	most grains, soybean

The critical moisture content θ_c , that denotes the transition from water-limited to potential transpiration rate is not at a fixed value. Restriction of water uptake rate due to water shortage starts at a higher water content when potential transpiration rate is higher, in other words θ_c then shifts to higher values. This phenomenon was documented by Denmead & Shaw (1962). Driessen (1986) listed the dependence of the relative position of this point in his Table 20, for five groups of plants that differ in drought sensitivity. This table can be summarized in the following way:

- i) The crop groups are characterized by the potential transpiration rate at which the critical soil water content θ_c is just halfway wilting point and field capacity, in other words where S is 0.5. This characteristic potential transpiration rate $T_{S=0.5}$ is given in Table 2.2 for the five crop groups of Table 20 of Driessen (1986).

- ii) The soil water depletion fraction p is then calculated as:

$$p = T_{S=0.5} / (T_m + T_{S=0.5})$$

or

$$1 - p = T_m / (T_m + T_{S=0.5})$$

The soil water content at which transpiration starts to fall short of the potential, the so-called critical soil water content, is given by:

$$\theta_c = \theta_{wp} + (1 - p) (\theta_{fc} - \theta_{wp})$$

- iii) The ratio between actual transpiration rate in the lower, dry part of the curve and the potential rate is now given by:

$$f_r = \frac{S}{(1 - p)}$$

After substitution of the equation for p we find a simple expression for the actual transpiration rate:

$$T = (T_m + T_{S=0.5}) S$$

This latter expression is not actually used in the program, but the ratio f_r is used instead. Here it serves to show the resulting dependence of actual transpiration on the two environmental conditions, potential rate T_m and actual water content θ (WCL), on the two soil parameters θ_{fc} and θ_{wp} , and on the plant parameter $T_{S=0.5}$.

Implementation in the model:

P = TRANSC / (TRANSC + PTRANS)
 PARAMETER TRANSC = 9.

```

CALL SUBFR (WCL1,WCFC1,P,WCWP1,WCWET1,WCST1, WSE1)
CALL SUBFR (WCL2,WCFC2,P,WCWP2,WCWET2,WCST2, WSE2)
CALL SUBFR (WCL3,WCFC3,P,WCWP3,WCWET3,WCST3, WSE3)
CALL SUBFR (WCL4,WCFC4,P,WCWP4,WCWET4,WCST4, WSE4)

```

```

PARAMETER WCWET1 = 0.35; WCWET2 = 0.35; WCWET3 = 0.35; WCWET4 = 0.35
PARAMETER WCWP1 = 0.075; WCWP2 = 0.075; WCWP3 = 0.075; WCWP4 = 0.075

```

The effect of availability of soil water on uptake in a compartment is presented by a factor ($WSE1-4$), with a value between 0.0 and 1.0. Figure 2.2 schematically shows the relation between this stress factor and soil water content.

These WSE -factors are computed in the Subroutine SUBFR. This function requires as inputs, the water content in the soil layer (WCL), the soil depletion factor (P), the water contents at field capacity ($WCFC$), wilting point ($WCWP$) and saturation ($WCST$), and the sensitivity coefficient for waterlogging ($WCWET$). In this subroutine, the critical water content ($WCCR$) is first calculated on the basis of the critical transpiration rate and P .

Water stress factors for the individual layers ($WSE1-4$) are used to compute total water uptake in Section 2.16. This leads to the actual transpiration ($ATRANS$).

2.18.2. Effect on CO_2 assimilation

$$PCEW = ATRANS / NOTNUL(PTRANS)$$

There is a significant influence of water stress on photosynthesis. Under ample moisture supply, leaf conductance is proportional to rate of photosynthesis so that photosynthesis rate largely determines transpiration rate (Goudriaan & van Laar, 1978). When water is in short supply, the inverse is true, as the rate of water uptake from the soil is then of crucial importance in governing stomatal opening and CO_2 assimilation is below its potential.

The factor used to reduce photosynthesis is $PCEW$. Where in the model daily total gross CO_2 assimilation ($DTGA$, $g\ CO_2\ m^{-2}\ ground\ d^{-1}$) is calculated (see Section 2.6) this is multiplied by $PCEW$.

2.18.3. Effect on carbohydrate partitioning

$$CPEW = MIN(1., 0.5 + ATRANS / NOTNUL(PTRANS))$$

The ratio of actual transpiration ($ATRANS$) and potential transpiration ($PTRANS$) is also used to represent the influence of water shortage on dry matter partitioning. When this ratio is above 0.5, the effect on physiological processes is usually small.

Carbohydrate partitioning between shoot and root under water stress is altered in favour of the root biomass. Brouwer (1962) described the physiological principle of this mechanism, based on the functional equilibrium. Yet it is difficult to quantify the instantaneous growth response of root biomass to water stress. It is assumed that up to a moderate stress level ($ATRANS / PTRANS > 0.5$), there is no significant effect on partitioning. At higher stress levels during the vegetative phase, the share that goes to the roots increases by up to 50% of the amount that otherwise would have gone to the shoot.

It is assumed that the relative partitioning of carbohydrates within the shoots between leaves, stems and storage organs is affected similarly to the partitioning between shoots and roots.

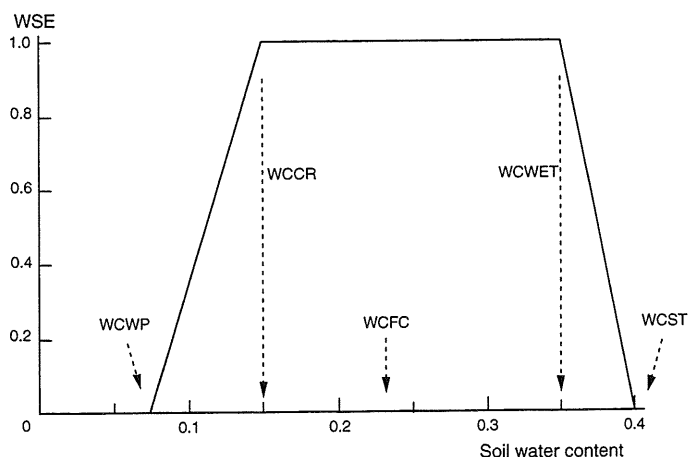


Figure 2.2. Water stress factor (WSE) as a function of soil moisture content. Wilting point ($WCWP, \theta_{wp}$), field capacity ($WCFC, \theta_{fc}$) and saturation ($WCST, \theta_{st}$) are soil characteristics. Values for WCCR depend on the potential transpiration/leaf area ratio and the sensitivity.

The parameter $CPEW$ (between 1 and 0) is used in the model as a multiplier in the calculation of the fraction of total dry matter increase allocated to the shoots (FSH), see Section 2.8.

2.19. Water use efficiency

$$\begin{aligned}
 TDTGA &= \text{INTGRL}(\text{ZERO}, DTGA) \\
 TAR &= TATRAN * 1.E3 / \text{NOTNUL}(TDTGA) \\
 * \quad TRC &= TATRAN * 1.E3 / \text{NOTNUL}(TDRW) \\
 CROFF &= (PTRANS + PEVAP) / \text{PENMAN}
 \end{aligned}$$

Various terms are used to express water use by crops. The most general one is the term 'crop water requirement' (Doorenbos & Kassam, 1979), i.e. the total amount of water needed to grow a crop. This amount includes both transpiration and evaporation. Values vary substantially among locations and years due to the large variation in evaporative demand and the inclusion of the soil evaporation. Hence, this variable is not used here.

Crop water requirements are often expressed in terms of the Penman reference evaporation through the use of 'crop factors', $CROFF$ (see e.g. Doorenbos & Pruitt, 1977; Feddes, 1987). In SUCROS2, we do not use this approach, but $CROFF$ is calculated to facilitate comparison with this common approach.

The 'transpiration coefficient', TRC , or its inverse the 'water use efficiency', is defined as the total amount of water transpired ($TATRAN$), divided by the total amount of biomass produced ($TDRW$, g DM m^{-2}). Note that soil evaporation is not included in this coefficient. It was established many years ago (de Wit, 1958; Tanner & Sinclair, 1982), that the transpiration coefficient during water stress is equal to that without stress. This is due to the constancy of the ratio of internal over external CO_2 concentration at different stress levels. Obviously, there are considerable, but predictable, differences in transpiration coefficient among environments and species.

Transpiration coefficient is still a crude concept in crop physiological studies, so a 'water use coefficient' of the crop, TAR (transpiration/assimilation ratio), defined as the amount of water transpired per unit gross photosynthesis in kilogram water per kilogram CO_2 , is also used (van Keulen & van Laar, 1986). TAR can be calculated on a daily basis ($ATRANS/DTGA$) as well as using cumulative values ($TATRAN/TDTGA$). Values for this water use coefficient range from about 50 or less to 200 or more. The lower values apply to C_4 crops in humid conditions and the high values to C_3 crops in dry climates.

2.20. Carbon balance check

```

CHKIN      = WLW * CFLV + WST * CFST + ...
            WRT * CFRT + WSO * CFSO
CHKFL      = TNASS * (12./44.)
TNASS      = INTGRL(TNASSI, RTNASS)
RTNASS     = ((GPHOT - MAINT)*44./30.) - ...
            (GRT*CO2RT + GLV*CO2LV + ...
            (GST+TRANSL)*CO2ST + GSO*CO2SO + ...
            (1.-CONVL)* TRANSL*CFST*44./12.)
CO2RT      = 44./12. * (ASRQRT*12./30. - CFRT)
CO2LV      = 44./12. * (ASRQLV*12./30. - CFLV)
CO2ST      = 44./12. * (ASRQST*12./30. - CFST)
CO2SO      = 44./12. * (ASRQSO*12./30. - CFSO)

CHKDIF     = (CHKIN-CHKFL)/NOTNUL(CHKIN)

```

```
PARAM CFLV=0.459; CFST=0.494; CFRT=0.467; CFSO=0.471
```

2.21. Run control

```

*      DAY      = 1. + AMOD(TIME-1., 365.)

FINISH DVS      > 2.
TIMER STTIME    = 80.; FINTIM = 300.; DELT = 1.; PRDEL = 5.
TRANSLATION_GENERAL DRIVER='EUDRIV'

PRINT DOY,DVS, DAYL, TDRW, TADRW, WLVG, WLVD, WLW, WST, ...
      WSO, WRT, LAI, EAI, HI, WL1, WL2, WL3, WL4, ...
      TPENM, TEVAPR, TEVAPD, TRAIN, TAINTC, TRNOFF, TDRAIN, ...
      TPTRAN, TATRAN, TPEVAP, TAEVAP, CHECK, TAR, EVAPR

```

In addition to the variables treated in SUCROS1, a number of additional variables, which reflect the crop and soil water balances, are specified. All values are stored in the output file RES.DAT at every print interval (PRDEL).

```

END      completes the specifications of the model;
STOP     terminates the simulation run;

```

```
SUBROUTINES
```

2.22. Subroutines

SUCROS2 is SUCROS1, extended for water-limited conditions. There are two additional subroutines (SUBFR is used to compute water stress factors for each soil layer and SUBGRT to decide whether root extension growth continues or ceases), and the main program in FST is extended with a section on water relations.


```

* 2.8 Dry matter partitioning
= ARGEN(FSHTB, DVS)
= (FSHP * CPEW) / (1. + (CPEW-1.) * FSHP)
= 1. - FSH
= 0.00,0.50, 0.10,0.50, 0.20,0.60, 0.35,0.78, ...
0.40,0.83, 0.50,0.87, 0.60,0.90, 0.70,0.93, ...
0.80,0.95, 0.90,0.97, 1.00,0.98, 1.10,0.99, ...
1.20,1.00, 2.50,1.00

= ARGEN(FLVTB, DVS)
= ARGEN(FSHTB, DVS)
= ARGEN(FSOTB, DVS)
= 0.00,0.65, 0.10,0.65, 0.25,0.70, 0.50,0.50, ...
0.70,0.15, 0.95,0.00, 2.50,0.00
= 0.00,0.35, 0.10,0.35, 0.25,0.30, 0.50,0.50, ...
0.70,0.85, 0.95,1.00, 1.05,0.00, 2.50,0.00
= 0.00,0.00, 0.95,0.00, 1.05,1.00, 2.50,1.00

= ABS(FLV+FST+FSTO - 1.)
> 1.E-6

* 2.9 Growth of plant organs and translocation
= FSH * (ASRQLV*FLV + ASRQST*FST + ASRQSO*FSTO) + ...
ASRQST*FST

= INSW(DVS-1., 0., WST * DVR * FRTRL)

= (GPHOT - MAINT + CONVL*TRANSL*CFST*30./12.) / ASRQ
= FRT * GTW
= FLV * FSH * GTW
= FST * FSH * GTW - TRANSL
= FSO * FSH * GTW

* The following values are calculated without
* the costs of nitrate reduction:
PARAMETER ASRQST = 1.444; ASRQLV = 1.463
PARAMETER ASRQST = 1.513; ASRQSO = 1.415
PARAMETER FRTRL = 0.20; CONVL = 0.947

* 2.10 Leaf and ear development
= 0.5 * EAI + LAI
= INTGRL(LAI, RLAI)
= GLAI - DLAI
CALL GLA(TIME, DOYEN, DTEFF, DVS, ... GLAI)
RGRL, DELT, SLA, LAI, GLV,
PARAMETER RGRL = 0.009
PARAMETER SLA = 0.022

= INTGRL(IEAI, REAI)
CALL SUBEAI(DELT,DVS,EAR,TADRW,RDRDV,EAI, REAI)
PARAMETER EAR = 0.63E-3

= LAI * RDR
= MAX(RDRDV, RDRSH)
= INSW(DVS-1.0, 0., DVR/(MAX(0.1, 2.-DVS))*FRDR)
= LIMIT(0., 0.03, 0.03 * (LAI-LAICR) / LAICR)
PARAMETER LAICR = 4.0; FRDR = 1.

DLV = WLVG * DLAI/NOTNUL(LAI)

* 2.11 Dry matter production
= INTGRL(WRTI, GRT)
= INTGRL(WLVI, RWLVG)
= GLV - DLV
= INTGRL(WLVDI, DLV)
= INTGRL(WSTI, GST)
= INTGRL(WSOI, GSO)

= WLVG + WLVD
= TADRW + WST + WSO
= TADRW
= WSO / NOTNUL(TADRW)

HI

* 2.12 Weather data
WEATHER WTRDIR='C:\SYS\WEATHER\'; CNTR='NLD'; ISTN=1; IYEAR=1990
* Reading weather data from the weather file:
* RDD Daily global radiation J/m2/d
* TMMN Daily minimum temperature degree C
* TMMX Daily maximum temperature degree C
* TMMX Vapour pressure kPa
* WN Wind speed m/s
* RAIN Precipitation mm/d
* LAT Latitude of the site degree
* DOY Daynumber of year = TIME d

DTR = RDD
DAVTMP = 0.5 * (TMMX + TMMN)
DITMP = TMMX - 0.25 * (TMMX-TMMN)
DTEFF = MAX(0., DAVTMP-TBASE)
PARAMETER TBASE = 0.
AVP = VP
WDS = WN
RRAIN = RAIN
TRAIN = INTGRL(ZERO, RRAIN)

* 2.13 Penman-Monteith combination equation
= EVAPR + EVAPD
= (1./LHVAP) * (SLOPE/(SLOPE+PSYCH)) * NRAD
= 4158.6 * SVP / (DAVTMP + 239.)**2
SVP = 0.611 * EXP(17.4 * DAVTMP / (DAVTMP + 239.))
PARAMETER LHVAP = 2.4E6
PARAMETER PSYCH = 0.067

= (1.-ALB) * DTR - RLWN
= ALBS*EXP(-0.5*LAI) + 0.25*(1.-EXP(-0.5*LAI))
= 0.25 * (1.-0.5*WCLI/WCST1)
= BBRAD * FVAP * FCLEAR * 86400.
= BOLITZM * (DAVTMP+273.)**4

```



```

PARAMETER BOLTZM = 5.668E-8
FVAP = 0.56-0.079*SQRT(AVP*10.)
FCLEAR = 0.1+0.9*FCLEAR
CLEAR = LIMIT(0., 1., ((DTR/DS0)-A)/B)
PARAMETER A = 0.25; B=0.45

WDF = 2.63 * (1.0 + 0.54 * WDS) * PSYCH
DRYP = (SVP-AVP) * WDF
EVAPD = DRYP/(SLOPE+PSYCH)

TPENM = INTGRL(ZERO, PENMAN)
TEVAPR = INTGRL(ZERO, EVAPR)
TEVAPD = INTGRL(ZERO, EVAPD)

* 2.14 The soil water balance
AINTC = MIN(RRAIN, INTC*LAI)
PARAMETER INTC = 0.25
RNOFF = MAX(0., 0.15*(RRRAIN-AINTC-10.)), ...
RRRAIN-AINTC-(WCST1*TKL1-WL1)/(2.*DELTA)
...
WLFL1 = RRRAIN - AINTC - RNOFF
WLFL2 = MAX(0., MIN(WL1-WCFC1*TKL1, ...
WLFL3 = MAX(0., WCST2*TKL2-WL2)/(2.*DELTA)
WLFL4 = MAX(0., MIN(WL2-WCFC2*TKL2, ...
WLFL5 = MAX(0., MIN(WL3-WCFC3*TKL3, ...
WLFL6 = MAX(0., MIN(WL4-WCFC4*TKL4)/(2.*DELTA), MDRATE))

PARAMETER WCFC1 = 0.23; WCFC2 = 0.23; WCFC3 = 0.23; WCFC4 = 0.23
PARAMETER WCST1 = 0.40; WCST2 = 0.40; WCST3 = 0.40; WCST4 = 0.40

DRAIN = WLFL5
RWL1 = WLFL1-WLFL2-EVSW1-TRWL1
RWL2 = WLFL2-WLFL3-EVSW2-TRWL2
RWL3 = WLFL3-WLFL4-EVSW3-TRWL3
RWL4 = WLFL4-WLFL5-EVSW4-TRWL4

WL1 = INTGRL(WL1I, RWL1)
WL2 = INTGRL(WL2I, RWL2)
WL3 = INTGRL(WL3I, RWL3)
WL4 = INTGRL(WL4I, RWL4)
WCL1 = WL1/TKL1
WCL2 = WL2/TKL2
WCL3 = WL3/TKL3
WCL4 = WL4/TKL4
RWCL1 = (WCL1-WCWP1)/(WCFC1-WCWP1)
RWCL2 = (WCL2-WCWP2)/(WCFC2-WCWP2)
RWCL3 = (WCL3-WCWP3)/(WCFC3-WCWP3)
RWCL4 = (WCL4-WCWP4)/(WCFC4-WCWP4)

TDRAIN = INTGRL(ZERO, DRAIN)
TAINTC = INTGRL(ZERO, AINTC)
TRNOFF = INTGRL(ZERO, RNOFF)

WCUM = WL1+WL2+WL3+WL4
CHECK = TRRAIN+WCUMI-TAINTC-TRNOFF-TDRAIN-WCUM-...
TATRAN-TAEVAP

* 2.15 Rooted depth
ZRT = INTGRL(ZRTI, EZRT)
EZRT = EZRTC * WSERT * AMTWP
* Temperature effect included, same as for AMAX (AMTWP)

CALL SUBGRT (ZRT, ZRTM, DVS, TKL1, TKL2, TKL3, TKL4, WCL1, WCL2, ...
WCL3, WCL4, WCWP1, WCWP2, WCWP3, WCWP4, WSERT)
PARAMETER EZRTC = 12.

* 2.16 Transpiration
PTRANS = (1. - EXP(-0.5*LAI)) * EVAPR + EVAPD * ...
MIN(2.0, LAI) - 0.5 * AINTC

FUNCTION EDPTFT = -.50, 0., -.05, 0., 0., .15, .15, .6, ...
.3, .8, .5, 1., 2., 1.
ERLB = ZRT1*AFGEN(EDPTFT, RWCL1) + ...
ZRT2*AFGEN(EDPTFT, RWCL2) + ...
ZRT3*AFGEN(EDPTFT, RWCL3) + ...
ZRT4*AFGEN(EDPTFT, RWCL4)
PTRANS/NOTNUL(ERLB)
TRRM = TRRM*WSE1+ZRT1*AFGEN(EDPTFT, RWCL1)
TRWL1 = TRRM*WSE2+ZRT2*AFGEN(EDPTFT, RWCL2)
TRWL2 = TRRM*WSE3+ZRT3*AFGEN(EDPTFT, RWCL3)
TRWL3 = TRRM*WSE4+ZRT4*AFGEN(EDPTFT, RWCL4)
ZRT1 = LIMIT(0., TKL1, ZRT)
ZRT2 = LIMIT(0., TKL2, ZRT-TKL1)
ZRT3 = LIMIT(0., TKL3, ZRT-TKL1-TKL2)
ZRT4 = LIMIT(0., TKL4, ZRT-TKL1-TKL2-TKL3)
ATRANS = TRWL1+TRWL2+TRWL3+TRWL4
TPTRAN = INTGRL(ZERO, PTRANS)
TATRAN = INTGRL(ZERO, ATRANS)

* 2.17 Evaporation
PEVAP = EXP(-0.5*LAI) * (EVAPR + EVAPD)
DSLRL = INTGRL(DSLRL, RDSLRL)
RDSLRL = INSW(RRAIN-0.5, 1., -(DSLRL-1.)/DELTA)
AEVAP = INSW(RRAIN-0.5, EVSD, EVSH)
EVSH = MIN(PEVAP, (WL1-WCAD1*TKL1)/DELTA+WLFL1)
PARAMETER WCAD1 = 0.025; WCAD2 = 0.025; WCAD3 = 0.025; WCAD4 = 0.025
EVSD = MIN(PEVAP, 0.6*PEVAP*(SQRT(DSLRL+1.))-...
SQRT(DSLRL))+WLFL1)
FEVL1 = MAX(WL1-WCAD1*TKL1, 0.1)*EXP(-EES*(0.5*TKL1))
FEVL2 = MAX(WL2-WCAD2*TKL2, 0.1)*EXP(-EES*(TKL1+...
(0.5*TKL2)))
FEVL3 = MAX(WL3-WCAD3*TKL3, 0.1)*EXP(-EES*(TKL1+TKL2+...
(0.5*TKL3)))
FEVL4 = MAX(WL4-WCAD4*TKL4, 0.1)*EXP(-EES*(TKL1+TKL2+TKL3+...
(0.5*TKL4)))

```

```

PARAMETER BES
= 0.002

FEVL1 = FEVL1+FEVL2+FEVL3+FEVL4
FEVL2 = AEVAP*(FEVL1/FEVL1)
FEVL3 = AEVAP*(FEVL2/FEVL2)
FEVL4 = AEVAP*(FEVL3/FEVL3)
FEVL5 = AEVAP*(FEVL4/FEVL4)

TPEVAP = INTGRL(ZERO, PEVAP)
TAEVAP = INTGRL(ZERO, AEVAP)

* 2.18 Effects of water stress

P = TRANSC/(TRANS+PTRANS)
PARAMETER TRANSC = 9.

CALL SUBFR (WCL1,WCFC1,P,WCWP1,WCWET1,WCST1,WSEL)
CALL SUBFR (WCL2,WCFC2,P,WCWP2,WCWET2,WCST2,WSE2)
CALL SUBFR (WCL3,WCFC3,P,WCWP3,WCWET3,WCST3,WSE3)
CALL SUBFR (WCL4,WCFC4,P,WCWP4,WCWET4,WCST4,WSE4)

PARAMETER WCWET1 = 0.35; WCWET2 = 0.35; WCWET3 = 0.35; WCWET4 = 0.35
PARAMETER WCWP1 = 0.075; WCWP2 = 0.075; WCWP3 = 0.075; WCWP4 = 0.075

PCW = ATRANS/NOTNUL (PTRANS)
CPEW = MIN(1., 0.5+ATrans/NOTNUL (PTRANS))

* 2.19 Water use efficiency

TDTGA = INTGRL(ZERO, DTGA)
TAR = TATRAN*1.E3/NOTNUL (TDTGA)
TRC = TATRAN*1.E4/(NOTNUL (TDRW)
CROFF = (PTRANS+PEVAP)/PENMAN

* 2.20 Carbon balance check

CHKIN = WLV * CFLV + WST * CFST + ...
WRT * CFRT + WSO * CFSTO
TNASS = (12./44.)
INTGRL(TNASS, RTNASS)
= ((GPHOT - MAINT)*44./30.) - ...
(GST+TRANSL)*CO2ST + GSO*CO2SO + ...
(1.-CONVL)*TRANSL*CFST*44./12.)
= 44./12. * (ASQRT*12./30. - CFRT)
= 44./12. * (ASQRT*12./30. - CFLV)
= 44./12. * (ASQRT*12./30. - CFST)
= 44./12. * (ASQRT*12./30. - CFSTO)

CHKDIF = (CHKIN-CHKFL)/NOTNUL (CHKIN)

PARAM CFLV=0.459; CFST=0.494; CFRT=0.467; CFSTO=0.471

* 2.21 Run control

* DAY = 1. + AMOD(TIME-1., 365.)

FINISH DVS > 2.

```

```

TIMER STTIME = 80.; FINTIM = 300.; DELT = 1.; PRDEL = 5.
TRANSLATION_GENERAL DRIVER='EUDRIV'

PRINT DOY, WRT, DAYL, TDRW, TADRW, WLVG, WLVD, WLW, WST, ...
WSO, DVS, LAI, EAI, HI, WL1, WL2, WL3, WL4, ...
TENN, TEVAPR, TEVAPD, TRAIN, TAINC, TRNOFF, TDRAIN, ...
TTRAN, TATRAN, TPEVAP, TAEVAP, CHECK, TAR, EVAPR, ...
EVAPD, CROFF, WSEL, WSE3, WSE4, CPEW, CPEW, ZRT, ERLB, WCUM, ...
RWCL1, RWCL2, RWCL3, RWCL4, CHKDIF, P

END
STOP

* 2.22 SUBROUTINES

* SUBROUTINE GLA
* Purpose: This subroutine computes daily increase of leaf area index
* (m2 leaf/ m2 ground/ d)
* Version: September 1997 (SUCROS97 V1.0)
* FORMAL PARAMETERS: (I=input, O=output, C=control, IN=init, T=time)
* name type meaning units class
* -----
* TIME R4 Time in simulation d T
* DOYM R4 Day number of crop emergence d T
* DTEFF R4 Daily effective temperature oC I
* DVS R4 Development stage of the crop - I
* RGRL R4 Relative leaf growth rate oC-1 d-1 I
* DELT R4 Time step of integration d T
* SLA R4 Specific leaf area m2 g-1 I
* LAI R4 Leaf area index m2 m-2 I
* GLV R4 Growth rate of the leaves g m-2 d-1 I
* GLAI R4 Growth rate of leaf area index m2 m-2 d-1 O
*
SUBROUTINE GLA (TIME, DOYM, DTEFF, DVS, RGRL, DELT, SLA, LAI, GLV,
$ GLAI)
IMPLICIT REAL (A-Z)
GLAI = SLA * GLV
*-----growth during maturation stage
GLAI = SLA * GLV
*-----growth during juvenile stage
IF ((DVS.LT.0.3).AND.(LAI.LT.0.75)) THEN
GLAI = (LAI * (EXP(RGRL*DTEFF*DELT)-1.))/DELT
ENDIF
*-----growth before seedling emergence
IF (TIME.IE.DOYM) GLAI = 0.
RETURN
END

* SUBROUTINE SUBEAI
* Purpose: This subroutine calculates ear area index
* Version: September 1997 (SUCROS97 V1.0)
* FORMAL PARAMETERS: (I=input, O=output, C=control, IN=init, T=time)

```

```

* name      type meaning      units      class
* ----      -
* DELT      R4 Time step of integration      d      T
* DVS        R4 Development stage of the crop      -      I
* EAR        R4 Ear area/weight ratio      g m-2      I
* TADRW      R4 Total above-ground dry weight      g m-2      I
* RDR        R4 Relative death rate      d-1      I
* EAI        R4 Ear area index      m2 m-2      I
* REAI       R4 Growth rate ear area index      m2 m-2 d-1      O
*
SUBROUTINE SUBEAI (DELT, DVS, EAR, TADRW, RDRDV, EAI, REAI)
IMPLICIT REAL(A-Z)
IF (DVS.LT.0.8) REAI = 0.
IF (DVS.GE.0.8 .AND. EAI.EQ.0.) THEN
  REAI = (EAR * TADRW) / DELT
ELSE
  REAI = 0.
ENDIF
IF (DVS.GE.1.3) REAI = -RDRDV * EAI
RETURN
END

* name      type meaning      units      class
* ----      -
* SUBROUTINE ASTRO
* Purpose: This subroutine calculates astronomic daylength,
*          diurnal radiation characteristics such as the daily
*          integral of sine of solar elevation and solar constant.
* Version: September 1997 (SUCROS97 V1.0)
*
* FORMAL PARAMETERS: (I=input, O=output, C=control, IN=init, T=time)
* name      type meaning      units      class
* ----      -
* DOY       R4 Daynumber (Jan 1st = 1)      -      T
* LAT       R4 Latitude of the site      degrees      I
* SC        R4 Solar constant      J m-2 s-1      O
* DSO       R4 Daily extraterrestrial radiation      J m-2 d-1      O
* SINLD     R4 Seasonal offset of sine of solar height      -      O
* COSLD     R4 Amplitude of sine of solar height      -      O
* DAYL      R4 Astronomic daylength (base = 0 degrees)      h      O
* DSINB     R4 Daily total of sine of solar height      s      O
* DSINBE    R4 Daily total of effective solar height      s      O
*
* FATAL ERROR CHECKS (execution terminated, message)
* condition: LAT > 67, LAT < -67
*
SUBROUTINE ASTRO (DOY, LAT,
& SC, DSO, SINLD, COSLD, DAYL, DSINB, DSINBE)
IMPLICIT REAL (A-Z)

*-----PI and conversion factor from degrees to radians
PI = 3.141592654
RAD = PI/180.

*-----check on input range of parameters
IF (LAT.GT.67.) STOP 'ERROR IN ASTRO: LAT> 67'
IF (LAT.LT.-67.) STOP 'ERROR IN ASTRO: LAT<-67'

*-----declination of the sun as function of daynumber (DOY)
DEC = -ASIN (SIN (23.45*RAD)*COS (2.*PI*(DOY+10.)/365.))

*-----SINLD, COSLD and AOB are intermediate variables
SINLD = SIN (RAD*LAT)*SIN (DEC)
COSLD = COS (RAD*LAT)*COS (DEC)
AOB = SINLD/COSLD

*-----daylength (DAYL)
DAYL = 12.0*(1.+2.*ASIN (AOB)/PI)

DSINB = 3600.*(DAYL*SINLD+24.*COSLD*SQRT (1.-AOB*AOB)/PI)
DSINBE = 3600.*(DAYL*(SINLD+0.4*(SINLD*SINLD+COSLD*COSLD*0.5))+
& 12.0*COSLD*(2.0+3.0*0.4*SINLD)*SQRT (1.-AOB*AOB)/PI)

*-----solar constant (SC) and daily extraterrestrial radiation (DSO)
SC = 1370.*(1.+0.033*COS (2.*PI*DOY/365.))
DSO = SC*DSINB

RETURN
END

* name      type meaning      units      class
* ----      -
* SUBROUTINE TOTASS
* Purpose: This subroutine calculates daily total gross
*          assimilation (DTGA) by performing a Gaussian integration
*          over time. At three different times of the day, assimilation
*          radiation is computed and used to determine assimilation
*          whereafter integration takes place.
* Version: September 1997 (SUCROS97 V1.0)
*
* FORMAL PARAMETERS: (I=input, O=output, C=control, IN=init, T=time)
* name      type meaning      units      class
* ----      -
* DOY       R4 Day number (January 1 = 1)      -      T
* LAT       R4 Latitude of the site      degrees      I
* DTR       R4 Daily total of global radiation      J/m2/d      I
* SCP       R4 Scattering coefficient of leaves for visible
*          radiation (PAR)      -      I
* AMAX      R4 Assimilation rate at light saturation      g CO2/
*          m2 leaf/s      m2 CO2/J      I
* EFF       R4 Initial light conversion factor      g CO2/J      I
* KDF       R4 Extinction coefficient diffuse flux leaves      -      I
* LAI       R4 Leaf area index as used for photosynthesis      m2/m2      I
*
* Note: This can involve stem, flower or
*       ear area index!!
*
* DAYL      R4 Astronomic daylength (base = 0 degrees)      h      O
* DTGA      R4 Daily total gross assimilation      g CO2/m2/d      O
* DSO       R4 Daily extraterrestrial radiation      J/m2/s      O
*
* SUBROUTINES called : ASTRO, ASSIM
&
SUBROUTINE TOTASS (DOY, LAT, DTR, SCP, AMAX, EFF, KDF, LAI,
& IMPLICIT REAL(A-Z)
REAL XGAUSS(3), WGAUSS(3)
INTEGER I1, IGAUSS
DATA IGAUSS /3/

```

```

DATA XGAUSS /0.112702, 0.500000, 0.887298/
DATA WGAUSS /0.277778, 0.444444, 0.277778/
PI = 3.141592654
CALL ASTRO(DOY, LAT, SC, DS0, SINLD, COSLD, DAYL, DSINB, DSINBE)
DTGAS = 0.
DO 10 I1=1, IGAUSS
  at the specified HOUR, radiation is computed and used to compute
  assimilation
  HOUR = 12.0+DAYL*0.5*XGAUSS(I1)
  -----
  -----sine of solar elevation
  SINB = MAX (0., SINLD+COSLD*COS (2.*PI*(HOUR+12.)/24.))
  -----
  -----diffuse light fraction (FRDF) from atmospheric
  transmission (ATMTR)
  PAR = 0.5*DTR*SINB*(1.+0.4*SINB)/DSINBE
  ATMTR = PAR/(0.5*SC*SINB)
  IF (ATMTR.LE.0.22) THEN
    FRDF = 1.
  ELSE IF (ATMTR.GT.0.22 .AND. ATMTR.LE.0.35) THEN
    FRDF = 1.-6.4*(ATMTR-0.22)**2
  ELSE
    FRDF = 1.47-1.66*ATMTR
  END IF
  FRDF = MAX (FRDF, 0.15+0.85*(1.-EXP (-0.1/SINB)))
  -----
  -----diffuse PAR (PARDF) and direct PAR (PARDR)
  PARDF = PAR * FRDF
  PARDR = PAR - PARDF
  CALL ASSIM (SCP, AMAX, EFF, KDF, LAI, SINB, PARDR, PARDF, FGROS)
  DTGAS = DTGAS+FGROS*WGAUSS(I1)
  -----
10 CONTINUE
  DTGAS = DTGAS * DAYL * 3600.
  RETURN
  END
  -----
  * SUBROUTINE ASSIM
  * Purpose: This subroutine performs a Gaussian integration over
  * depth of canopy by selecting five different LAI's and
  * computing assimilation at these LAI levels. The
  * integrated variable is FGROS.
  * Version: September 1997 (SUCROS97 V1.0)
  *
  * FORMAL PARAMETERS: (I=input, O=output, C=control, IN=init, T=time)
  * name type meaning
  * ---
  *
  * SCP Scattering coefficient of leaves for visible radiation (PAR) I
  * AMAX Assimilation rate at light saturation g CO2/m2 leaf/s I
  * EFF Initial light conversion factor g CO2/J I
  * KDF Extinction coefficient of diffuse flux leaves m2/m2 I
  * LAI Leaf area index as used for photosynthesis Note: This can involve stem, flower or ear area index!! I
  * SINB Sine of solar height I
  * PARDR Instantaneous flux of direct radiation (PAR) W/m2 I
  * PARDF Instantaneous flux of diffuse radiation (PAR) W/m2 I
  * FGROS Instantaneous assimilation rate of whole canopy g CO2/m2 soil/s O
  *
  *-----
  * SUBROUTINE ASSIM (SCP, AMAX, EFF, KDF, LAI, SINB, PARDR, PARDF,
  * & FGROS)
  * IMPLICIT REAL(A-Z)
  * REAL XGAUSS(5), WGAUSS(5)
  * INTEGER I1, I2, IGAUSS
  *
  *-----Gauss weights for five point Gauss
  * DATA IGAUSS /5/
  * DATA XGAUSS /0.0469101, 0.2307534, 0.5, 0.7692465, 0.9530899/
  * DATA WGAUSS /0.1184635, 0.2393144, 0.2844444, 0.2393144, 0.1184635/
  *
  *-----Reflection of horizontal and spherical leaf angle distribution
  * SOV = SQRT(1.-SCP)
  * REPH = (1.-SOV)/(1.+SOV)
  * REFS = REPH*2./(1.+2.*SINB)
  *
  *-----extinction coefficient for direct radiation and total direct flux
  * CLUSTFF = KDF / (0.8*SOV)
  * KBL = (0.5/SINB) * CLUSTFF
  * KDRT = KBL * SOV
  *
  *-----selection of depth of canopy, canopy assimilation is set to zero
  * FGROS = 0.
  *
  * DO 10 I1=1, IGAUSS
  * LAIC = LAI * XGAUSS(I1)
  *
  *-----absorbed fluxes per unit leaf area: diffuse flux, total direct
  * flux, direct component of direct flux
  * VISDF = (1.-REFH)*PARDR*KDF *EXP (-KDF *LAIC)
  * VIST = (1.-REFS)*PARDR*KDRT *EXP (-KDRT *LAIC)
  * VISD = (1.-SCP) *PARDR*KBL *EXP (-KBL *LAIC)
  *
  *-----absorbed flux (J/M2 leaf/s) for shaded leaves and assimilation of
  * shaded leaves
  * VISSHD = VISDF + VIST - VISD
  * IF (AMAX.GT.0.) THEN
  * FORSH = AMAX * (1.-EXP(-VISSHD*EFF/AMAX))
  * ELSE
  * FORSH = 0.
  * END IF
  *
  *-----direct flux absorbed by leaves perpendicular on direct beam and
  * assimilation of sunlit leaf area

```

```

VISPP = (1.-SCP) * PARDR / SINB
FGRSUN = 0.
DO 20 I2=1,IGAUSS
  VISSUN = VISSHD + VISPP * XGAUSS(I2)
  IF (AMAX.GT.0.) THEN
    FGRS = AMAX * (1.-EXP(-VISSUN*EFF/AMAX))
  ELSE
    FGRS = 0.
  END IF
  FGRSUN = FGRSUN + FGRS * WGAUSS(I2)
20 CONTINUE
*-----fraction sunlit leaf area (FSLA) and local assimilation
rate (FGL)
FSLA = CLUSTF * EXP(-KBL*LAIC)
FGL = FSLA * FGRSUN + (1.-FSLA) * FGRSH
*-----integration of local assimilation rate to canopy
assimilation (FGROS)
FGROS = FGROS + FGL * WGAUSS(I1)
10 CONTINUE
FGROS = FGROS * LAI
RETURN
END

```

```

*-----Subroutine SUBGR
* Purpose: To decide whether root extension growth continues or
ceases (value either 0 or 1)
* Version: September 1997 (SUCROS97 V1.0)
* FORMAL PARAMETERS: (I=input, O=output, C=control, IN=init, T=time)
* name type meaning units class
*-----
* ZRT R4 Rooted depth mm I
* ZRTM R4 Maximum value for rooted depth mm I
* DVS R4 Development stage of the crop - I
* TKL1-4 R4 Thickness of the soil layers mm I
* WCL1-4 R4 Volumetric water content in soil layers cm3/cm3 I
* WCWP1-4 R4 Volumetric water content at wilting point cm3/cm3 I
* WSERT R4 Variable to calculate root extension - O
*-----
SUBROUTINE SUBGR(ZRT,ZRTM,DVS,TKL1,TKL2,TKL3,TKL4,WCL1,WCL2,
$ WCL3,WCL4,WCWP1,WCWP2,WCWP3,WCWP4,WSERT)
IMPLICIT REAL(A-Z)
SAVE
WSERT = 1.
IF (ZRT.LT.TKL1 .AND. WCL1.LT.WCWP1) WSERT = 0.
IF (ZRT.GT.TKL1 .AND. ZRT.LT.(TKL1+TKL2) .AND.
$ WCL2.LT.WCWP2) WSERT = 0.
IF (ZRT.GT.(TKL1+TKL2) .AND. ZRT.LT.(TKL1+TKL2+TKL3) .AND.
$ WCL3.LT.WCWP3) WSERT = 0.
IF (ZRT.GT.(TKL1+TKL2+TKL3) .AND. ZRT.LT.(TKL1+TKL2+TKL3+TKL4)
$ .AND. WCL4.LT.WCWP4) WSERT = 0.
IF (DVS.GE.1.) WSERT=0.
IF (ZRT.GT.ZRTM) WSERT=0.
RETURN

```

```

*-----Subroutine SUBFR
* Purpose: To compute factors accounting for water stress effect on
water uptake
Revision 24 Nov 96 by Paul Kiepe
To avoid division by zero, if P=0.
Version: September 1997 (SUCROS97 V1.0)
* FORMAL PARAMETERS: (I=input, O=output, C=control, IN=init, T=time)
* name type meaning units class
*-----
* WCL R4 Volumetric water content in soil layers cm3/cm3 I
* WCFC R4 Volumetric water content at field capacity cm3/cm3 I
* P R4 Soil water depletion factor - I
* WCWP R4 Volumetric water content at wilting point cm3/cm3 I
* WCWET R4 Volumetric water content where
water logging begins cm3/cm3 I
* WCST R4 Volumetric water content at saturation cm3/cm3 I
* WSE R4 Factor accounting for effect of uptake
availability of soil water - O
*-----
SUBROUTINE SUBFR(WCL,WCFC,P,WCWP,WCWET,WCST,WSE)
IMPLICIT REAL(A-Z)
SAVE
WCCR = WCWP + (1.-P) * (WCFC - WCWP)
IF (WCL.GT.WCWET) THEN
  FR = (WCST-WCL)/(WCST-WCWET)
ELSE IF (WCL.LE.WCWET .AND. WCL.GT.WCCR) THEN
  FR = 1.
ELSE IF (WCL.LE.WCCR .AND. WCL.GT.WCWP) THEN
  FR = (WCL-WCWP)/(WCCR-WCWP)
ELSE
  FR = 0.
ENDIF
WSE = MIN(1.,MAX(0., FR))
RETURN
END

```


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Appendix I: MOMASSP

In SUCROS, daily canopy assimilation rate is found by Gaussian integration over the day. This method, which is computationally very efficient, obscures however the underlying within-day dynamics of the canopy assimilation rate. To see this dynamics and to study the photosynthesis-light response curve of the canopy as a whole a separate FST program is here presented which uses the modules of SUCROS, but specifically applied on the time scale of the within-day dynamics.

This means that the canopy variables such as leaf area index (*LAI*) are input parameters, and do not grow. Also, the leaf photosynthesis properties such as *AMAX* are treated as input parameters. In reality they might not be constant due to temperature and/or water stress. To see these kind of effects, the model presented here should be extended.

The daily time course of incoming radiation is handled as in SUCROS: solar height determines the radiation level, using a daily constant transmissivity of the atmosphere.

The computational accuracy of the equations for radiation distribution over the canopy is checked by the variable *BALANS*. This variable is calculated as the difference between the net fluxes above and below the canopy and the independently calculated sum of *PAR* absorption by the individual leaves (*PARABS*).

```

DEFINE_CALL RADMOM(INPUT,INPUT,INPUT,INPUT,INPUT,INPUT,...
                  OUTPUT,OUTPUT,OUTPUT)
DEFINE_CALL ASSMOM(INPUT,INPUT,INPUT,INPUT,INPUT,INPUT,INPUT,INPUT,...
                  OUTPUT,OUTPUT,OUTPUT,OUTPUT,OUTPUT)

TITLE Time course of canopy assimilation rate within a day
*      MOMASSP V1.0, Version September 1997

INITIAL
PARAM PI      = 3.141592654
PARAM LATT    = 52.
PARAM AMAX    = 1000.; EFF    = 12.
PARAM DAY     = 1.00; ATMTR = 0.5
PARAM LAI     = 5.; KDF      = 0.7; SCP = 0.2

RAD      = PI/180.

*-----declination of the sun as function of daynumber (DAY)
DEC      = -ASIN(SIN(23.45*RAD)*COS(2.*PI*(DAY+10.)/365.))

*-----SINLD, COSLD and AOB are intermediate variables
SINLD    = SIN(RAD*LATT)*SIN(DEC)
COSLD    = COS(RAD*LATT)*COS(DEC)
AOB      = SINLD/COSLD

*-----daylength (DAYL) and photoperiodic daylength (DAYLP)
DAYL     = 12.0*(1.+2.*ASIN(AOB)/PI)

```

*-----run control

TIMER STTIME = 0.; FINTIM = 24.; DELT = 1.; PRDEL = 1.

TRANSLATION_GENERAL DRIVER='EUDRIV'

PRINT LAI, FGROS, BALANS, PARINC, REFL, SOIL, PARABS

DYNAMIC

 HOUR = TIME

 CALL RADMOM (HOUR, DAY, DAYL, SINLD, COSLD, ATMTR, ...
 SINB, PARDR, PARDF)

 CALL ASSMOM (SCP, AMAX, EFF, KDF, LAI, SINB, PARDR, PARDF, ...
 REFL, SOIL, PARABS, FGROS, BALANS)

 PARINC = PARDF+PARDR

END

PARAM LAI = 1.

END

PARAM LAI = 0.1

END

STOP

```

*-----*
* Subroutine RADMOM:                                     *
* This is a modified RADIAT Subroutine                   *
* Fraction diffuse is calculated according to momentane values as *
* described by                                           *
* Spitters, C.J.T., H.A.J.M. Toussaint & J. Goudriaan, 1986, *
* Separating the diffuse and direct component of global radiation *
* and its implications for modeling canopy photosynthesis. Part I. *
* Components of incoming radiation.                     *
* Agric. and Forest Meteorology 38, 217-229.            *
*                                                        *
* Computation of diffuse and direct amount of photosynthetically *
* active radiation (PAR) from average global radiation (AVRAD), *
* DAY of the year and HOUR of the day.                   *
*                                                        *
* FORMAL PARAMETERS: (I=input,O=output,C=control,IN=init,T=time) *
* name  type meaning                                units  class *
* ----  - - - - - - - - - - - - - - - - - - - - - - - - - - - *
* HOUR   R4  Selected hour during the day             h      T   *
* DAY    R4  Day number (January 1 = 1)                d      T   *
* DAYL   R4  Daylength                                h      I   *
* SINLD  R4  Seasonal offset of sine of solar height   -      I   *
* COSLD  R4  Amplitude of sine of solar height         -      I   *
* ATMTR  R4  Atmospheric transmission coefficient       -      I   *
* SINB   R4  Sine of solar elevation                   -      O   *
* PARDR  R4  Instantaneous direct flux of incoming PAR J/m2/s  O   *
* PARDF  R4  Instantaneous diffuse flux of incoming PAR J/m2/s  O   *
*-----*

```

```

SUBROUTINE RADMOM (HOUR, DAY, DAYL, SINLD, COSLD, ATMTR,
$                SINB, PARDR, PARDF)
IMPLICIT REAL (A-Z)
PARAMETER (PI=3.141592654)

*-----sine of solar elevation (SINB), integral of SINB (DSINB)
AOB    = SINLD/COSLD
SINB    = MAX(0., SINLD+COSLD*COS(2.*PI*(HOUR+12.)/24.))
DSINB   = 3600.*(DAYL*SINLD+24.*COSLD*SQRT(1.-AOB*AOB)/PI)
SC      = 1370.*(1.+0.033*COS(2.*PI*DAY/365.))
AVRAD   = ATMTR*SC*SINB

*-----diffuse light fraction (FRDF) from atmospheric transmission (ATMTR)
FRDF    = 1.47-1.66*ATMTR
IF (ATMTR.LE.0.35.AND.ATMTR.GT.0.22) FRDF=1.-6.4*(ATMTR-0.22)**2
IF (ATMTR.LE.0.22) FRDF=1.
FRDF    = MAX(FRDF, 0.15+0.85*(1.-EXP(-0.1/MAX(0.01, SINB))))

*-----diffuse PAR (PARDF) and direct PAR (PARDR)
PAR      = 0.5*AVRAD
PARDF    = MIN(PAR, SINB*FRDF*ATMTR*0.5*SC)
PARDR    = PAR-PARDF

RETURN
END

*-----*
* Subroutine ASSMOM *
* Performs a Gaussian integration over depth of canopy by *
* selecting five different LAI's and computing assimilation at *
* these LAI levels. The integrated variable is FGROS. *
* Calculation of the BALANS of PAR *
* *
* FORMAL PARAMETERS: (I=input, O=output, C=control, IN=init, T=time) *
* name type meaning units class *
* ---- ---- *
* SCP R4 Scattering coefficient of leaves for *
* visible radiation (PAR) - I *
* AMAX R4 Assimilation rate at light saturation microg CO2/ *
* m2 leaf/s I *
* EFF R4 Initial light cobversion factor microg CO2/J I *
* KDF R4 Extinction coefficient for leaves - I *
* LAI R4 Leaf area index m2/m2 I *
* SINB R4 Sine of solar elevation - I *
* PARDR R4 Instantaneous direct flux of incomng PAR J/m2/s I *
* PARDF R4 Instantaneous diffuse flux of incoming PAR J/m2/s I *
* REFL R4 Reflected flux of PAR by the crop J/m2/s O *
* SOIL R4 Flux of PAR absorbed by the soil surface J/m2/s O *

```

```
* PARABS R4 Total PAR absorbed by the leaves J/m2/s O *
* FGROS R4 Instantaneous assimilation rate of microg CO2/m2/s O *
* whole canopy *
* BALANS R4 Difference between PARABS and net flux at J/m2/s O *
* canopy boundaries *
*-----*
```

```
SUBROUTINE ASSMOM(SCP, AMAX, EFF, KDF, LAI, SINB, PARDR, PARDF,
$ REFL, SOIL, PARABS, FGROS, BALANS)
IMPLICIT REAL(A-Z)
REAL XGAUSS(5), WGAUSS(5)
INTEGER I1, I2, IGAUSS
```

```
*-----Gauss weights for five point Gauss
DATA XGAUSS /0.0469101,0.2307534,0.5000 ,0.7692465,0.9530899/
DATA WGAUSS /0.1184635,0.2393144,0.284444,0.2393144,0.1184635/
DATA IGAUSS /5/
```

```
*-----reflection of horizontal and spherical leaf angle distribution
SQV = SQRT(1.-SCP)
REFH = (1.-SQV)/(1.+SQV)
REFS = REFH*2./(1.+1.6*SINB)
```

```
*-----extinction coefficient for direct radiation and total direct flux
CLUSTF = KDF / (0.8*SQV)
KBL = (0.5/MAX(0.01,SINB)) * CLUSTF
KDRT = KBL * SQV
```

```
*-----selection of depth of canopy, canopy assimilation is set to zero
FGROS = 0.
IABS = 0.
DO 10 I1 = 1, IGAUSS
LAIC = LAI*XGAUSS(I1)
```

```
*-----absorbed fluxes per unit leaf area: diffuse flux, total direct
* flux, direct component of direct flux.
VISDF = (1.-REFH)*PARDF*KDF *EXP(-KDF *LAIC)
VIST = (1.-REFS)*PARDR*KDRT *EXP(-KDRT*LAIC)
VISD = (1.-SCP) *PARDR*KBL *EXP(-KBL *LAIC)
```

```
*-----absorbed flux (J/m2 leaf/s) for shaded leaves and assimilation of
* shaded leaves
VISSHD = VISDF + VIST - VISD
IF (AMAX.GT.0.) THEN
FGRSH = AMAX*(1.-EXP(-VISSHD*EFF/AMAX))
ELSE
FGRSH = 0.
END IF
```

```

*-----direct flux absorbed by leaves perpendicular on direct beam and
*      assimilation of sunlit leaf area
      VISPP = (1.-SCP) * PARDR / MAX(0.01,SINB)
      FGRSUN = 0.
      IABSUN = 0.
      DO 20 I2 = 1,IGAUSS
        VISSUN = VISSHD + VISPP *XGAUSS(I2)
        IF (AMAX.GT.0.) THEN
          FGRS = AMAX*(1.-EXP(-VISSUN*EFF/AMAX))
        ELSE
          FGRS = 0.
        END IF
        FGRSUN = FGRSUN + FGRS *WGAUSS(I2)
        IABSUN = IABSUN + VISSUN*WGAUSS(I2)
20      CONTINUE

*-----fraction sunlit leaf area (FSLLA) and local assimilation rate (FGL)
      FSLLA = CLUSTF* EXP(-KBL*LAIC)
      FGL = FSLLA * FGRSUN+(1.-FSLLA)*FGRSH
      IABSL = FSLLA * IABSUN+(1.-FSLLA)*VISSHD

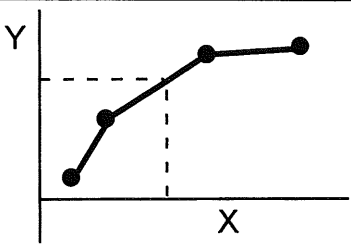
*-----integration of local assimilation rate to canopy assimilation (FGROS)
      FGROS = FGROS + FGL *WGAUSS(I1)
      IABS = IABS + IABSL*WGAUSS(I1)
10      CONTINUE

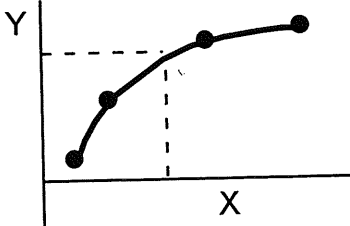
      FGROS = FGROS*LAI
      PARABS = IABS *LAI
      REFL = REFS *PARDR + REFH*PARDF
      SOIL = (1.-REFS)*PARDR*EXP(-KDRT*LAI) +
$      (1.-REFH)*PARDF*EXP(-KDF *LAI)
      PARINC = PARDF+PARDR
      BALANS = PARINC-REFL-SOIL-PARABS
      RETURN
      END

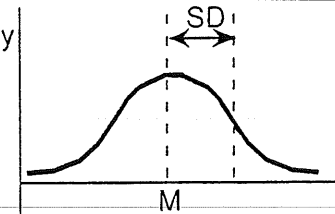
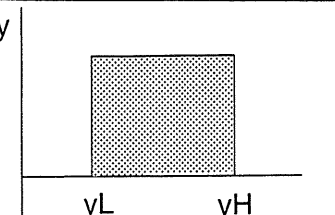
```


Appendix II: FST and FORTRAN intrinsic functions

List of FST intrinsic functions with explanation. The input arguments K and L denote an integer constant, variable or expression. Array arguments are written as A or B. The symbol F means an FST interpolation function and all other input arguments are real constants, variables or expressions. Taken from Rappoldt & van Kraalingen (1996).

FST function	Mathematical notation or Graph
$Y = \text{AFGEN}(F, X)$ Linear interpolation between (x,y) function points. Y - Result of interpolation, estimated F(X) F - Table of (x,y) values specified with FUNCTION statement X - Value of independent variable	
$Y = \text{ARIMPR}(A, B, K, L)$ Returns the improduct of a vector A and a vector B calculated over the subscript range K,...,L. Y - Returned improduct A - Array variable seen as vector B - Array variable seen as vector K - Start of subscript range L - End of subscript range with $L \geq K$	$y = \sum_{i=K}^L A_i B_i$
$Y = \text{ARLENG}(A, K, L)$ Returns the length of the vector with elements A(K),..., A(L) in (L-K+1)-dimensional space. Y - Returned length A - Array variable seen as vector K - Start of subscript range L - End of subscript range with $L \geq K$	$y = \sqrt{\sum_{i=K}^L A_i^2}$
$Y = \text{ARMAXI}(A, K, L)$ Returns the maximum value among the array elements A(K),..., A(L). Y - Resulting number A - Array variable K - Start of subscript range L - End of subscript range with $L \geq K$	$y = \max_{i=K}^L A_i$
$Y = \text{ARMEAN}(A, K, L)$ Returns the arithmetic mean of the array elements A(K),..., A(L). Y - Maximum value A - Array variable K - Start of subscript range L - End of subscript range with $L \geq K$	$y = \frac{\sum_{i=K}^L A_i}{L - K + 1}$

$Y = \text{ARMINI}(A, K, L)$ Returns the minimum value among the array elements $A(K), \dots, A(L)$. Y - Resulting number A - Array variable K - Start of subscript range L - End of subscript range with $L \geq K$	$y = \min_{i=K}^L A_i$
$Y = \text{ARSMPS}(A, K, L, D)$ Simpson's integral of a function over $L-K$ closed intervals $(x_K, x_{K+1}), (x_{K+1}, x_{K+2}), \dots, (x_{L-1}, x_L)$. At the $L-K+1$ points the function takes the values $A(K), \dots, A(L)$. All intervals have equal width D . Y - Approximate integral A - Array containing function values K - Start of subscript range L - End of subscript range with $L > K$ D - Interval width	$y = D \sum_{i=K}^L w_i A_i$ in with the coefficients w_i follow - trapezoidal rule for - extended $1/n^3$ rule for - alternative extended Simpson's rule for $n \geq 8$
$Y = \text{ARSTDV}(A, K, L)$ Returns the standard deviation of the array elements $A(K), \dots, A(L)$ seen as a sample. Y - Returned standard deviation A - Array variable K - Start of subscript range L - End of subscript range with $L > K$	$y = \sqrt{\frac{\sum_{i=K}^L (A_i - \bar{A})^2}{L - K}}$
$Y = \text{ARSUMM}(A, K, L)$ Returns the sum of the array elements $A(K), \dots, A(L)$. Y - Resulting sum A - Array variable K - Start of subscript range L - End of subscript range with $L \geq K$	$y = \sum_{i=K}^L A_i$
$Y = \text{CSPLIN}(F, X)$ Natural cubic splines interpolation between (x, y) function points according to Press <i>et al.</i> (1989). Y - Result of interpolation, estimated $F(X)$ F - Table of (x, y) values specified with FUNCTION statement X - Value of independent variable	
$Y = \text{ELEMNT}(A, K)$ Returns value of the K -th element of array A after verifying its existence by comparing K with the declared array bounds. Y - Returned element value A - Array variable K - Subscript	$y = A_K$

$Y = \text{FCNSW}(X, Y1, Y2, Y3)$ Input switch. Y is set equal to Y1, Y2 or Y3 depending on the value of X. Y - Returned as either Y1, Y2 or Y3 X - Control variable Y1 - Returned value of Y if $X < 0$ Y2 - Returned value of Y if $X = 0$ Y3 - Returned value of Y if $X > 0$	$\begin{cases} y=y_1, & x < 0 \\ y=y_2, & x = 0 \\ y=y_3, & x > 0 \end{cases}$
$Y = \text{INTGRL}(YI, YR)$ Integration command in the form of a function call. The algorithm of the numerical integration depends on the selected translation mode and driver. Y - State variable YI - Initial value of Y, must be a variable YR - Rate of change, must be a variable	$y(t) = y(0) + \int_0^t \frac{dy(t)}{dt} dt$
$Y = \text{INSW}(X, Y1, Y2)$ Input switch. Y is set equal to Y1 or Y2 depending on the value of X. Y - Returned as either Y1 or Y2 X - Control variable Y1 - Returned value of Y if $X < 0$ Y2 - Returned value of Y if $X \geq 0$	$\begin{cases} y=y_1, & x < 0 \\ y=y_2, & x \geq 0 \end{cases}$
$Y = \text{LIMIT}(XL, XH, X)$ Y is equal to X but limited between XL and XH Y - Returned as X bounded on [XL,XH] XL - Lower bound of X XH - Upper bound of X	$\begin{cases} y=x, & x_l \leq x \leq x_h \\ y=x_l, & x < x_l \\ y=x_h, & x > x_h \end{cases}$
$Y = \text{NOTNUL}(X)$ Y is equal to X but 1.0 in case of $X=0.0$. Note that X is evaluated without any tolerance interval. Y - Returned result X - Checked for being zero	$\begin{cases} y=x, & x \neq 0 \\ y=1, & x = 0 \end{cases}$
$Y = \text{REAAND}(X1, X2)$ Returns 1.0 if both input values are positive, otherwise $Y=0.0$.	$\begin{cases} y=1, & x_1, x_2 > 0 \\ y=0, & x_1 \leq 0 \text{ or } x_2 \leq 0 \end{cases}$
$Y = \text{REANOR}(X1, X2)$ Returns 1.0 if both input values are less than or equal to zero, otherwise $Y=0.0$.	$\begin{cases} y=1, & x_1, x_2 \leq 0 \\ y=0, & x_1 > 0 \text{ or } x_2 > 0 \end{cases}$
$Y = \text{RGNORM}(M, SD)$ Random number Generator which returns numbers with an univariate normal distribution. Y - Returned random number M - Mean of the normal distribution SD - Standard deviation of the distribution	
$Y = \text{RGUNIF}(YL, YH)$ Random number Generator which returns numbers with a uniform distribution on (YL,YH). Y - Returned random number YL - Lower bound of interval YH - Upper bound of interval	

List of Fortran intrinsic functions with explanation. The input arguments I and J denote an integer constant, variable or expression. The input arguments X, X1, X2, are real constants, variables or expressions. Taken from Rappoldt & van Kraalingen (1996).

Fortran function	Explanation	Mathematical notation	Restrictions
ABS (X)	absolute value of x	$ x $	
INT (X)	the integer part of x, result is integer	$\text{int}(x)$	
AINTE (X)	the integer part of x, converted to real	$\text{int}(x)$	
NINT (X)	the nearest integer, result is integer	$\text{int}(x)$	
ANINT (X)	the nearest integer converted to real	$\text{int}(x)$	
MAX (X1, X2, ..., Xn)	maximum value among the real arguments	$\max(x_1, x_2, \dots, x_n)$	$n \geq 2$
AMAX (X1, X2, ..., Xn)	maximum value among the real arguments	$\max(x_1, x_2, \dots, x_n)$	$n \geq 2$
MIN (X1, X2, ..., Xn)	minimum value among the real arguments	$\min(x_1, x_2, \dots, x_n)$	$n \geq 2$
AMIN (X1, X2, ..., Xn)	minimum value among the real arguments	$\min(x_1, x_2, \dots, x_n)$	$n \geq 2$
MOD (I, J)	remainder of i/j with sign of i, result is integer	$i \bmod j$	$j \neq 0$
AMOD (X, Y)	remainder of x/y with sign of x, result is real	$x \bmod y$	$y \neq 0$
COS (X)	cosine of x, x in radians	$\cos(x)$	
COSH (X)	hyperbolic cosine of x	$\cosh(x)$	
ACOS (X)	arccosine of x in range $[0, \pi]$	$\arccos(x)$	$-1 \leq x \leq 1$
EXP (X)	exponential function	e^x	
LOG (X)	natural logarithm of x	$e \log x$	$x > 0$
ALOG (X)	natural logarithm of x	$e \log x$	$x > 0$
LOG10 (X)	base 10 logarithm of x	$10 \log x$	$x > 0$
ALOG10 (X)	base 10 logarithm of x	$10 \log x$	$x > 0$
REAL (I)	the real number nearest to integer I		
SQRT (X)	square root of x	\sqrt{x}	$x \geq 0$
SIN (X)	sine of x, x in radians	$\sin(x)$	
SINH (X)	hyperbolic sine of x	$\sinh(x)$	
ASIN (X)	arc sin of x in range $[-\pi/2, \pi/2]$	$\arcsin(x)$	$-1 \leq x \leq 1$
TAN (X)	tangent of x, x in radians	$\tan(x)$	$x \bmod \pi/2 \neq \pi/4$
TANH (X)	hyperbolic tangent of x	$\tanh(x)$	
ATAN (X)	arc tangent of x in range $[-\pi/2, \pi/2]$	$\arctan(x)$	
ATAN2 (X, Y)	arc tangent of x/y in range $[-\pi/2, \pi/2]$	$\arctan(x/y)$	

Appendix III: Definition of abbreviations

Name	Description	Units
A	Parameter in the Ångström formula	-
AEVAP	Actual soil evaporation rate, derived from Penman evaporation	mm d ⁻¹
AINTC	Actual amount of precipitation intercepted by the canopy	mm d ⁻¹
ALB	Albedo, reflection coefficient, for short-wave radiation	-
ALBS	Albedo, reflection coefficient, for soil surface	-
AMAX	Actual CO ₂ assimilation rate at light saturation for individual leaves	g CO ₂ m ⁻² leaf s ⁻¹
AMDVS	Factor accounting for effect of development stage on AMX	-
AMDVST	Table of AMDVS as a function of DVS	-, -
AMTMP	Factor accounting for effect of daytime temperature on AMX	-
AMTMPT	Table of AMTMP as function of DDTMP	-, °C
AMX	Potential CO ₂ assimilation rate at light saturation for individual leaves	g CO ₂ m ⁻² leaf s ⁻¹
AOB	Intermediate variable	-
ASIN	Arcsine function (intrinsic FORTRAN function)	-
ASRQ	Assimilate (CH ₂ O) requirement for dry matter prod.	g CH ₂ O g ⁻¹ DM
ASRQLV	Assimilate requirement for leaf dry matter production	g CH ₂ O g ⁻¹ DM leaf
ASRQRT	Assimilate requirement for root dry matter production	g CH ₂ O g ⁻¹ DM root
ASRQSO	Assimilate requirement for storage organ dry matter production	g CH ₂ O g ⁻¹ DM stor. organs
ASRQST	Assimilate requirement for stem dry matter production	g CH ₂ O g ⁻¹ DM stem
ASSIM	FORTTRAN subroutine to calculate FGROS	-
ASTRO	FORTTRAN subroutine to compute e.g. daylength	-
ATMTR	Atmospheric transmission coefficient	-
ATRANS	Total actual transpiration rate of the canopy	mm d ⁻¹
AVP	Actual vapour pressure	kPa
B	Parameter in Ångström formula	-
BBRAD	Black body radiation	J m ⁻² s ⁻¹
BOLTZM	Stefan-Boltzmann constant	J m ⁻² d ⁻¹ °K ⁻⁴
CFLV	Mass fraction carbon in the leaves	g C g ⁻¹ DM
CFRT	Mass fraction carbon in the roots	g C g ⁻¹ DM
CFSO	Mass fraction carbon in the storage organs	g C g ⁻¹ DM
CFST	Mass fraction carbon in the stems	g C g ⁻¹ DM
CHECK	Variable to check the water balance (should be zero)	mm
CHKDIF	Difference between carbon added to the crop since initialization and the net total of integrated carbon fluxes, relative to their sum	-
CHKIN	Carbon in the crop accumulated since simulation started	g C m ⁻²
CHKFL	Sum of integrated carbon fluxes into and out of the crop	g C m ⁻²
CLUSTF	Cluster factor	-
CLEAR	Penman's original clearness factor	-
CONVL	Conversion factor for remobilization of stem carbohydrates into glucose	-
COS	Cosine function (intrinsic FORTRAN function)	-
COSLD	Intermediate variable in calculating solar height	-
CO2LV	CO ₂ production factor for growth of leaves	g CO ₂ g ⁻¹ DM
CO2RT	CO ₂ production factor for growth of roots	g CO ₂ g ⁻¹ DM
CO2SO	CO ₂ production factor for growth of storage organs	g CO ₂ g ⁻¹ DM
CO2ST	CO ₂ production factor for growth of stems	g CO ₂ g ⁻¹ DM
CPEW	Factor accounting for effect of water stress on DM partitioning	-
CROPF	Crop factor for crop water requirement	-
DAVTMP	Daily average temperature	°C
DAY	Day number since 1 January (day of year)	d
DAYL	Daylength	h d ⁻¹
DDTMP	Daily average daytime temperature	°C
DEC	Declination of the sun	radians
DELT	Time interval of integration	d
DLAI	Death rate of leaf area	m ² m ⁻² d ⁻¹
DLV	Death rate of leaves	g leaf m ⁻² d ⁻¹
DOY	Day number since 1 January (day of year) (from AB/TPE weather system)	d
DOYEM	Day of year of crop emergence	d

DPAR	Daily photosynthetic active radiation	$\text{J m}^{-2} \text{d}^{-1}$
DRAIN	Drainage rate below the root zone	mm d^{-1}
DRYP	Drying power term in Penman equation	$\text{mm d}^{-1} \text{kPa } ^\circ\text{C}^{-1}$
DSO	Daily extra-terrestrial radiation	$\text{J m}^{-2} \text{d}^{-1}$
DSINB	Integral of SINB over the day	s d^{-1}
DSINBE	As DSINB, but with a correction for lower atmospheric transmission at lower solar elevations	s d^{-1}
DSLRL	Number of days since last rain	d
DTEFF	Daily effective temperature	$^\circ\text{C}$
DTGA	Daily total gross CO_2 assimilation of the crop	$\text{g CO}_2 \text{ m}^{-2} \text{ ground d}^{-1}$
DTGAS	Total gross CO_2 assimilation of the crop	$\text{g CO}_2 \text{ m}^{-2} \text{ ground s}^{-1}$
DTMAX	Daily maximum temperature	$^\circ\text{C}$
DTMIN	Daily minimum temperature	$^\circ\text{C}$
DTR	Daily solar radiation	$\text{J m}^{-2} \text{d}^{-1}$
DTRT	Table of DTR as function of day of the year	$\text{J m}^{-2} \text{d}^{-1}, \text{d}$
DVR	Development rate	d^{-1}
DVRR	Table of DVR in post-anthesis phase as function of temperature	$\text{d}^{-1}, ^\circ\text{C}$
DVRV	Table of DVR in pre-anthesis phase as function of temperature	$\text{d}^{-1}, ^\circ\text{C}$
DVS	Development stage of the crop	-
EAI	Ear area index	$\text{m}^2 \text{ ear m}^{-2} \text{ ground}$
EAR	Ear area/weight ratio	$\text{m}^2 \text{ ear g}^{-1} \text{ DM TADRW}$
EDPTFT	Table to read the root activity coefficient	-
EES	Soil-specific extinction coefficient	mm^{-1}
EFF	Initial light conversion factor for individual leaves	$\text{g CO}_2 / \text{J}$
EMERG	Parameter to indicate emergence	-
ERLB	Cumulative effective root length	mm
ERRSH	Check in partitioning tables (total should be 1.)	-
EVAPD	Potential soil evaporation due to drying power of the air	mm d^{-1}
EVAPR	Potential soil evaporation due to radiation	mm d^{-1}
EVSD	Evaporation rate on days without rain	mm d^{-1}
EVSH	Evaporation rate on days with rain	mm d^{-1}
EVSW1-4	Rate of evaporation	mm d^{-1}
EZRT	Rate of root elongation	mm d^{-1}
EZRTC	Constant for root elongation	mm d^{-1}
FCLEAR	Sky clearness function in calculation of net long-wave radiation	-
FEVL1-4	Distribution factors for soil water extraction over compartments	-
FEVLT	Sum of FEVL	-
FGL	CO_2 assimilation rate at one depth in the canopy	$\text{g CO}_2 \text{ m}^{-2} \text{ leaf s}^{-1}$
FGROS	Instantaneous canopy CO_2 assimilation	$\text{g CO}_2 \text{ m}^{-2} \text{ ground s}^{-1}$
FGRS	Intermediate variable for calculation of assimilation of sunlit leaves	-
FGRSH	CO_2 assimilation rate at one depth in the canopy for shaded leaves	$\text{g CO}_2 \text{ m}^{-2} \text{ leaf s}^{-1}$
FGRSUN	CO_2 assimilation rate at one depth in the canopy for sunlit leaves	$\text{g CO}_2 \text{ m}^{-2} \text{ leaf s}^{-1}$
FINTIM	Period of simulation	d
FLV	Fraction of shoot dry matter allocated to leaves	-
FLVTB	Table of FLV as function of DVS	-, -
FRDF	Fraction diffuse in incoming radiation	-
FRDR	Parameter to determine rate of increase in RDR	-
FRT	Fraction total dry matter allocated to roots	-
FRTRL	Fraction stem weight eventually translocated to storage organs	-
FSH	Fraction total dry matter allocated to shoots	-
FSHP	Fraction total dry matter allocated to shoots (water-limited production)	-
FSHTB	Table of FSH as function of DVS	-, -
FSLLA	Fraction of sunlit leaf area	-
FSO	Fraction of shoot dry matter allocated to storage organs	-
FST	Fraction of shoot dry matter allocated to stems	-
FSTTB	Table of FST as function of DVS	-, -
FVAP	Vapour pressure effect on RWLN (Brunt equation)	-
GLA	FORTTRAN subroutine to calculate GLAI	-
GLAI	Net growth rate of leaf area index	$\text{m}^2 \text{ leaf m}^{-2} \text{ ground d}^{-1}$
GLV	Dry matter growth rate of leaves	$\text{g DM m}^{-2} \text{ ground d}^{-1}$
GPHOT	Daily total gross CH_2O assimilation of the crop	$\text{g CH}_2\text{O m}^{-2} \text{ ground d}^{-1}$
GRT	Dry matter growth rate of roots	$\text{g DM m}^{-2} \text{ ground d}^{-1}$
GSO	Dry matter growth rate of storage organs	$\text{g DM m}^{-2} \text{ ground d}^{-1}$

GST	Dry matter growth rate of stems	$\text{g DM m}^{-2} \text{ ground d}^{-1}$
GTW	Gross growth rate of crop dry matter, including translocation	$\text{g DM m}^{-2} \text{ ground d}^{-1}$
HI	Harvest index	$\text{g stor. organs g}^{-1} \text{ TADRW}$
HOURL	Selected hour during the day	h
I1	Do-loop counter	-
I2	Do-loop counter	-
IEAI	Initial ear area index	$\text{m}^2 \text{ ear m}^{-2} \text{ ground}$
IDSLR	Initial of DSLR	d
IDVS	Initial development stage	-
IGAUSS	Do-loop counter	-
ILAI	Initial leaf area index	$\text{m}^2 \text{ leaf m}^{-2} \text{ ground}$
INTC	Interception capacity of precipitation of 1 layer of leaves	mm d^{-1}
KBL	Extinction coefficient for direct component of direct PAR flux	$\text{m}^2 \text{ ground m}^{-2} \text{ leaf}$
KDF	Extinction coefficient for leaves	$\text{m}^2 \text{ ground ha}^{-1} \text{ leaf}$
KDRT	Extinction coefficient for total direct PAR flux	$\text{m}^2 \text{ ground ha}^{-1} \text{ leaf}$
LAI	Leaf area index	$\text{m}^2 \text{ leaf m}^{-2} \text{ ground}$
LAIC	Leaf area index above selected height in canopy	$\text{m}^2 \text{ leaf m}^{-2} \text{ ground}$
LAICR	Critical leaf area index beyond which death to self-shading occurs	$\text{m}^2 \text{ leaf m}^{-2} \text{ ground}$
LAITB	Table of LAI as function of day of the year	$\text{m}^2 \text{ leaf m}^{-2} \text{ ground, d}$
LAT	Latitude of the weather station (from AB/TPE weather system)	degrees
LATT	Latitude of the weather station	degrees
LONG	Longitude of weather station (from AB/TPE weather system)	degrees
LHVAP	Latent heat of evaporation of water	$\text{J kg}^{-1} \text{ H}_2\text{O}$
MAINLV	Maintenance respiration coefficient of leaves	$\text{g CH}_2\text{O g}^{-1} \text{ DM d}^{-1}$
MAINRT	Maintenance respiration coefficient of roots	$\text{g CH}_2\text{O g}^{-1} \text{ DM d}^{-1}$
MAINSO	Maintenance respiration coefficient of storage organs	$\text{g CH}_2\text{O g}^{-1} \text{ DM d}^{-1}$
MAINST	Maintenance respiration coefficient of stems	$\text{g CH}_2\text{O g}^{-1} \text{ DM d}^{-1}$
MAINT	Maintenance respiration rate of the crop	$\text{g CH}_2\text{O m}^{-2} \text{ d}^{-1}$
MAINTS	Maintenance respiration rate of the crop at reference temperature	$\text{g CH}_2\text{O m}^{-2} \text{ d}^{-1}$
MDRATE	Maximum drainage rate of the subsoil	mm d^{-1}
MNDVS	Factor accounting for effect of DVS on maintenance respiration	-
NRAD	Net radiation	$\text{J m}^{-2} \text{ d}^{-1}$
P	Soil water depletion fraction	-
PAR	Instantaneous flux of photosynthetically active radiation	$\text{J m}^{-2} \text{ ground s}^{-1}$
PARDF	Instantaneous diffuse flux of incoming PAR	$\text{J m}^{-2} \text{ ground s}^{-1}$
PARDR	Instantaneous direct flux of incoming PAR	$\text{J m}^{-2} \text{ ground s}^{-1}$
PCEW	Factor that accounts for reduced photosynthesis due to water stress	-
PENMAN	Penman reference value for potential evaporation	mm d^{-1}
PEVAP	Potential soil evaporation	mm d^{-1}
PI	Ratio of circumference to diameter of circle	-
PRDEL	Time interval for printing	d
PSYCH	Psychromatic instrument constant	$\text{kPa } ^\circ\text{C}^{-1}$
PTRANS	Potential transpiration rate derived from Penman evaporation	mm d^{-1}
Q10	Factor accounting for increase in maintenance respiration with a 10 °C rise temperature	-
RAD	Factor to convert degrees to radians	$\text{radians degree}^{-1}$
RAIN	Daily precipitation (from AB/TPE weather system)	mm d^{-1}
RDR	Relative death rate of leaves	d^{-1}
RDRDV	Relative death rate due to developmental ageing	d^{-1}
RDRSH	Relative death rate due to self-shading at high LAI	d^{-1}
RDRT	Table of RDR as function of DAVTMP	$\text{d}^{-1}, ^\circ\text{C}$
REAI	Growth rate ear area index	$\text{m}^2 \text{ m}^{-2} \text{ d}^{-1}$
REDF	Factor accounting for effect of temperature on AMAX	-
REFH	Reflection coefficient for diffuse PAR	-
REFS	Reflection coefficient for direct PAR	-
RGRL	Relative growth rate of leaf area during exponential growth	$(^\circ\text{C d})^{-1}$

RLWN	Net long-wave radiation	$\text{J m}^{-2} \text{d}^{-1}$
RNOFF	Runoff	mm d^{-1}
RRAIN	Daily precipitation	mm d^{-1}
RWL1-4	Rate of increase for WL1-4	mm d^{-1}
RWCL1-4	Relative available volumetric water content in soil layers	-
SC	Solar constant, corrected for varying distances between sun-earth	$\text{J m}^{-2} \text{s}^{-1}$
SCP	Scattering coefficient of leaves for PAR	-
SINB	Sine of solar elevation	-
SINLD	Intermediate variable in calculating solar declination	-
SLA	Specific leaf area	$\text{m}^2 \text{leaf g}^{-1} \text{leaf}$
SLOPE	Tangent of the relationship between saturated vapour pressure and temperature	$\text{kPa } ^\circ\text{C}^{-1}$
STTIME	Time start simulation	d
SQV	Intermediate variable in calc. of reflection coefficient	-
SUBEAI	FORTTRAN subroutine to compute REAI	-
SUBFR	FORTTRAN subroutine to compute WSE	-
SUBGRT	FORTTRAN subroutine to compute WSERT	-
SVP	Saturated vapour pressure	kPa
TADRW	Total above-ground dry matter	g DM m^{-2}
TAEVAP	Cumulative actual soil evaporation	mm
TAINTC	Total amount of rainfall intercepted by the canopy	mm
TAI	Total area index	$\text{m}^2 \text{m}^{-2} \text{ground}$
TAR	transpiration / assimilation ratio	$\text{kg H}_2\text{O kg}^{-1} \text{CO}_2$
TATRAIN	Total amount of water transpired by the crop	mm
TBASE	Base temperature for juvenile leaf area growth	$^\circ\text{C}$
TDRAIN	Total drainage	mm
TDRW	Total biomass	g DM m^{-2}
TDGTA	Total gross CO_2 assimilation of the crop	$\text{g CO}_2 \text{m}^{-2} \text{ground}$
TEFF	Factor accounting for effect of temperature on maintenance respiration	-
TEVAPD	Cumulative potential soil evaporation due to drying power of the air	mm
TEVAPR	Cumulative potential soil evaporation due to radiation	mm
TKL1-4	Thickness of the soil layers	mm
TKLT	Sum of thickness of the soil layers	mm
TMAXT	Table daily max. temp. as function of day of the year	$^\circ\text{C}, \text{d}$
TMINT	Table daily min. temp. as function of day of the year	$^\circ\text{C}, \text{d}$
TMMX	Daily maximum temperature (from AB/TPE weather system)	$^\circ\text{C}$
TMMN	Daily minimum temperature (from AB/TPE weather system)	$^\circ\text{C}$
TNASS	Total net CO_2 assimilation	$\text{g CO}_2 \text{m}^{-2}$
TNASSI	Initial value of TNASS	$\text{g CO}_2 \text{m}^{-2}$
TOTASS	FORTTRAN subroutine to calculate the gross CO_2 assimilation of the crop	-
TPENM	Cumulative potential evapotranspiration	mm
TPEVAP	Cumulative potential ecaporation	mm
TPTRAN	Cumulative actual soil evaporation	mm
TRAIN	Total precipitation	mm
TRANSC	Characteristic potential transpiration rate (see Table 2.2)	mm d^{-1}
TRANSL	Translocation rate of stem dry matter to storage organs	$\text{g DM m}^{-2} \text{d}^{-1}$
TRC	Transpiration coefficient	$\text{kg H}_2\text{O kg}^{-1} \text{DM}$
TREF	Reference temperature	$^\circ\text{C}$
TRNOFF	Total runoff	mm
TRRM	Potential rate of water uptake per mm effective rooted depth	d^{-1}
TRWL1-4	Rate of transpiration	mm d^{-1}
TSTORE	Total surface storage due to waterlogging	mm
VISD	Absorbed direct component of direct flux per unit leaf area (at depth LAIC)	$\text{J m}^{-2} \text{leaf s}^{-1}$
VISDF	Absorbed diffuse flux per unit leaf area (at depth LAIC)	$\text{J m}^{-2} \text{leaf s}^{-1}$
VISPP	Absorbed light flux by leaves perpendicular on direct beam	$\text{J m}^{-2} \text{leaf s}^{-1}$
VISSHD	Total absorbed flux for shaded leaves per unit leaf area (at depth LAIC)	$\text{J m}^{-2} \text{leaf s}^{-1}$
VISSUN	Total absorbed flux for sunlit leaves in one of three Gauss point classes	$\text{J m}^{-2} \text{leaf s}^{-1}$
VIST	Absorbed total direct flux per unit leaf area (at depth LAIC)	$\text{J m}^{-2} \text{leaf s}^{-1}$
VP	Actual vapour pressure (from AB/TPE weather system)	kPa

WCAD1-4	Volumetric water content in each soil layer at dry air	$\text{cm}^3 \text{H}_2\text{O cm}^{-3} \text{soil}$
WCCR	Critical volumetric water content	$\text{cm}^3 \text{H}_2\text{O cm}^{-3} \text{soil}$
WCFC1-4	Volumetric water content at field capacity in each soil layer	$\text{cm}^3 \text{H}_2\text{O cm}^{-3} \text{soil}$
WCL1-4	Volumetric water content in each soil layer	$\text{cm}^3 \text{H}_2\text{O cm}^{-3} \text{soil}$
WCL1-4	Initial values for WCL1-4	$\text{cm}^3 \text{H}_2\text{O cm}^{-3} \text{soil}$
WCUM	Total amount of water in the soil profile	mm
WCUMI	Initial value for WCUM	mm
WCWET1-4	Volumetric water content where water logging begins	$\text{cm}^3 \text{H}_2\text{O cm}^{-3} \text{soil}$
WCWP1-4	Volumetric water content at wilting point in each soil layer	$\text{cm}^3 \text{H}_2\text{O cm}^{-3} \text{soil}$
WDF	Wind function	$\text{mm d}^{-1} \text{ } ^\circ\text{C}^{-1}$
WDS	Wind speed	m s^{-1}
WGAUSS	Array containing weights to be assigned to Gauss points	-
WL1-4	Amount of water in soil compartments	mm
WL11-WL41	Initial amounts for WL1-4	mm
WLFL1-4	Infiltration and drainage rates for the soil layer	mm d^{-1}
WLV	Dry weight of the leaves (green + dead)	g m^{-2}
WLVD	Dry weight of dead leaves	g m^{-2}
WLVDI	Initial value for WLVD	g m^{-2}
WLVG	Dry weight of green leaves	g m^{-2}
WLVl	Initial dry weight of the leaves	g m^{-2}
WN	Wind speed (from AB/TPE weather system)	m s^{-1}
WRT	Dry weight of the roots	g m^{-2}
WRTI	Initial dry weight of the roots	g m^{-2}
WSE1-4	Factor accounting for effect of uptake availability of soil water	-
WSERT	Auxiliary variable to calculate root extension	-
WSO	Dry weight of storage organs	g m^{-2}
WSOI	Initial value for WSO	g m^{-2}
WST	Dry weight of the stems	g m^{-2}
WSTI	Initial value for WST	g m^{-2}
XGAUSS	Array containing Gauss points	-
ZERO	Initial value of zero in an integration	-
ZRT	Rooted depth	mm
ZRT1-4	Thickness of rooted layer	mm
ZRTI	Initial value for ZRT	mm
ZTRM	Maximum value for rooted depth	mm
ZRTMC	Maximum value for rooted depth as crop characteristic	mm
ZRTMS	Maximum value for rooted depth as soil characteristic	mm

