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**A CLOSED SYSTEM FOR MEASUREMENT  
OF PHOTOSYNTHESIS, RESPIRATION AND  
CO<sub>2</sub> COMPENSATION POINTS**

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# A CLOSED SYSTEM FOR MEASUREMENT OF PHOTOSYNTHESIS, RESPIRATION AND CO<sub>2</sub>-COMPENSATION POINTS

## INTRODUCTION

Fundamental data for the production of glass-house crops in relation to temperature, light and CO<sub>2</sub>-conc. are greatly needed. Nowadays, advanced equipment is available to control temperature and CO<sub>2</sub>-conc. in the glass-house climate. An efficient temperature regulation is now extremely important, because of the amount of energy required to heat the glass-house. In practice the application of artificial light is useful but depends to a large extent on economic factors. Data about the relation between temperature, light and CO<sub>2</sub> on photosynthesis of glass-house crops are scanty.

Many research workers have built open, semi-closed or closed systems or have discussed aspects, which have to be considered in building such a system (ACOCK 1974; JARVIS et al. 1971). At the Agricultural University and Research Institutes in Wageningen, The Netherlands, open systems have been built for measurements of leaves (CHALLA 1976; GAASTRA 1959; PIETERS 1974), whole plants (LOUWERSE and VAN OORSCHOT 1969) or stands (LOUWERSE and EIKHOUDT 1975). VERFAILLIE (1972) constructed a closed system in which the environmental control of the aerial part and the control of the roots was separated. The equipment was used for grains (e.g. rice) and could not be applied to vegetables such as lettuce and sweet pepper. A closed system facilitates the measurement of CO<sub>2</sub>-exchange from high external CO<sub>2</sub>-conc. to levels as low as the CO<sub>2</sub>-compensation point. HEATH and MEIDNER (1967) stated that data obtained in that way give information about possible practical use of CO<sub>2</sub>-application. The CO<sub>2</sub>-compensation point gives information about the photosynthetic efficiency of plants. For these reasons a relatively simple and cheap apparatus is constructed, based on the principle of a closed system and suitable for glass-house crops.

## METHODS AND APPARATUS

### *General description*

Fig. 1 is a diagram of the equipment which consists of the following components: plant chamber and pot chamber, the equipment for light- and temperature control. The infra-red gas-analyser and a 24 channel mV-recorder are not shown in Fig. 1. The closed circuit with the perspex plant chamber (Pl.ch.) and the temperature control equipment is placed on a metal trolley (g; 800 × 880 × 960 mm) with universal wheels (h<sub>1</sub>-h<sub>4</sub>). This trolley can be pushed under and beside the frame (e). Details of the perspex chamber and temperature control equipment will be given in subsequent paragraphs.

The light equipment consists of 5 Philips high intensity mercury vapour lamps (a<sub>1</sub>-a<sub>5</sub>; HPLR of 400 W each), arranged at 250 mm from each other,

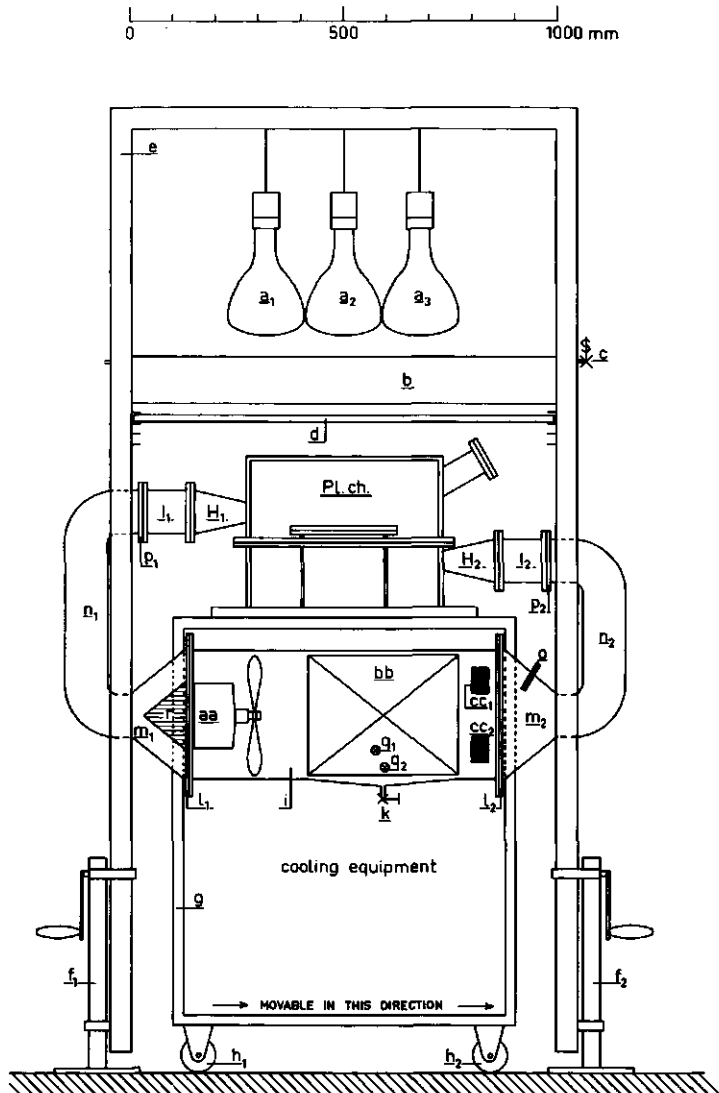


Fig. 1. Diagram of the equipment. All sizes in mm.  $a_1$ - $a_3$  = lamps, aa = fan and motor, b = water bath, bb = cooling coil, c = valve, cc<sub>1</sub> and cc<sub>2</sub> = air-heating elements, d<sub>1</sub>-d<sub>5</sub> = metal screens, e = metal frame, f<sub>1</sub>-f<sub>4</sub> = screw jacks, g = metal trolley, h<sub>1</sub>-h<sub>4</sub> = universal wheels, i = copper duct, I<sub>1</sub>-I<sub>2</sub> = perspex interunits, k = drain cock, l<sub>1</sub>-l<sub>2</sub> = copper flanges, m<sub>1</sub>-m<sub>2</sub> = copper interunits, n<sub>1</sub>-n<sub>2</sub> = flexible tubes, o = temperature sensor, p<sub>1</sub>-p<sub>2</sub> = perspex flanges, Pl.ch = plant chamber, q<sub>1</sub>-q<sub>2</sub> = places of transits through the copper duct, r = copper cone fixed on aa.

measured from the central lamp. Light intensity is regulated by movable metal screens (d) with a different size and a different number of perforations. A range of irradiance between 0 and 215 W m<sup>-2</sup> (400-700 nm) at plant level can be realized. The difference in light intensity at the horizontal direction in

the plant chamber is less than 15%. A water bath (b) was installed in order to reduce the long wave radiation. The distance from the water bath to the lamps is 50 mm and from the water bath to the plant chamber 120 mm. The temperature in the water bath is regulated between 12° and 35°C with a thermostat, which operates a valve (c) for the tap-water supply. Lamps, water bath and screens are mounted on a metal frame (e; U-tube, 2250 × 1090 × 1090 mm), the height of which can be increased 400 mm by 4 hand-operated screw jacks (f<sub>1</sub>-f<sub>4</sub>). More details of the equipment are given in the Appendix.

A copper duct i (700 × 320 × 424 mm) is equipped with a fan (aa), a cooling coil (bb) and 2 air-heating elements (cc<sub>1</sub> and cc<sub>2</sub>). A copper cone r is fixed on aa and placed in the airstream. The drain cock (k) is inserted at the lowest point of the duct in order to drain superfluous water. At points q<sub>1</sub> and q<sub>2</sub> 2 copper tubes connect the cooling coil with the cooling equipment at the bottom of the trolley. The copper tubes and 3 transits for electric wires through the copper duct are hermetically sealed with Bucarit-aquarium putty. The duct is connected at both ends to sloping copper units (m<sub>1</sub> and m<sub>2</sub>) by means of copper flanges (l<sub>1</sub> and l<sub>2</sub>) and bolts and hermetically clothed with foamed cellrubber. The sloping units are connected with flexible tubes (∅ 100 mm) to the inlet (n<sub>2</sub>) and to the outlet (n<sub>1</sub>) of the plant chamber. The copper part is isolated with Armaflex rubber and the flexible tubes are wrapped in Virginia foam rubber tape. A temperature sensor (o) for the temperature control equipment is placed at unit m<sub>2</sub>. The length of tube n<sub>1</sub> can be varied for various heights of the plant chamber. Both tubes (n<sub>1</sub> and n<sub>2</sub>) have perspex flanges (p<sub>1</sub> and p<sub>2</sub>) which connect the perspex interunits I<sub>1</sub> and I<sub>2</sub> by means of bolts and a quad ring (∅ 113 × 6 mm). The room temperature can be varied between 10° and 34°C with an accuracy of ± 0.8°C by means of thermostatic controlled electric heaters and a cooling battery (s).

#### *Details of the plant chamber*

The plant chamber (Fig. 2) consists of a perspex (polymethylmethacrylate) cylinder (A; h = 150 mm) mounted on a solid perspex bottom plate (B; ∅ 620 mm; h = 25 mm) and an upper unit (C) with an internal height of 190 mm. The height of the cylinder can be increased with 2 interunits (D and E) with heights of 100 and 250 mm, resp. (not shown in Fig. 2). The inner diameter of the cylinders (A, C, D, E) is 441 mm and the wall thickness 8 mm. The units are airtight connected with O-rings (∅ 480 × 6 mm) and 6 adjustable metal clips (F). The total volume of the closed circuit with A and C is 180 litres. This volume (b) was calculated from the increase of the CO<sub>2</sub>-concentration (ΔCO<sub>2</sub>) after injection of a known volume (Δv) of pure CO<sub>2</sub> into the system according to the equation  $\Delta v = a + b\Delta CO_2$ . In plotting Δv against ΔCO<sub>2</sub> a straight line was obtained from which the volume was calculated. When there is no leakage, the symbol a is zero in the equation.

Cylinder A is provided with perspex tubes (G<sub>1</sub>-G<sub>4</sub>) which are used to insert wires for sensor elements, electrical cables and copper tubes conducting the

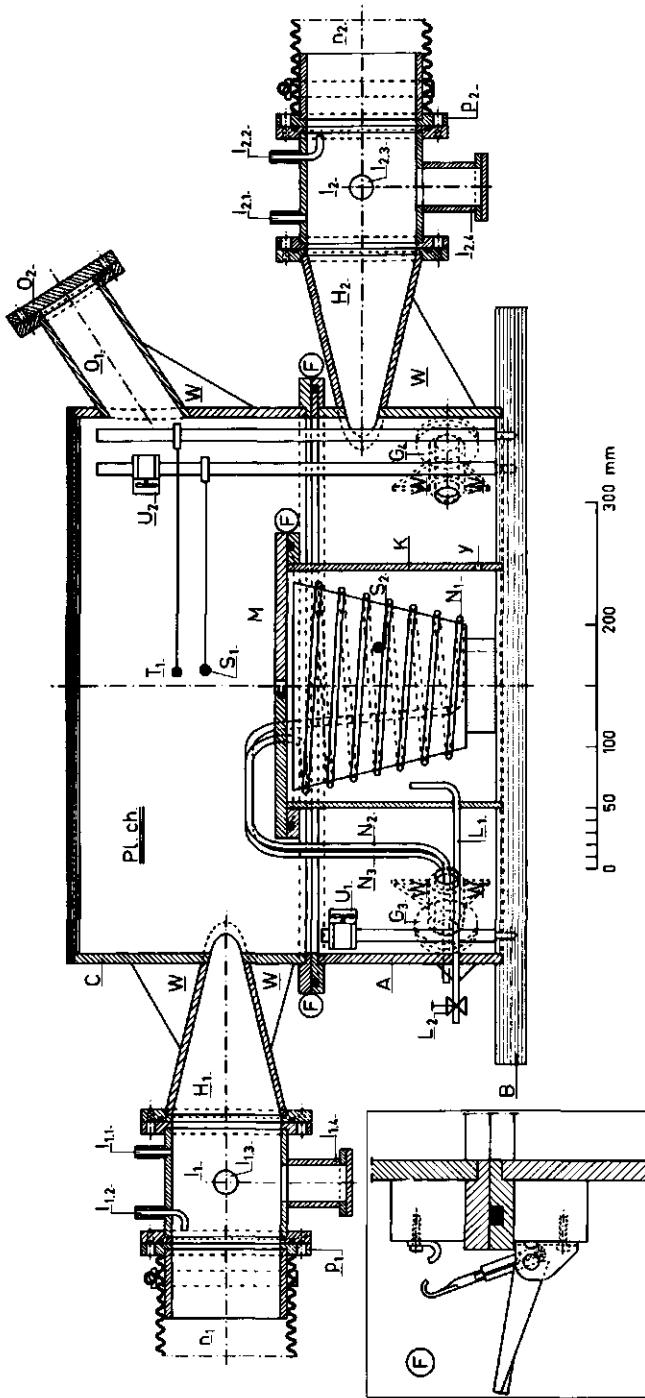


Fig. 2. Diagram of the plant chamber. All sizes in mm. A = perspex basal unit, B = solid perspex bottom plate, C = perspex upper unit, D and E = perspex interunits, F = metal clips (see detail), G = perspex tubes ( $\varnothing 40 \times 30$ ;  $l_1 = 32$ ),  $H_2$  = perspex air inlet (opening with Pl.ch.: 210 wide and maximally 40 high),  $H_1$ , perspex air outlet,  $I_1$  and  $I_2$  = perspex interunits ( $\varnothing 110 \times 100$ ,  $l = 100$ ),  $I_1, I_1, I_1, I_2, I_2, I_1$  and  $I_2$  = perspex tubes ( $\varnothing 24 \times 12$ ;  $l = 15$ ),  $I_1, I_1$  and  $I_2, I_2$  = perspex tubes, similar to G, K = perspex pot chamber ( $\varnothing 200 \times 190$ ;  $h = 190$ ),  $L_1$  = perspex tube ( $\varnothing 5 \times 3$  mm;  $l = 180$  mm),  $L_2$  = valve, M = perspex disk ( $\varnothing 250$ ; thickness 10),  $n_1$  and  $n_2$  = flexible tubing,  $N_1$  = copper spiral ( $\varnothing 6 \times 4$ ),  $N_2, N_3$  = plastic tubes,  $O_1$  = perspex tube ( $\varnothing 60 \times 50$ ;  $l = 75$ ),  $O_2$  = perspex flange,  $P_1, P_2$  = perspex flanges, Pl.ch. = plant chamber,  $S_1$  and  $S_2$  = thermocouples,  $T_1$  = photocells,  $U_1$  and  $U_2$  = fans,  $W$  = perspex supports,  $Y$  = place of transit for a thermocouple wire.

thermostat controlled water to achieve any desired temperature of the pot in the chamber. The tubes  $G_1$ – $G_4$  are filled with perspex stops to prevent  $\text{CO}_2$ -pockets in the closed circuit. Air leakage is prevented by use of perspex stop flanges, bolts and airtight foamed cell rubber. The air inlet ( $H_2$ ) is connected to the interunit  $I_2$  by a flange and a quad ring ( $\varnothing 113 \times 6$  mm). In the subscript of Fig. 2 those dimensions of the various parts are given, which have not been mentioned here. The bottom plate is provided with holes with screw thread to insert PVC bars on which sensors can be fitted. A perspex cylinder (K), the pot chamber, is glued onto the bottom plate in which a pot with a soil-volume of almost 2,3 litres can be inserted. The cylinder is provided with a perspex tube ( $L_1$ ) for supply of water and air via a valve ( $L_2$ ).  $W$  are perspex supports. Point Y is the place for a transit of thermocouple wires.

An airtight seal of the pot chamber with the pot is obtained by means of a flat disk (M) of 2 segments, an O-ring ( $\varnothing 226 \times 6$  mm) and metal clips (F). Disks with different slot sizes are used because of various thicknesses of the plant stems. The slot is sealed with aquarium putty after inserting the pot with the plant in the pot chamber. The temperature of the pot can be regulated in a range between 15–35°C by a copper tube ( $N_1$ ) bent into a spiral ( $l = 225$  or  $315$  cm) and connected to an isolated water bath ( $N_4$ ) of 10 litres which contains a portable thermoregulator ( $N_5$ ) and a cooling unit ( $N_6$ ).  $N_2$  and  $N_3$  are plastic tubes.  $N_4$ – $N_6$  are mentioned in the Appendix. The difference in temperature between the pot and the water bath depends mainly on the applied difference in air and soil temperature.

The upper unit C is provided with an air outlet  $H_1$ , constructed in the same way as the air inlet  $H_2$ . Opposite to  $H_1$  a perspex tube ( $O_1$ ) with a flange ( $O_2$ ), a perspex stop and an O-ring ( $\varnothing 63 \times 4$  mm) are attached. Through this tube the leaf temperature of a plant can be measured with an infra-red thermometer (P; see Appendix) before or after the  $\text{CO}_2$ -exchange measurements.

$H_1$  and  $H_2$  are connected by perspex flanges ( $p_1$  and  $p_2$ ) with the interunits ( $I_1$  and  $I_2$ ) and flexible tubes ( $n_1$  and  $n_2$ ). The interunit  $I_2$  is provided with perspex tubes  $I_2I_1$  and  $I_2I_2$  (both  $l = 50$  mm),  $I_2I_3$  and  $I_2I_4$ .  $I_2I_1$  is connected by means of a threeway valve onto a  $\text{CO}_2$ -injector and a  $\text{CO}_2$ -cylinder. In this way pure  $\text{CO}_2$  can be injected in the circulating airstream with an accuracy of 5%. The time needed after injection to achieve a steady mixture is about 4 minutes.  $I_2I_2$  is connected to a U-shaped glass tube (not shown) filled with paraffin oil, which indicates the pressure difference between the closed circuit and the ambient air and prevents damage to the equipment in case of excessive under or over pressure.

Through tube  $I_2I_3$  a humidity sensor (Q; see Appendix) can be inserted in the airstream.  $I_2I_4$  is used for wires. Interunit  $I_1$  has similar tubes ( $I_1I_1$ ,  $I_1I_2$ ,  $I_1I_3$ ,  $I_1I_4$ ) as  $I_2$ . Tubes  $I_1I_1$  and  $I_1I_2$  are connected via nyloseal tubes to the in- and outlet of the URAS ( $R_4$ ). The nyloseal tubes are impermeable for  $\text{CO}_2$ . Nyloseal flareless tube fittings were used for the connections. The circuit is pro-

vided with a filter ( $R_1$ ), a membrane pump ( $R_2$ ) and a flowmeter ( $R_3$ ; see Appendix). In tube  $I_1I_3$  a humidity sensor ( $Q$ ) has been inserted.

Transpiration is determined by measuring in- and outgoing air of the plant chamber by the humidity sensors. The temperatures of the air in cylinder  $K$  and in the soil of the pot are measured by copper-constantan thermocouples ( $S_1$ ;  $0.5 \text{ mm}^2$ ). The air and leaf temperature is measured by managanin-constantan thermocouples ( $S_2$ ;  $0.2 \text{ mm}^2$ ) fixed on thin aluminium bars and movable in all directions. The irradiance at various horizontal and vertical positions in the empty plant chamber was measured with a flat photometer for visible light (type TFDL - 65 - 2020) and a Kipp solarimeter (type  $cc_1$ ). The maximum irradiance at plant level is  $215 \text{ W m}^{-2}$ . The difference in horizontal distribution was less than 15% and the vertical measurements showed a quadratic relation. During  $\text{CO}_2$ -exchange measurements the irradiance is recorded continuously by photocells ( $T_1$ ) which are fixed on the thin aluminium bars.

To improve the turbulence in the plant chamber 2 small fans ( $U_1$  and  $U_2$ ) are used. Usually the wind-speed is not recorded during  $\text{CO}_2$ -exchange measurements. The wind-speed in the centre of the interunits is about  $4.80 \text{ m s}^{-1}$ . In the plant chamber without a plant it was  $0.60\text{--}0.95 \text{ m s}^{-1}$  with units  $A$  and  $C$  (in the centre  $0.8 \text{ m s}^{-1}$ ) and  $0.50\text{--}1.10 \text{ m s}^{-1}$  with units  $A$ ,  $C$ ,  $D$  and  $E$ . Wind-speed was measured by a heatball anemometer, constructed at the Department of Physics and Meteorology, Agricultural University. Because of the relatively high wind-speed the difference between leaf and ambient air temperature was small, which is in accordance with results obtained by PAPHENHAGEN (1974).

The URAS, thermocouples, photocells and humidity sensors are connected to a 24 channel mV-recorder (Philips, type PR 3500) or to a datalogger (Fluke, type 2240 A).

#### *Principle of the temperature control system*

A diagram of the temperature control system is given in Fig. 3. The copper-duct  $i$  of the closed circuit (see Fig. 1.) is provided with a fan ( $aa$ ), a cooling coil ( $bb$ ), 2 air-heating elements ( $cc_1$  and  $cc_2$ ) and the temperature sensor ( $o$ ).

Glycol is circulated through the cooling coil. The glycol circuit consists of an expansion vessel ( $dd$ ) with pressure gauge ( $ee$ ), a threeway valve with servomotor ( $ff$ ), a pump ( $gg$ ) for circulating the glycol through the glycol circuit and a valve ( $hh$ ). The threeway valve determines the distribution of glycol through the evaporator ( $ii$ ) and a bypass. In this way the cooling capacity is adapted continuously to the cooling requirement. Temperature is regulated proportionally. The valve  $hh$  is used for filling the circuit with glycol.

The freon circuit consists of a freon compressor ( $kk_1$ ), an air cooled condenser ( $kk_2$ ), a liquid vessel ( $kk_3$ ), a filter drier ( $ll$ ), a sight glass ( $rr$ ), double tubes evaporator ( $ii$ ), thermostatic expansion valves ( $mm_1$  and  $nn_1$ ) with bulb sensors ( $mm_2$  and  $nn_2$ ), a liquid separator ( $oo$ ) and a filter drier ( $pp$ );  $qq$  and  $ss$  are pressure valves.

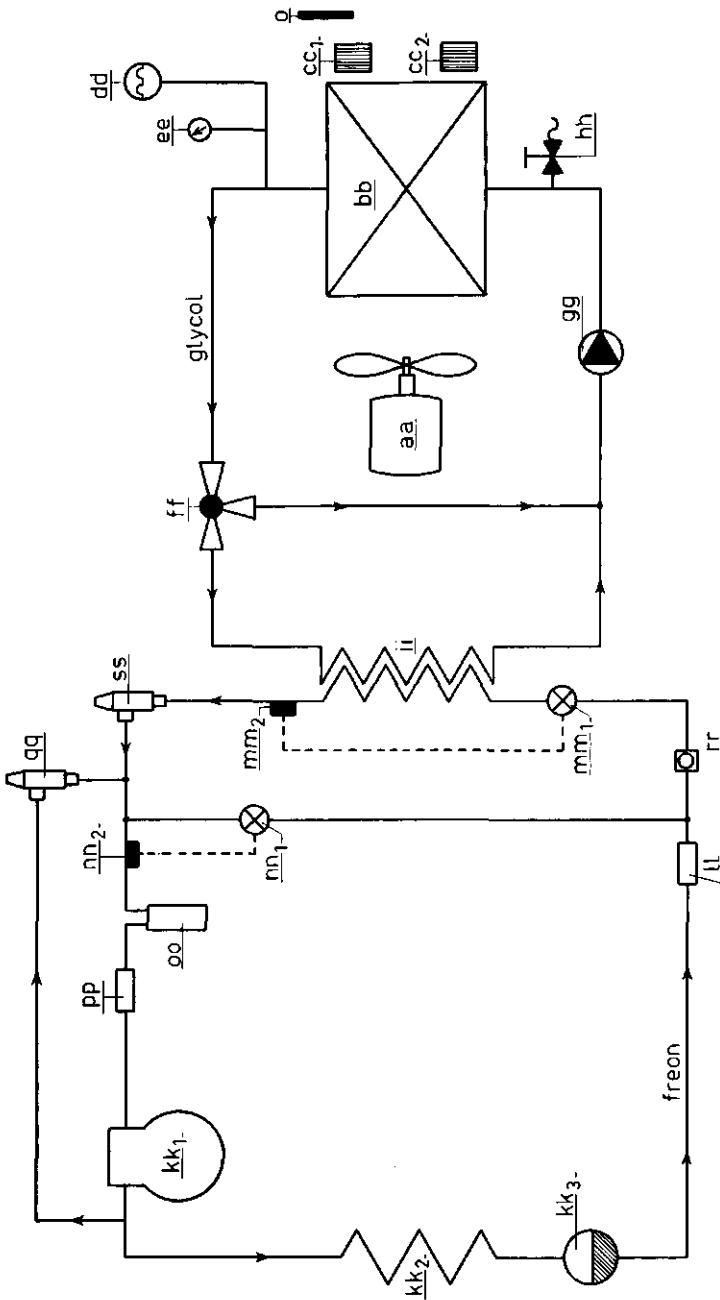


Fig. 3. Diagram of the temperature controlsystem. aa = fan and motor, bb = cooling coil, cc<sub>1</sub> and cc<sub>2</sub> = air-heating elements, dd = expansion vessel, ee = pressure gauge, ff = three-way valve and servo motor, gg = pump, hh = valve, ii = double tubes evaporator (condensor), kk<sub>1</sub> = freon compressor, kk<sub>2</sub> = condenser, kk<sub>3</sub> = cooling vessel, ll = filter drier, mm<sub>1</sub> and nn<sub>1</sub> = thermostatic expansion valves, mm<sub>2</sub> and nn<sub>2</sub> = pressure bulb sensors, oo = temperature sensor, oo = liquid separator, pp = filter drier, qq = pressure valve, rr = sight glass, ss = constant pressure valve.

A high pressure and high temperature exist in compressor  $kk_1$ . In  $kk_2$  the pressure is still high but the temperature becomes lower, due to the cooling by



ventilators with ambient air. A high pressure exists from  $kk_1$  till  $mm_1$  and  $nn_1$ . The pressure difference between the high pressure and low pressure part (ii) is provided by  $mm_1$ . A low pressure and low temperature exist at ii. Freon evaporates in ii and takes heat off from the glycol circuit.

The freon system is continuously operating but below full capacity. Pressure valve  $ss$  regulates the pressure in ii in such way that the temperature in ii never becomes too low. When  $ss$  is closing, an extreme low pressure between  $ss$  and  $kk_1$  can exist, because the capacity of  $kk_1$  remains unchanged. For the protection of the compressor the extreme low pressure is taken off via a gas short-circuit, regulated by  $qq$ . Expansion valve  $nn_1$  is necessary to prevent high temperatures in the short-circuit in a period of prolonged low cooling capacity at ii. Temperature sensor bulb  $nn_2$  regulates  $nn_1$  in such way that the temperature in the shortcircuit never becomes too high and the compressor is protected against burning. The evaporation of freon after  $nn_1$  in the low pressure part cools the short-circuit.

Since the room temperature can be controlled in a range between 10 and 34°C, the temperature in the plant chamber can be chosen between 5 and 32°C. Usually the room temperature was kept a few degrees above the plant chamber temperature in order to prevent condensation on the plant chamber wall. The temperature of the plant chamber could be kept constant with an accuracy of  $\pm 0.5^\circ\text{C}$ . With rapid changes in irradiance manual control of the temperature can be applied in order to achieve more quickly the desired temperature.

In case the equipment fails, a safety fuse will cut the current in order to prevent damage.

#### SOME PRELIMINARY RESULTS ON PHOTOSYNTHESIS AND TRANSPIRATION

During preliminary experiments it appeared that the humidity sensors were accurate and sufficiently sensitive. The difficulty of exactly calibrating the sensors at the high air humidity and of the high wind-speed applied in the plant chamber, which gives a small difference in water vapour between the in- and outgoing air, resulted in a less accurate recording of transpiration than desired. At present data on transpiration can be obtained only under steady conditions (ACOCK et al. 1977; KING et al. 1977) by measuring the amount of water condensed at point  $k$  (see Fig. 1.). Measurement of transpiration by humidity sensors would have been cheap. In the near future we hope to use a URAS for continuous recording of transpiration.

The rates of photosynthesis and respiration are determined in a closed system by measuring the  $\text{CO}_2$ -content of the circulating air by infra-red gas-analysis. The rate of photosynthesis ( $P_n$ ) depends on the decline in  $\text{CO}_2$ -concentration ( $\Delta\text{CO}_2$ ) per unit time ( $\Delta t$ ) and the volume ( $b$ ) of the closed circuit according to  $P_n = b \cdot \Delta\text{CO}_2 / \Delta t \cdot c$ . Symbol  $c$  contains a factor for the calibration of the URAS and the density of  $\text{CO}_2$  at the measured temperature. Analogue to the measurements of HEATH and MEIDNER (1967) with lettuce leaves

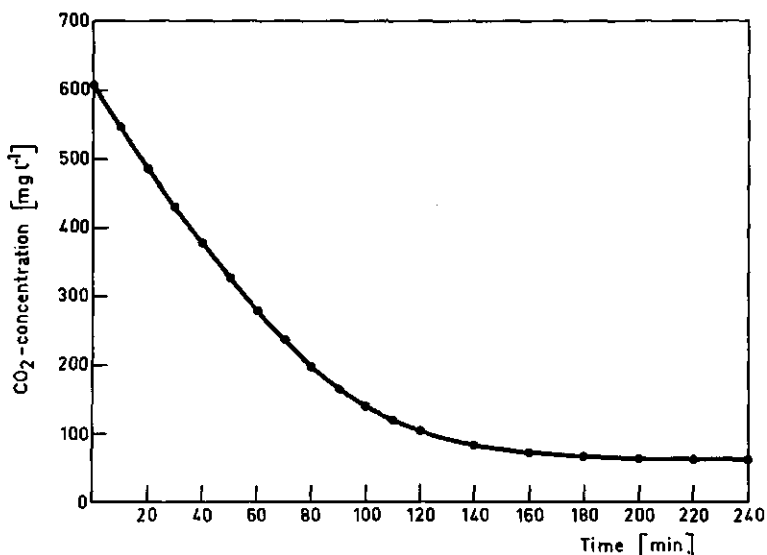


Fig. 4. Decrease of CO<sub>2</sub>-concentration during 4 hours in a closed circuit with a sweet pepper plant cv. Bruinsma Wonder at irradiance of 61 W m<sup>-2</sup> at plant level. The injected CO<sub>2</sub>-conc. was about 620 mg l<sup>-1</sup>. Plant chamber and pot chamber temperature was 25.5°C ± 0.5°C during the measurement. The plant was grown at day-night temperatures of 26–21°C in a glass-house in April-May 1977. The leaf area was 23.3 dm<sup>2</sup> and the plant had 3 small fruits.

or VERFAILLIE (1972) with rice plants, the CO<sub>2</sub>-exchange can be measured at any external CO<sub>2</sub>-concentration. Fig. 4 shows the decrease in CO<sub>2</sub>-concentration against time for a sweet pepper plant cv. Bruinsma Wonder. It is evident from Fig. 4 that below a concentration of 300 mg l<sup>-1</sup> the rate of photosynthesis declines until a steady condition is achieved and the net CO<sub>2</sub>-exchange is zero. The CO<sub>2</sub>-concentration at the compensation point, which was 62 mg l<sup>-1</sup> in this particular case, can be read directly from the chart. Leakage in a short period is neglectable. If there was some leakage of CO<sub>2</sub>, the CO<sub>2</sub>-compensation point would actually be lower than on the chart.

When knowledge regarding photosynthesis at only one CO<sub>2</sub>-concentration is required, a calculated amount of CO<sub>2</sub> can be injected each time to obtain the desired CO<sub>2</sub>-concentration. Fig. 5a shows an example with lettuce cv. Amanda Plus at various light intensities. The figure shows that within a few minutes after injection a gradual decline in CO<sub>2</sub>-concentration set in and ΔCO<sub>2</sub> can be measured. The data of Fig. 5a were used to calculate the CO<sub>2</sub>-exchange rates, which are presented in Fig. 5b, showing the photosynthesis-light response curve.

It should be mentioned that the volume of the plant chamber can be varied depending on the height of the plant. With the smallest volume, plants should have a leaf area of at least 5 dm<sup>2</sup> in order to obtain accurate data.

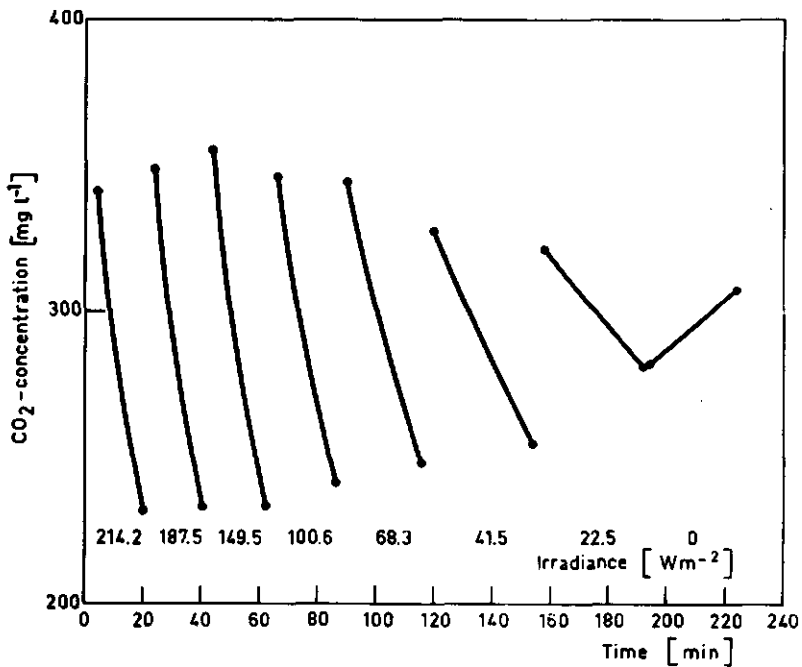


Fig. 5a. Decrease of CO<sub>2</sub>-concentration in a closed circuit with a lettuce plant cv. Amanda Plus during short periods at various irradiance levels. The CO<sub>2</sub>-conc. was between 350 and 250 mg l<sup>-1</sup>. Plant chamber and pot chamber temperature was 14 ± 0.5°C during the measurement. The plant was grown at day-night temperatures of 16–11°C in a glass-house in February-March 1977 with 30 W m<sup>-2</sup> (400–700 nm) artificial illumination and the last two weeks before the measurement 65 W m<sup>-2</sup>. The fresh weight was 52.4 g and the leaf area 18.0 dm<sup>2</sup>.

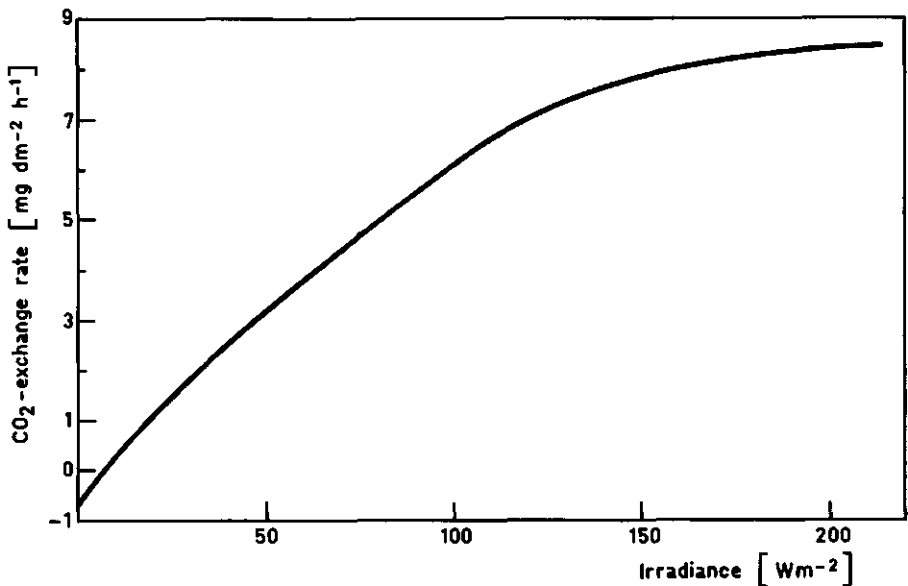


Fig. 5b. CO<sub>2</sub>-exchange rate ( $mg CO_2 dm^{-2} h^{-1}$ ) of a lettuce plant cv. Amanda Plus at various irradiance levels.

## SUMMARY

A closed system for determination of photosynthesis, respiration and CO<sub>2</sub>-compensation points is described. The internal gaseous volume of the closed circuit is 180 litres. It consists of a plant chamber, a copper duct with built-in fan, cooling coil and air-heating elements and connecting flexible tubes. The cylindrical perspex plant chamber has an internal diameter of 441 mm and a height of 340 mm, which can be enlarged to 690 mm. The cylindrical perspex pot chamber has an internal diameter of 190 mm and a height of 190 mm.

Temperature in the plant chamber can be kept constant in the range between 5 and 32°C and in the pot chamber between 15 and 35°C with an accuracy of  $\pm 0.5^\circ\text{C}$ . Temperatures are measured by thermocouples. The maximum irradiance on plant level is  $215 \text{ W m}^{-2}$  (400–700 nm). Irradiance is measured by selenium photocells and air humidity with thin film humidity sensors. Wind-speed in the centre of the plant chamber is about  $0.8 \text{ m s}^{-1}$ . The rate of CO<sub>2</sub>-exchange is determined by an infra-red gas-analyser. Injection of pure CO<sub>2</sub> or a gas mixture facilitates continuous monitoring of photosynthesis and respiration. During short periods leakage can be neglected.

All measurements are recorded on a 24 channel mV-recorder or a data-logger. The equipment has been used in a controlled environment room but can be transferred to the field. Since 1976 this closed system has been used for CO<sub>2</sub>-exchange measurements with lettuce and sweet pepper plants.

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## APPENDIX

- aa Ventilator motor. Küba, type EA-24, with Küba-wings 300KS 15/12 and stepless revolution regulator, type VRH-502.
- b Water bath of aluminium plate ( $h = 110$  mm) with a glass plate ( $d = 10$  mm) on the bottom.
- bb Cooling coil Küba, type  $6 \times 7$  (0.3) B6. Total cooling area is  $10$  m<sup>2</sup>. At a temperature difference of  $10^\circ\text{C}$  the capacity with forced cooling is about  $5040$  kJ h<sup>-1</sup>.
- c Water bath thermostat. Danfoss solenoid valve, type EVJD 15.
- cc<sub>1</sub> and cc<sub>2</sub> Air-heating elements. Küba, type HR300. Power  $315$  W.
- dd Expansion vessel. Flexon, type 2/0.5.
- ee Flexon pressure gauge with a range of  $0.1$ – $0.4$  g m<sup>-2</sup>.
- f<sub>1</sub>–f<sub>4</sub> Old screw jacks, used for cars.
- ff Servomotor. Zentra, type VM-13P and a threeway valve, Zentra type DRK-15.
- F Metal clips. Camloc, type 5 IL 7-IBF.
- gg Pump. SMC, Commander 'S', with a maximal working pressure of  $6 \cdot 10^5$  Pa.
- ii Double tubes evaporator (condensor). Küba, type G3. Capacity at a temperature difference of  $10^\circ\text{C}$  is  $7350$  kJ h<sup>-1</sup>.
- kk<sub>1</sub>–kk<sub>3</sub> Compressor unit L'unité hermétique, type TAH4518/AHR. This fan-cooled condensing unit consists out of the freon compressor kk<sub>1</sub>, condensor kk<sub>2</sub>, and cooling unit kk<sub>3</sub>. Airflow of  $23 \cdot 10^5$  l h<sup>-1</sup>.
- ll Filter drier. Danfoss, type DC-0833.
- mm<sub>1</sub> Thermostatic expansion valve, Danfoss, type TF2-0.5 with pressure sensor mm<sub>2</sub>. Capacity max.  $6300$  kJ h<sup>-1</sup>.
- n<sub>1</sub>–n<sub>2</sub> Flexible tubes Flexofit, type NG2M ( $\varnothing 100$  mm).
- nn<sub>1</sub> Thermostatic expansion valve, Danfoss, type TF2-0.2 with pressure sensor nn<sub>2</sub>. Capacity: max.  $3780$  kJ h<sup>-1</sup>.
- N<sub>5</sub> Portable thermoregulator. Braun, type Thermomix II. Capacity:  $800$  l h<sup>-1</sup>. Temperature range  $0$ – $40^\circ\text{C}$ .
- N<sub>6</sub> Cooling unit. Grant, type CC15. Cooling power of  $295$  kJ h<sup>-1</sup> at  $0^\circ\text{C}$  and of  $590$  kJ h<sup>-1</sup> at  $25^\circ\text{C}$ .
- o Temperature sensor. Zentra, type GF-11 with selector, type FG-2. The temperature in the closed circuit is regulated proportionally by the Zentra thermostat type 2G13/TE3/TK, (ES) with above mentioned sensor and selector by switching the cooling coil bb and air-heating elements cc<sub>1</sub> and cc<sub>2</sub> simultaneously.
- oo Liquid separator (a suction line accumulator), Virginia, type VA32-55.
- pp Lo-side filter drier, Virginia, type AL 24-5SV.
- p Infra-red thermometer, Heimann, type KT with objective A. Temperature range  $0$ – $60^\circ\text{C}$ .
- qq Capacity regulator/receiver pressure valve. Danfoss, type CPC-15.

- Q The Vaisala humidity sensor has been described by SUATOLA and ANTONSON (1973). The electronical circuit is changed by Hoogendoorn B.V. 's-Gravenzande, The Netherlands.
- rr Sight glass. Danfoss, type SGI-10S.
- R<sub>2</sub> Membrane pump. Hartmann und Braun, type 2-Wisa.
- R<sub>3</sub> Flowmeter. Brooks, type E/C, model 1550-V. Capacity: 0–115 l h<sup>-1</sup>.
- R<sub>4</sub> Infra-red gas-analyser, Hartmann und Braun, URAS-2. The URAS has a measuring cuvette of 21 cm with an optical H<sub>2</sub>O-filter in order to reduce interference with the water vapour content of the air sample. Applied flow rate is about 40 l h<sup>-1</sup>. The URAS is weekly calibrated with gas mixtures mixed by 2 mixing pumps (R<sub>5</sub> and R<sub>6</sub>), set in series. Variations in sensitivity of the URAS are always less than 3%.
- R<sub>5</sub> and R<sub>6</sub> Gas mixing pumps. Wöstoff, type SA 27/2a and SA 27/3a.
- s Searle-Bush refrigerators, type SR-240.
- ss Constant pressure valve. Danfoss, type CPP-15.
- T<sub>2</sub>–T<sub>6</sub> Small selenium cells. Megatron, type B (∅ 7 mm).  
The photocells are calibrated with a flat photometer and the Kipp solarimeter, mentioned in the text.
- U<sub>1</sub>–U<sub>2</sub> Fans. Micronell, type V361 M. Maximal capacity 50.10<sup>4</sup> l h<sup>-1</sup>.