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[Environmental consequences of processing manure to produce
mineral fertilizer and bio-energy]

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Environmental consequences of processing manure to produce mineral fertilizer and bio-energy¹

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Abstract

Liquid animal manure and its management contributes to environmental problems such as, global warming, acidification, and eutrophication. To address these environmental issues and their related costs manure processing technologies were developed. The objective here was to assess the environmental consequences of a new manure processing technology that separates manure into a solid and liquid fraction and de-waters the liquid fraction by means of reverse osmosis. This results in a liquid mineral concentrate used as mineral nitrogen and potassium fertilizer and a solid fraction used for bio-energy production or as phosphorus fertilizer. Five environmental impact categories were quantified using life cycle assessment: climate change (CC), terrestrial acidification (TA), marine eutrophication (ME), particulate matter formation (PMF), and fossil fuel depletion (FFD). For pig as well as dairy cattle manure, we compared a scenario with the processing method and a scenario with additional anaerobic digestion of the solid fraction to a reference situation applying only liquid manure. Comparisons were based on a functional unit of 1 ton liquid manure. System boundaries were set from the manure storage under the animal house to the field application of all end products. Scenarios with only manure processing increased the environmental impact for most impact categories compared to the reference: ME did not change, whereas, TA and PMF increased up to 44% as a result of NH₃ and NO_x emissions from processing and storage of solid fraction. Including digestion reduced CC by 117% for pig manure and 104% for dairy cattle manure, mainly because of substituted electricity and avoided N₂O emission from storage of solid fraction. FFD decreased by 59% for pig manure and increased 19% for dairy cattle manure. TA and PMF remained higher compared to the reference. Sensitivity analysis showed that CH₄ emission from manure storage, NH₃ emission during processing, and the replaced nitrogen fertilizer by the mineral concentrate were important parameters affecting final results. It was concluded that processing fattening pig and dairy cattle manure to produce mineral fertilizer increased overall environmental consequences in terms of CC (except for dairy cattle manure), TA, PMF, and FFD compared to current agricultural practice. Adding the production of bio-energy reduced CC and FFD. Only when NH₃ emission from processing was low and bio-energy was produced, overall equal or better environmental performance was

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obtained for TA and PMF. It was emphasized that real time measurements should be done to enhance the environmental assessment of manure processing technologies. Results of this study present the full environmental consequences of manure processing and key parameters affecting the environmental impact of manure management. Outcomes can be used for decision making and further tackling of environmental problems related to manure management.

Keywords: LCA; slurry treatment; fertilizer; anaerobic digestion; greenhouse gases; ammonia

1. Introduction

The environmental impact from animal manure and its management (i.e., storage and application) has increased considerably through growth of livestock production worldwide. In the Netherlands, for example, national production of pig and dairy cattle manure increased from about 46 million tons in 1950 to 68 million tons in 2009 (CBS, 2011). Manure contributes to the following environmental impacts: acidification and particulate matter formation, mainly through volatilization of ammonia (NH_3) and nitrogen oxides (NO_x); climate change through emissions of greenhouse gases (GHG); eutrophication, mainly through leaching of nitrate (NO_3^-) and phosphate (PO_4^{3-}) to soil and surface water; and depletion of fossil energy sources as a result of management (Prapasongsa et al., 2010; Sandars et al., 2003; Thomassen et al., 2008).

These environmental impacts have led to international and national regulations (e.g., Gothenburg Protocol, NEC-Directives, and Nitrates Directive) designed to reduce emissions related to animal manure and management. This has induced surpluses in several regions of the world including the Netherlands, increasing manure removal costs for farmers. To decrease these costs and the environmental impact, manure processing technologies have been developed, including anaerobic digestion (AD), biological treatment, composting, incineration, and gasification (Burton and Turner, 2003). These technologies were mainly developed to reduce GHG emissions, NH_3 volatilization and fossil fuel depletion by producing bio-energy. However, the whole life cycle of these technologies, including the storage and application of end products should be addressed to evaluate their true environmental performance.

The environmental impact of manure processing technologies has been analyzed along the entire life cycle of the manure and its end products by means of life cycle assessment (LCA) in several studies (Hamelin et al., 2011; Lopez-Ridaura et al., 2009; Prapasongsa et al., 2010). GHG emissions were reduced through AD of manure as a result of bio-energy production (electricity and heat) and the substitution of mineral fertilizer. Reductions by up to 147 kg carbon dioxide equivalents (CO_2 -eq.) per ton of pig manure and 104 kg CO_2 -eq per ton of solid fraction of separated pig manure were reached through AD (Hamelin et al., 2011; Prapasongsa et al., 2010). Acidification and eutrophication potentials did not vary, or very little, when digestion was applied. On the other hand these potentials have been shown to be increased

through aeration of the liquid fraction from separated manure combined with composting of the solid fraction (Lopez-Ridaura et al., 2009).

A manure processing technology using liquid and solid separation and reverse osmosis (RO), currently being developed and investigated in the Netherlands, aims at producing a liquid nitrogen (N) and potassium (K) concentrate. The process produces as main products: mineral concentrate (MC), considered to have similar fertilizing properties as mineral N and K fertilizer, and a solid fraction that can be used as a substrate for AD and as a phosphorus (P) fertilizer. Although LCA studies have focused on the environmental impact of some manure processing technologies, the impact of this process has not been investigated.

The objective of this study was to assess the environmental impact of this new manure processing method for fattening pig and dairy cattle manure, and to compare it to conventional manure management practices. We used LCA to determine and compare the environmental impact of manure processing to produce mineral fertilizer, with and without AD, including the application of its end products and compared it to current agricultural practice.

2. Materials and methods

2.1. LCA approach and functional unit

Life cycle assessment is a method to determine the environmental impact of a system providing a product or service. An LCA includes all pollutants and consumptions of finite resources from each stage in the life cycle, and allows a comparative analysis of the environmental impact of different production scenarios of a product (ISO-14040, 2006). In particular, the LCA in this study aimed at assessing the environmental consequences of moving to a manure management system including manure processing relative to a reference without processing. We, therefore included in the analysis the change in environmental impact of all processes (also called marginal processes or suppliers) affected by this change in manure management (Weidema et al., 1999).

For a comparative assessment, the environmental impact is related to a functional unit (FU) that expresses the function of the system in quantitative terms. The function of the system is to process liquid manure into a MC that can be applied as mineral N and K fertilizer and a solid fraction suitable for bio-energy production or as P fertilizer. As the available manure was the starting point, a functional unit (FU) of 1 ton untreated liquid fattening pig or dairy cattle manure was applied. The same chemical composition of manure was applied in the references and the scenarios. This ensured that in all cases equal amounts of nutrients and dry matter were introduced into the system.

2.2. Manure management system and scenarios

2.2.1. System boundaries

The LCA included the environmental impacts from manure storage in the animal house and outside storage; processing of manure; storage, distribution, and field application of the end products; and the transport of materials between different life cycle stages (Fig. 1). To assess distribution and transport distances, we distinguished between four locations for product application: local application on a dairy farm with grassland, local application on an arable or dairy farm with arable land, external (i.e. off farm) application on an arable farm, and application on an arable farm outside the

Netherlands. The system further included environmental impacts related to production of chemicals used for processing (e.g., flocculants), consumed electricity, and substituted electricity in the case of bio-energy production. The system boundaries also encompassed impacts from the production, transport, and application of avoided mineral fertilizer, i.e., N, P and K avoided from mineral fertilizer as a result of using nutrients from manure. The analysis further included environmental emissions and resource use from the production of capital goods except for the manure storage and processing plants.

The system excluded the impacts from animal production, as we assumed that a change in the animal production sector would not be driven by a change in manure management. Additionally, biogenic CO₂ emissions were not incorporated in the calculations as they are considered to be short cyclic carbon taken up by crops (IPCC, 1997). The emission of P was excluded because manure processing was assumed to not affect the total amount of P in manure and end products. Input of P to the soil and crop, therefore, was the same for all references and scenarios.

Marginal products for mineral fertilizer production were assumed to be: ammonium nitrate for N, triple superphosphate for phosphorus pentoxide (P₂O₅), and potassium chloride for potassium oxide (K₂O). Marginal electricity production was based on current Dutch statistics and EU production outlooks from the International Energy Agency. The long term marginal electricity source for the Netherlands was estimated to be a mix of coal (28%), natural gas (67%), and wind (5%) (IEA, 2008, 2011). The utilization of excess heat from AD, i.e. heat produced in addition of the required heat for the process, was not included as heat offset possibilities are still limited in the Netherlands (Dumont, 2010).

2.2.2. Manure processing

Manure processing was done in five full-scale pilot plants operating in the Netherlands (Hoeksma et al., 2011). These pilot plants processed up to 50,000 tons of manure annually and aimed at producing a concentrated N-K liquid and a remaining solid fraction mainly through three processing steps: 1. separation of solids and liquids by means of dissolved air floatation, 2. separating the liquid from the solid remains by a sieve belt press or a screw press, and 3. de-watering of the effluent with reverse osmosis (Fig. 2). The plants produce three end products: MC, solid fraction,

and permeate, i.e., water remaining after reverse osmosis. The MC and solid fraction were applied in crop production as fertilizers. The solid fraction was also used as a substrate for AD to produce bio-energy where after it was applied. Permeate was treated in a water purification plant and discharged to surface water (Fig. 1).

2.2.3. Definition of scenarios

For processing pig and dairy cattle manure, we compared the environmental impact of four scenarios relative to two reference situations. A reference for pig (PRef) as well as dairy cattle manure (CRef) was considered because their manure management systems differ considerably (Table 1). Furthermore, manure from fattening pigs was considered for the pig manure scenarios as this is the most common type of pig manure in the Netherlands.

The scenarios represented central processing plants. Scenario 1 implied processing of fattening pig or cattle manure into MC, solid fraction and permeate (PSc1 and CSc1), whereas scenario 2 also included AD of solid fraction to produce bio-energy (PSc2 and CSc2, Table 1).

Manure was stored for an average period of three months in the animal house in PRef and CRef. Additionally, in PRef, pig manure was stored for one month in a covered outside storage tank, which was excluded in PSc1 and PSc2 because manure processing reduced the need for storage space given that manure is collected from the farms on a monthly basis (De Vries et al., 2011). The end products were stored for a period of three months in a covered circular concrete tank, except for the solid fraction, which was stored in an open shed. They were then applied to the field (Table 1). All emissions and resource use for the processes were included in the assessment.

2.3. Life cycle data inventory and assumptions

2.3.1. Chemical composition of manure and end products

The chemical composition of manure after storage (Table 2) was based on KWIN (2009-2010) and corrected for emissions from the storage system to obtain the composition after excretion following a mass balance approach. Distribution of mass and nutrients to the end products was based on data from the pilot plants (Table 2). Data used for pig manure were also used for cattle manure.

2.3.2. Storage of manure and end products

Emission of nitrogen occurred from manure and product storages as NH_3 , nitrous oxide (N_2O), nitrogen monoxide (NO) and nitrogen gas (N_2) (Table 3). Emissions of NH_3 from processing and storage of end products was estimated as two times the emission from manure storage (total 4% N; 2% of N entering the processing plant and 2% of N during storage). A higher emission was assumed as a result of more contact area with outside air during processing and storage of end products. Emissions of N_2O , NO and N_2 from storage of MC were not included as they were considered to be negligible (Mosquera et al., 2010). Emission of N_2O from storage of solid fraction was based on solid manure storage (Groenestein et al., 2011). Leaching of NO_3^- , P and K during storage was assumed to be negligible because it is obligatory to have sealed concrete floors in manure and product storage systems in the Netherlands. Indirect emissions of N_2O were included as 1% of $\text{NH}_3\text{-N} + \text{NO}_x\text{-N}$ and 0.75% of $\text{NO}_3\text{-N}$ after application (IPCC, 2006a).

Emission of methane (CH_4) occurred during storage of manure and of end products. Methane emission from manure storage prior to processing was modeled specific to the conditions of this study (De Mol and Hilhorst, 2003); the modeled data captured changes in emission related to changes in manure storage retention time between the references (3 months) and the scenarios (1 month) (De Vries et al., 2010). Methane emission from digestate storage was considered to be equal to outside storage of pig manure (Table 3); emissions during the storage of end products were based on Mosquera et al. (2010) and scaled relative to the ratio of emission from raw manure storage, and storage of solid (42 times lower) and liquid fractions (12 times lower).

2.3.3. Manure processing

Separation of liquid manure and de-watering consumes electricity and chemicals for cleaning. Production emissions of these products were included in the assessment and taken from the ecoinvent database (EcoinventCentre, 2007). Electricity demand for processing was 9.0 kWh ton^{-1} manure entering the processing unit (Table 3). About 0.39 liters of flocculating additives (polyacrylamide) per ton of manure were used for

separating solid particles from the liquid fraction. In addition, 0.022 liters of sodium hydroxide (NaOH) and 0.081 liters of sulfuric acid (H₂SO₄) per ton of manure was used for cleaning the installations (Hoeksma et al., 2011).

2.3.4. Anaerobic digestion

AD of the solid fraction was applied in PSc2 and CSc2. Digestion took place in a digester with a retention time of 60 days. The produced biogas was used in a combined heat and power plant (CHP) with an electric capacity of 250 kWh (Zwart et al., 2006). The energetic and electric efficiencies of the CHP were respectively 80 and 35% (Van der Leeden et al., 2003).

Emissions of CH₄, N₂O and NO_x and consumption of energy occurred during digestion and the combustion of the biogas. Methane losses were 1.5% of produced CH₄ (1% from the installation and 0.5% from the gas engine) (IPCC, 2006a). Emissions of N₂O were 0.1 kg N₂O TJ⁻¹ of produced electricity and emissions of NO_x were 0.42 g NO_x m⁻³ of produced biogas (IPCC, 1997; VROM, 2010). Digestion required 66 MJ of electricity per ton substrate and 166 MJ heat per ton substrate (Berglund and Börjesson, 2006). Electricity was taken from the grid whereas heat originated from the CHP.

During AD the composition of solid fraction changed, as part of the organic nitrogen was converted into mineral nitrogen. To factor this in, we considered a 20% increase of N_{min} during AD (Ovinge, 2008; Schröder et al., 2008).

2.3.5. Distribution of products and transport distances

Distribution of manure (flows a, b, and c in Fig. 1) in the reference situations (PRef; CRef) was calculated based on Dutch national statistics, an average defined arable and dairy farm, and legal application standards of N and P₂O₅. Of the arable farms, 57% was on clay and 43% on sandy soil. For dairy farms these proportions were respectively 27% and 59% and additionally 14% was on peat soil. On the average arable farm, the total annual N, P₂O₅, and K₂O demand was: 179 kg N ha⁻¹, 85 kg P₂O₅ ha⁻¹, and 171 kg K₂O ha⁻¹ (De Vries et al., 2011). On the dairy farm, total annual N, P₂O₅, and K₂O demand was: 274 kg N ha⁻¹, 97 kg P₂O₅ ha⁻¹, and 360 kg K₂O ha⁻¹. The legal application standards for animal manure applied on the arable

farm were 170 kg N ha⁻¹ and 85 kg P₂O₅ ha⁻¹ and on the dairy farm 250 kg N ha⁻¹ and 100 kg P₂O₅ ha⁻¹ (combined grassland and arable land) (MEAAI, 2010). Application amounts of K₂O from animal manure were dependent on application limits of N and P₂O₅.

As a consequence of these limits, an average of 39% of fattening pig manure on province level was transported and applied to another province in the Netherlands (external application) (CBS, 2011; De Vries et al., 2011). Additionally, 2.7% of the surplus pig manure was exported outside the Netherlands and assumed to be applied in Northern France or Germany (Luesink, 2009 Personal communication). Exported manure was disinfected by heating it to 70 degrees C and consumed approximately 24 kWh electricity per ton of manure (Melse et al., 2004). Emissions of nitrogen during disinfection were not considered as they were expected to contribute very little to the end result.

On average 13.8% of the dairy cattle manure on farm level was transported and applied to an external arable farm (De Vries et al., 2011). No export of cattle manure outside the Netherlands was assumed as this occurs rarely. Manure applied on farm was distributed relatively to the ratio of nitrogen applied to grassland (86%) and arable land (14%).

In the scenarios it was assumed that the MC was authorized to be used over and above the application standards of nitrogen from animal manure, but not over the total nitrogen application standards, to represent its possibility of being used as mineral fertilizer. All MC, therefore, was applied in the local area. In the pig manure scenarios 56% was applied on grassland and 44% on arable land (De Hoop et al., 2011). Mineral concentrate was applied first in the local area where after solid fraction or digestate was applied until one of the application standards was reached. The remainder was transported off farm and if necessary outside of the Netherlands

Transport distances were based on data from the manure processing plants (DR, 2010 Unpublished data) and expert judgment (Table 4). Emission data and resource use for all transportation were taken from the ecoinvent database (EcoinventCentre, 2007). Distances for application outside the Netherlands were estimated distances to Northern France and Germany. Transport distance of chemicals used for processing was 150 km.

2.3.6. Manure product application and avoided fertilizer

Manure, MC, and digestate were applied with a manure injector on grassland and arable land. Solid fraction was applied by means of a solid manure spreader and incorporated into the soil directly after application (arable land). Mineral fertilizer was applied with a broadcast spreader. The environmental impact from production and combustion of diesel and capital goods for spreading of the products were taken from the ecoinvent database (EcoinventCentre, 2007). All application areas were assumed to have similar management.

During and after application of manure and end products emissions of NH_3 , N_2O , NO and leaching of NO_3^- occurred (Table 3). Ammonia emission factors for the application of MC were adjusted relatively to emission factors for the application of manure. Absolute NH_3 emissions for MC were recorded to be similar to manure (Huijsmans and Hol, 2010). Taking the higher mineral nitrogen content of MC into account, the emission factors of MC were calculated as 0.32 times the emission factor of manure (i.e., the ratio between the emission factor of liquid manure and MC).

Nitrous oxide emission factors for application of MC were adjusted in a similar way. Based on Velthof and Hummelink (2011), N_2O emission factors from MC were 1.5 times the emission factor of manure. All nitrous oxide emission factors applied to grassland were weighted by soil type (i.e. the implementation of farms on different soils in section 2.3.5).

The nitrogen fertilizer replacement values (NFRVs, also called mineral fertilizer equivalent values) were used to calculate the avoided N fertilizer from using manure products (Table 3). For cattle manure applied on farms, NFRV was 45%, as a consequence of grazing, and 60% in the case of off farm application (DR, 2009). These ratios were applied to adjust replacement values for MC and solid fraction. Replacement values for pig and dairy cattle manure applied on arable farms were weighted by soil type. Fertilizer replacement values for P_2O_5 and K_2O were considered as 100%. Furthermore, the NFRV for undigested solid fraction was also used for digested solid fraction, since a recent study has indicated that the NFRV of digested manure increased in the first year after application but declined more rapidly afterwards and did not differ in the long term (Schröder et al., 2007).

In CSc1 and CSc2 over-application of K_2O on farm occurred (0.57 kg total), so was assumed not to substitute mineral fertilizer.

Nitrate leaching was computed as a percentage of the total N applied from each product. The leaching fractions for the products were based on N-balance calculations, i.e., after subtracting gaseous emission and N-uptake by crops (Dekker et al., 2009). Leaching after application of the MC was considered equal to leaching from liquid fraction after separation of liquid manure. The leaching from digestate was considered equal to leaching from undigested solid fraction.

2.4. Impact assessment

In the life cycle impact assessment, the emissions and resource use from the references and scenarios are accounted for and categorized into the environmental impact categories to which they contribute (Heijungs et al., 1992). Five impact categories were selected based on their relevance for manure management: climate change (CC expressed in kg CO₂-equivalants (eq.), including emission of CO₂, CH₄, and N₂O), terrestrial acidification (TA expressed in kg SO₂-eq., including emission of NH₃, NO_x, and SO₂), marine eutrophication (ME expressed in kg N-eq., including emission of NH₃, NO_x, and leaching of NO₃⁻), particulate matter formation (PMF expressed in kg PM₁₀-eq., including emission of particulates < 10 μm and NH₃, NO_x, and SO₂ as precursors of particulate matter), and fossil fuel depletion (FFD expressed in kg oil-eq., with 42 MJ kg oil-eq⁻¹). The scenarios and impact assessments were modeled and computed in SimaPro v.7.2 (PRé Consultants, the Netherlands) and by using the ReCiPe midpoint v.1.04 impact assessment method (Goedkoop et al., 2009).

2.5. Sensitivity analysis

A sensitivity analysis was conducted to assess the influence of changes in important parameters and underlying assumptions on the comparison between the scenarios and references and therewith the solidity of the end results. In the analyses, the effect of changing four parameters was tested: CH₄ emission from manure storage, NH₃ emission from manure processing, NFRV of MC, and excess heat utilization from AD.

3. Results

3.1. Environmental consequences of processing manure to produce mineral fertilizer

The processing of pig manure and application of end products as fertilizer (PSc1) showed an increase in all environmental impact categories except for ME compared to the reference system. Climate change, FFD, TA, and PMF increased by respectively 9%, 33%, 19%, and 23% (Fig. 3). The increase in CC was caused mainly by emission of GHGs from storage of end products (Table 5). Although CH₄ emission from manure storage decreased, storage of solid fraction resulted in higher N₂O emissions from more denitrification compared to anaerobic storage of liquid manure (Table 3). Fossil fuel depletion increased as a result of energy demand for manure processing despite the energy demand for transportation having been approximately halved and avoided fossil fuel of mineral fertilizer produced. Less energy for transport was needed for two reasons. First, less weight had to be transported because water is removed during the process. Second, less long distance transport was required due to application of MC in the local area. TA and PMF increased due to NH₃ emission from manure processing together with NH₃ and NO_x emission from product storage. Storage of solid fraction resulted in higher NO_x emission. However, TA and PMF were governed by NH₃ emission from manure storage prior to processing, which was equal in all cases.

Processing dairy cattle manure and applying the end products (CSc1) showed a decrease in CC of 67% and an increase in FFD of 110%, in TA of 31%, and in PMF of 44% compared to the reference situation (Fig. 4). ME did not change. The decrease in CC was caused by less CH₄ emission from manure storage due to a shorter storage time, which was not offset by increased N₂O emission from storage of solid fraction. Fossil fuel depletion increased as a result of energy demand for manure processing and transportation of manure and end products. Energy for transportation increased, because products had to be transported to and from the processing location whereas in the reference situation only surplus cattle manure was transported locally. TA and PMF in CSc1 increased for the same reasons as in PSc1.

3.2. Environmental consequences of processing manure to produce bio-energy

The second scenario for pig and dairy cattle manure (PSc2 and CSc2) included the AD of solid fraction for bio-energy production. In PSc2, although TA and PMF increased due to higher NH₃ emissions from manure processing and product storage, other measures mainly decreased. CC reduced 117% and FFD 59% compared to the reference situation (Fig. 3). TA and PMF were lower compared to PSc1, as storage of solid fraction was avoided, but was higher (12%) than in the reference situation. Again, ME did not change. Climate change and FFD reduced mainly due to substitution of fossil electricity (85 MJ) as a result of bio-energy production. Furthermore, CC reduced as a result of less CH₄ emission from manure storage and less N₂O emission from storage of solid fraction as it was assumed to be digested shortly after production (Table 5). Fossil fuel depletion reduced not only because of substituted fossil electricity, but also because of less energy for transport compared to PRef. The produced energy more than counteracted the required energy for processing.

Processing of dairy cattle manure and AD of solid fraction (CSc2) reduced CC by 104%, but increased FFD by 19%, TA by 9%, and PMF by 12% compared to the reference situation. As in CSc1, ME did not change. Climate change decreased as a result of less CH₄ emission from manure storage, less N₂O emission from storage of solid fraction, and because of the substitution of fossil based electricity (56 MJ). FFD increased as a result of low energy production and energy demand for processing and transportation (Table 6). TA and PMF increased for the same reason as in CSc1.

3.3. Sensitivity analysis

3.3.1. Methane emission from manure storage

In this study we modeled CH₄ emissions from manure storage specifically for the described circumstances. We assumed that storage time of manure was reduced to 1 month only in case of manure processing although in practical circumstances, even with manure processing, manure storage time might be longer. We therefore tested this assumption by exploring the effect of a 3 month storage time in the scenarios. Results showed an increase in CC for all scenarios (Table 7). In PSc1 and PSc2, CC was about 26 kg CO₂-eq higher than their baseline situations, whereas in CS1 and

CSc2, this increase was about 78 kg CO₂-eq. For CSc1 and CSc2, this meant a change in the comparison between the scenarios and reference indicating the importance of shortening the storage time of manure to reduce CC. Furthermore, it shows the necessity of accurately estimating CH₄ emission from manure storages in LCAs.

3.3.2. Ammonia emission from manure processing

In this study, we applied an estimated NH₃ emission factor of 4% of N including both emission during storage of the end products (2%) and emissions during manure processing (2%) (Table 3). Data on NH₃ emissions during processing are scarcely available, and therefore over or under estimation may occur. Since we considered testing a higher emission irrelevant, (as this would increase TA and PMF and to lesser extent ME and CC), a lower emission rate during processing (0.3% of N in manure entering the processing plant) was tested (Melse and Verdoes, 2005). Results showed a decrease in TA and PMF of approximately 10% in CSc1, 13% in CSc2 and a decrease of 7% in both PSc1 and PSc2 (Table 7). The total impact for TA and PMF in PSc2 was approximately equal to the reference. The impact for CSc2 was even lower than its reference. This indicates that for improving the environmental performance of manure processing, controlling NH₃ emission during processing is essential.

3.3.3. NFRV of mineral concentrate

The NFRV of MC has been reported to vary considerably depending on factors such as, soil type, method of application and weather conditions (Velthof, 2009). To assess the influence of a change in the NFRV on the impact assessment, this parameter was varied plus and minus 20%. Results showed that mainly ME, CC and FFD decreased with a 20% increase of the NFRV and increased with a 20% decrease of the NFRV (approximate variation for ME was 14%, CC 29 – 265%, and FFD 10 – 147%).

3.3.4. Excess heat utilization from anaerobic digestion

The effect of including heat use of AD on the impact assessment was explored to represent existing initiatives of heat utilization. The substituted marginal source for heat in the Netherlands was assumed to be a mix of heat based on natural gas (79%) and heat based on light fuel oil (21%) (CBS, 2009; Menkveld and Beurskens, 2009).

Heat from natural gas was divided into heat from boilers smaller than 100 kW with low NO_x emission technology (55%) and heat from industrial furnaces with low NO_x emission technology (24%) as these sources are the most common in the Netherlands (EcoinventCentre, 2007; Menkveld and Beurskens, 2009). Results showed a reduction in CC and FFD (respectively 118% – 160% and 26% – 50%) in the scenarios with AD (Table 7), thereby in CSc2, FFD was lower compared to the reference situation. This indicates that utilization of excess heat from AD strongly improves the environmental performance of manure management concerning CC and FFD.

4. Discussion

Overall, processing pig and dairy cattle manure to produce mineral fertilizer increased the environmental impact. In environmental terms, processing without AD does not represent an attractive alternative to current agricultural practice, as it increases FFD, CC, TA, and PMF. In the pig manure scenarios, the additional energy required for processing outweighed the reduction in energy required for transportation. This has also been observed in other studies (Lopez-Ridaura et al., 2009). In the cattle manure scenarios, even additional energy for transportation was needed. This indicates that other drivers e.g., economic viability or social acceptance, are more likely to propel initiatives for manure processing instead of the related environmental impact as considered in this study.

The importance of controlling nitrogen emissions from manure processing and product storage (NH₃, NO_x, and N₂O) is stressed by the modeled increases in CC, TA, and PMF, as environmental impact is affected both directly and indirectly due to less substituted mineral fertilizer. The importance of nutrient recovery for mineral fertilizer substitution has been indicated in other studies as well (Prapasongsa et al., 2010). Furthermore, as Dinuccio et al. (2008) have mentioned, storing separated fractions from mechanical separation of manure has the potential to increase CC. Emission data from storage of separated fractions are still rare. These emissions are difficult to quantify as they depend on specific circumstances such as, storage type, storage time and climatologic conditions. Our initial estimates, therefore, were based on a combination of comparative lab results and best available data. Our model results show that it is important to further quantify these emissions under different conditions and include them in environmental assessments of manure management techniques.

Processing pig manure and digestion of the solid fraction for bio-energy production presented a better alternative, as it added a strong environmental advantage by reducing CC and FFD. This is in agreement with other studies which showed a similar reduction in CC of approximately 40 kg CO₂-eq, including manure storage with a natural crust cover (Hamelin et al., 2011; Prapasongsa et al., 2010). It also indicates that it is preferable to avoid producing end products with potentially high denitrification rates during storage as this results in increased CC. Furthermore, AD of the solid fraction from pig and cattle manure reduced TA and PMF compared to the scenarios without AD, as storage of solid fraction was avoided. However, TA and PMF remained higher compared to the references. This may be partly due to the assumption that NH₃ emission factors, as a percentage of N_{min}, during application of digestate were assumed equal to undigested manure. The higher N_{min} in the digestate, therefore, increased total NH₃ emission. However, absolute emissions during application have been reported to be equal compared to undigested manure due to higher infiltration rates of digestate into the soil (Amon et al., 2006). In that case, including AD would lead to more reduction of TA and PMF improving its environmental potential compared to current practice.

Surprisingly, processing dairy cattle manure for bio-energy production did not lower FFD more than the reference. This indicates that processing of cattle manure in this fashion provides only little environmental benefit, reducing only CC. Moreover, the method presented in this research is costly with processing costs approximately 9 – 13 euro per ton of manure (De Hoop et al., 2011). Because cattle manure management differs strongly from pig manure management, simpler technologies requiring less energy may provide a better solution for handling cattle manure surpluses (Evers et al., 2010). Studies on the environmental consequences of such methods have not been conducted.

Compared to the references, in the scenarios ME did not change (maximum variation of 3%). The main reason was that emissions of NO₃⁻, NO_x, and NH₃ counteracted each other in the different scenarios although they contribute in different degrees to ME, i.e., when emission of NO₃⁻ was lower, emissions of NH₃ and NO_x were higher and vice versa. This indicates that trade-off between different substances within an impact category may occur and require attention.

Important parameters affecting final results, as sensitivity analysis showed, include CH₄ emission from manure storage, NH₃ emission during processing, and the

NFRV of the MC. Methane emission from manure storage has been reported elsewhere as an important parameter affecting the greenhouse gas balance and therewith CC from manure management systems (IPCC, 2006a; Lopez-Ridaura et al., 2009). Data on CH₄ emission from manure storages should, therefore, be carefully considered, and it is advised to use models, as in this study, based on a higher Tier method in the IPCC guidelines to obtain specific data related to the circumstances of the conducted study. NH₃ emission directly affects TA and PMF and to a lesser extent ME and CC and should therefore be kept to a minimum. This could be achieved by for example reducing contact with outside air, to ensure lower NH₃ emission and overall equal or better performance compared to current practice. Furthermore, it shows the necessity of obtaining more detailed data on NH₃ emissions, as well as other N-substances, such as N₂O, NO and N₂, occurring during processing to enhance LCA studies of manure management as very often emissions from processing may be underestimated. The NFRV of MC mainly affected ME, CC and FFD. It will depend on circumstances, such as soil type, weather conditions, cropping system, and time of application of the manure product. NFRVs used in calculating mineral fertilizer substitution rates should, therefore, be tailored to the specific conditions applicable over the long term. As Schröder et al. (2005) states, a correct assessment of the NFRV for each manure product is important in reducing the environmental impact of manure management in terms of NO₃⁻ leaching.

Marginal production of electricity was not addressed in the sensitivity analysis as recent studies have shown that a change in marginal electricity will not affect the outcome of the study (De Vries et al., 2011; Hamelin et al., 2011).

This study included CH₄, N₂O and NH₃ emissions from in house storage of manure as these emissions contribute strongly to CC, TA, and PMF. It also indicates that future work should consider the loss of N from manure storage prior to processing to determine a proper mineral fertilizer substitution rate. Additionally, although studies on reducing emissions from animal houses have been done e.g., (Aarnink et al., 1996; Canh et al., 1998; Monteny et al., 2006), new developments are needed, such as separating feces and urine under the slats (Aarnink and Ogink, 2007), and should be assessed to indicate improvements of the environmental performance of manure management.

As N and P application standards in the Netherlands will be lowered in the coming years to comply with the EU Nitrates Directive (MEAAI, 2010), local manure

surpluses will likely increase, inducing more transportation of manure and its derived products. This, however, should not affect the conclusions of this study, as changing distribution and transport distances has only a limited effect on the environmental impact of manure management. Moreover, mineral fertilizer replacement rates may also change due to lowering of the application standards. The reference system, however, will also change in conjunction with those standards and, therefore, conclusions of this study will not change (i.e., the comparison between scenarios and references will stay the same). On the other hand, availability of other fertilization products could change fertilization strategies on farms and therewith the environmental impact. This should be studied in more detail as it was out of scope in this study.

Finally, future processing scenarios are also expected to include the processing of digestate from AD. Currently, however, this approach has practical difficulties as digestates vary in composition as a result of varying input materials and because processing conditions change from plant to plant (Hoeksma et al., 2011). It is expected that AD of liquid manure will increase energy production as compared to AD of the solid fraction and therewith further reduce CC (De Vries et al., 2011).

5. Conclusion

Processing of fattening pig and dairy cattle manure by using liquid and solid separation and reverse osmosis (RO) to produce mineral fertilizer increased overall environmental impact in terms of climate change (CC) (except for dairy cattle manure), terrestrial acidification (TA), particulate matter formation (PMF), and fossil fuel depletion (FFD) compared to current agricultural practice. Marine eutrophication (ME) did not change. Adding the production of bio-energy enhanced the environmental performance by substituting fossil electricity and reducing storage emissions from solid fraction. Utilization of excess heat increased this trend for CC and FFD. However, the addition of AD did not present a better option compared to current practice considering TA and PMF, and FFD for cattle manure, unless when NH_3 emissions from processing were kept low. In that case, equal or better environmental performance was obtained for TA and PMF.

Key parameters affecting the environmental performance were identified as NH₃ emission from manure processing and product storage together with N₂O and NO_x emissions from product storage as a result of denitrification; controlling these was essential to reduce the environmental impact of manure processing and to improve the potential for substituting mineral fertilizer. Additionally, CH₄ emission from manure storage should be modeled as precisely as possible to the circumstances being studied, to correctly assess its environmental consequences. Overall, this emphasizes a continuous need of real time measurements of these emissions to ‘feed’ future LCA studies.

Results of this study show the environmental consequences and key parameters affecting the environmental impact of manure management as it considers the full life cycle of the processing and application of all end products. It also shows that innovations that appear worthwhile for reducing environmental impact do not always deliver the expected results when considering all consequences within the system. Furthermore, it highlights the importance of particular emissions during both processing and storage. For those tackling environmental problems around manure management, this assessment has provided a number of key outcomes to inform their decision making.

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Figures

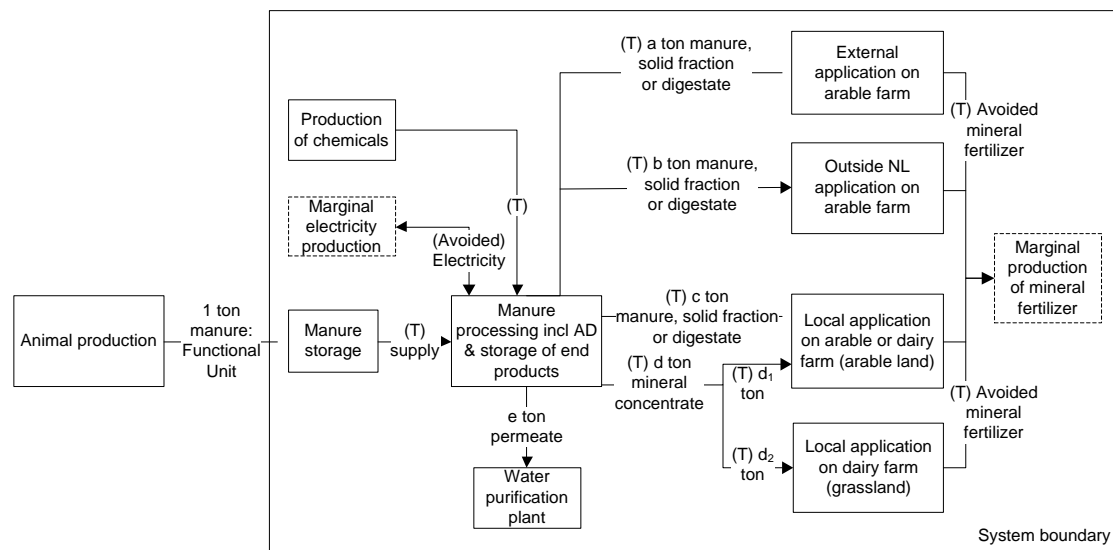


Fig. 1. Manure management system with input of 1 ton pig or dairy cattle manure and distribution of end products as considered in the assessment. Black arrows represent mass flows of materials. The two-way arrow for electricity production and consumption points out that electricity is consumed as well as produced. (T) represents transportation.

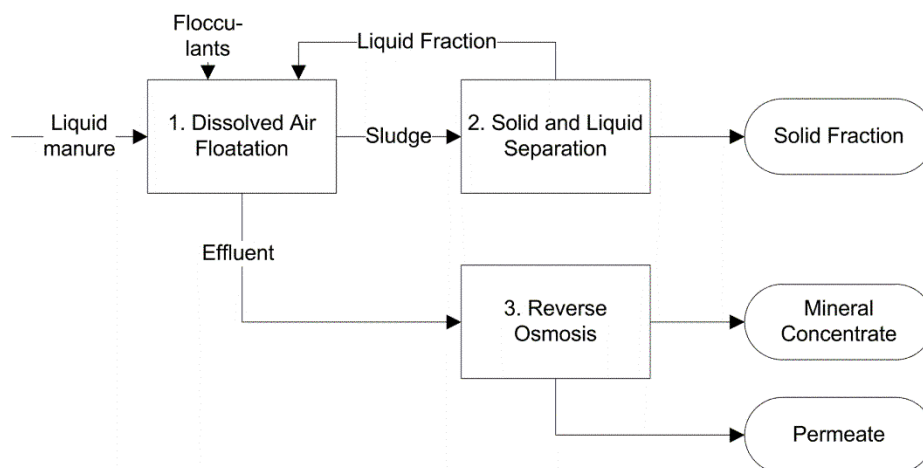


Fig. 2. Schematic overview of the manure processing technology and its intermediate and end products (after Hoeksma et al. (2011)).

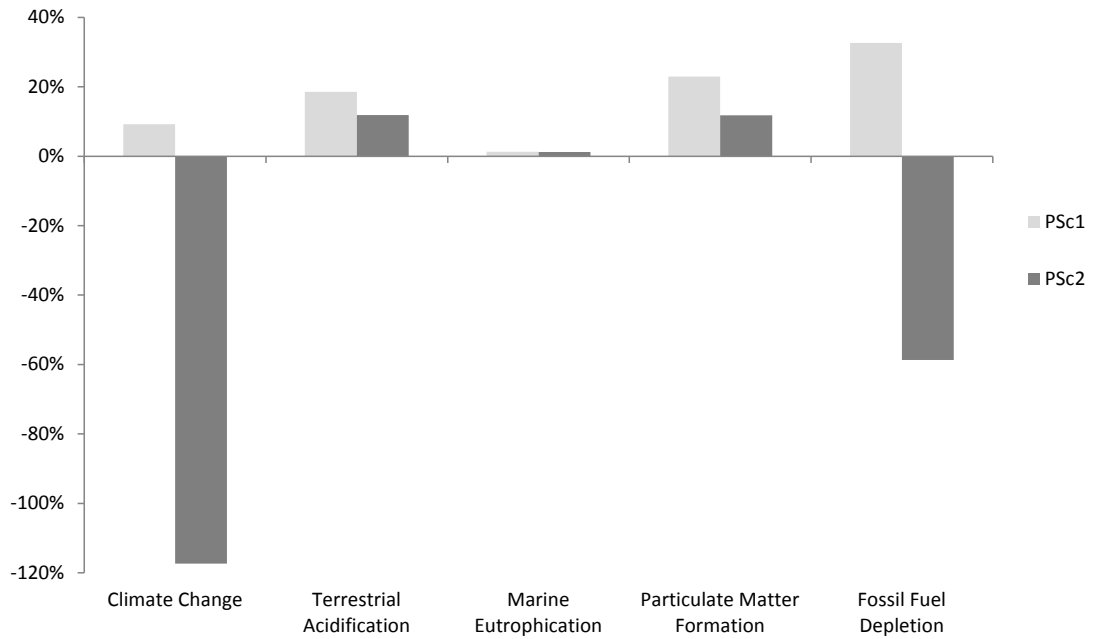


Fig. 3. Relative change in the environmental impact of the fattening pig manure scenarios (PSc1 & PSc2) compared to the reference (PRef = 0%).

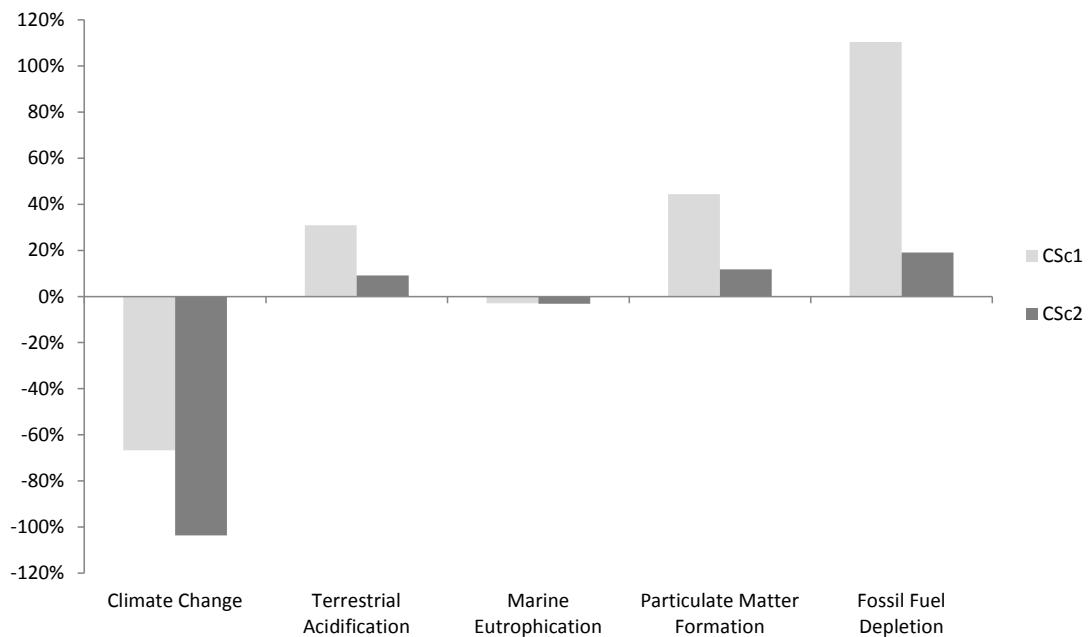


Fig. 4. Relative change in the environmental impact of the dairy cattle manure scenarios (CSc1 & CSc2) compared to the reference (CRef = 0%).

Table 1. Considered processes in the references and manure processing scenarios for pig and dairy cattle manure

Scenario	Storage in house	Outside storage	Manure processing	Anaerobic digestion	Product storage	Field application
Pig						
PRef	X	X	-	-	-	X
PSc1	X	-	X	-	X	X
PSc2	X	-	X	X	X	X
Cattle						
CRef	X	-	-	-	-	X
CSc1	X	-	X	-	X	X
CSc2	X	-	X	X	X	X

PRef = pig manure reference, PSc1 = pig manure scenario 1, PSc2 = pig manure scenario 2, CRef = dairy cattle manure reference, CSc1 = dairy cattle manure scenario 1, CSc2 = dairy cattle manure scenario 2. ‘X’ indicates included processes whereas ‘-’ indicates excluded processes.

Table 2. Calculated distribution of mass and nutrients for processing and chemical composition of manure and end products after storage

Product	Distribution of mass and nutrients ^b			Chemical composition						
	Mass (%)	OM (%)	N, N _{min} , P, K (%)	DM (kg ton ⁻¹)	OM (kg ton ⁻¹)	N _{tot} (kg ton ⁻¹)	N _{min} (kg ton ⁻¹)	P ₂ O ₅ (kg ton ⁻¹)	K ₂ O (kg ton ⁻¹)	Density (kg m ⁻³)
PM after storage^a	-	-	-	90.0	60.0	7.60	4.60	4.2	7.2	1040
PM after in house storage	-	-	-	90.4	60.4	7.63	4.63	4.2	7.2	1040
PM after excretion	-	-	-	93.7	63.7	9.34	6.01	4.2	7.2	1040
Mineral concentrate	39	12	53, 70, 5, 79	27.1	18.1	9.90	7.77	0.5	14.7	1031
Solid fraction	19	88	45, 28, 95, 19	416	278	14.9	3.68	20.8	7.2	n.d.
Permeate	42	0	2, 3, 0, 1	0.17	0.11	0.32	0.27	0.0	0.2	1001
Digested solid fraction	-	-	-	351	213 ^c	17.1	7.25	20.8	7.2	n.d.
CM after storage^a	-	-	-	86.0	64.0	4.40	2.20	1.6	6.2	1005
CM after excretion	-	-	-	92.3	70.3	4.66	2.22	1.6	6.2	1005
Mineral concentrate	Equal to pig manure			25.8	19.2	5.71	3.65	0.2	12.6	1031
Solid fraction				395	294	8.58	3.03	7.9	6.2	n.d.
Permeate				0.16	0.12	0.18	0.07	0.0	0.2	1001
Digested solid fraction				-	-	-	352	251	9.89	3.36

^a- = not applicable, n.d. = not determined. OM = organic matter, DM = dry matter, N_{tot} = total nitrogen, N_{min} = mineral nitrogen (NH₄⁺-N), PM = pig manure, and CM = cattle manure.

^a (KWIN, 2009-2010).

^b (De Vries et al., 2011; Hoeksma et al., 2011).

^c Calculated based on 50% C in the organic matter, 37.5 m³ CH₄ ton⁻¹ solid fraction and a CH₄ content of 60% in the biogas. Includes storage losses after digestion (0.17 kg CH₄ ton⁻¹).

Table 3. Emission factors and energy use during storage, processing, and field application of manure and end products and methane yields of anaerobically digested solid fractions

	Unit	Storage in house		Outside storage	Processing/AD		Product storage			Field application								
		PM	CM	PM	PM	CM	MC	Dig	SF	PM, CM, Dig		AN		MC		SF		
										Gr	Ar	Gr	Ar	Gr	Ar	Gr	Ar	
NH ₃ -N	% TAN	27 ^a	10 ^a	2% N ^a	4% N						19 ⁱ	2 ⁱ	2.5 ⁱ		6.0 ⁱ	0.64 ⁱ	40 ⁱ	22 ⁱ
N ₂ O-N	% N	0.1 ^a			-	-	0.1 ^b	2 ^a	0.4 ^j	1.3 ^j	1.3 ^j	1 ^j	0.6 ^j	1.95 ^j	0.4 ^j	1.3 ^j		
N ₂ -N	% N	1 ^a			-	-	1 ^c	10 ^c	-	-	-	-	-	-	-	-	-	-
NO-N	% N	0.1 ^a			-	-	0.1 ^c	2 ^c	0.55 ^k									
NO ₃ -N	% N	-	-	-	-	-	-	-	20.3 ^l		15.8 ^l		18.1 ^l		22.6 ^l			
NFRV ^a	%	-	-	-	-	-	-	-	62;45 ^m		100 ^m		60 ^m	60;80 ^m	31 ^m	31;41 ^m		
CH _{4 long} ^a	kg ton ⁻¹	1.33 ^d	3.32 ^d	0.17 ^d	-	0.014 ^e	0.17 ^d	0.004 ^e	-	-	-	-	-	-	-	-	-	
CH _{4 short} ^a	kg ton ⁻¹	0.29 ^d	0.21 ^d		-				-	-	-	-	-	-	-	-	-	-
CH _{4 yield}	m ³ ton ⁻¹	-	-	-	37.5 ^f	25 ^f	-	-	-	-	-	-	-	-	-	-	-	
Energy	kWh ton ⁻¹	1.7 ^g		0.5 ^g	9.0 ^h		0.5 ^g		-	Ecoinvent database ⁿ								

‘-‘ = not included. AD = anaerobic digestion, PM = pig manure, CM = cattle manure, MC = mineral concentrate, Dig = digestate, SF = solid fraction, AN = ammonium nitrate, Gr = grassland, Ar = arable land, TAN = total ammoniacal nitrogen (NH₄⁺ and NH₃), NFRV = nitrogen fertilizer replacement value, CH_{4 long} = methane emission factor for long term (3 months) storage, and CH_{4 short} = methane emission factor for short term (1 month) storage.

^a (Groenestein et al., 2011).

^b (IPCC, 2006b).

^c N₂-N and NO-N emission factors calculated as ratio of N₂O-N (Oenema et al., 2000).

^d (De Mol and Hilhorst, 2003).

^e (Mosquera et al., 2010).

^f Solid fraction from fattening pig manure (Timmerman et al., 2009). Solid fraction from dairy cattle manure (Van Dooren, 2010 Unpublished data).

^g (Wesnæs et al., 2009).

^h Energy requirement for processing (De Vries et al., 2011).

ⁱ (Huijsmans et al., 2011; Huijsmans and Hol, 2010; Huijsmans et al., 2007).

^j (Velthof and Hummelink, 2011; Velthof and Mosquera, 2010).

^k (Stehfest and Bouwman, 2006).

^l (Dekker et al., 2009).

^m (De Vries et al., 2011; DR, 2009)

ⁿ (EcoinventCentre, 2007).

Table 4. Transport distances and method of transportation in the references and scenarios

Scenario	Supply of manure (km)	Supply of mineral fertilizer (km)	Local transport (km)	External transport (km)	Outside NL transport (km)
PRef	-		31 ^a	120 ^a	200 ^b
PSc1&2	13.9 ^a	50 ^b	31 ^a	120 ^a	200 ^b
CRef	-		1 ^b	50 ^b	-
CSc1&2	13.9 ^a		13.9 ^a	50 ^b	-
Transport method	Lorry >32 ton	Lorry 16 – 32 ton	Lorry >32 ton	Lorry >32 ton	Lorry 16 – 32 ton

‘-‘ = not included.

^a (DR, 2010 Unpublished data).

^b Estimated transport distances. One km distance in CRef with tractor and trailer.

Table 5. Impact assessment results for the life cycle stages in the pig manure reference and scenarios

	Total*	Manure storage	Manure processing & product storage	Anaerobic digestion	Manure application	MC application	Solid fraction/ digestate application	Avoided fertilizer	Transport
Climate change (kg CO ₂ -eq)									
PRef	33.8	51.0	-	-	51.2	-	-	-75.7	7.2
PSc1	36.9	19.9	42.0	-	-	25.1	20.8	-74.8	3.8
PSc2	-5.9	19.9	12.4	-12.9	-	25.1	23.1	-77.2	3.8
Terrestrial acidification (kg SO ₂ -eq)									
PRef	5.0	5.3	-	-	0.31	-	-	-0.65	0.03
PSc1	5.9	4.8	0.99	-	-	0.36	0.33	-0.62	0.02
PSc2	5.6	4.8	0.91	-0.02	-	0.36	0.11	-0.64	0.02
Marine eutrophication (kg N-eq)									
PRef	0.93	0.21	-	-	1.5	-	-	-0.80	0.01
PSc1	0.95	0.19	0.10	-	-	0.73	0.67	-0.76	0.01
PSc2	0.95	0.19	0.05	-0.01	-	0.73	0.76	-0.79	0.01
Particulate matter formation (kg PM ₁₀ -eq)									
PRef	0.62	0.69	-	-	0.06	-	-	-0.15	0.01
PSc1	0.76	0.63	0.15	-	-	0.05	0.05	-0.14	0.01
PSc2	0.69	0.63	0.12	-0.01	-	0.05	0.02	-0.14	0.01
Fossil fuel depletion (kg oil-eq)									
PRef	-6.4	0.53	-	-	0.62	-	-	-10.3	2.8
PSc1	-4.3	0.48	3.4	-	-	0.18	0.21	-10.0	1.5
PSc2	-10.2	0.48	3.4	-5.5	-	0.18	0.09	-10.2	1.5

‘-‘ = not included, *Totals do not always correspond to the sum of columns due to rounding.

Table 6. Impact assessment results for the life cycle stages in the cattle manure reference and scenarios

	Total*	Manure storage	Manure processing & product storage	Anaerobic digestion	Manure application	MC application	Solid fraction/digestate application	Avoided fertilizer	Transport
Climate change (kg CO ₂ -eq)									
CRef	69.0	87.0	-	-	19.0	-	-	-37.7	0.7
CSc1	22.9	9.2	27.9	-	-	10.5	6.9	-34.0	2.2
CSc2	-2.5	9.2	11.1	-7.7	-	10.5	7.0	-34.8	2.2
Terrestrial acidification (kg SO ₂ -eq)									
CRef	1.4	0.67	-	-	0.99	-	-	-0.29	0
CSc1	1.8	0.67	0.58	-	-	0.24	0.56	-0.27	0.01
CSc2	1.5	0.67	0.53	-0.01	-	0.24	0.33	-0.28	0.01
Marine eutrophication (kg N-eq)									
CRef	0.61	0.03	-	-	0.95	-	-	-0.37	0
CSc1	0.60	0.03	0.07	-	-	0.42	0.40	-0.33	0
CSc2	0.59	0.03	0.03	0	-	0.42	0.45	-0.34	0
Particulate matter formation (kg PM ₁₀ -eq)									
CRef	0.16	0.09	-	-	0.14	-	-	-0.07	0
CSc1	0.24	0.09	0.09	-	-	0.04	0.08	-0.06	0
CSc2	0.18	0.09	0.07	0	-	0.04	0.05	-0.06	0
Fossil fuel depletion (kg oil-eq)									
CRef	-3.9	0.48	-	-	0.46	-	-	-5.1	0.26
CSc1	0.4	0.48	3.4	-	-	0.18	0.21	-4.8	0.84
CSc2	-3.1	0.48	3.4	-3.3	-	0.18	0.08	-4.8	0.84

‘-‘ = not included, *Totals do not always correspond to the sum of columns due to rounding.

Table 7. Results of the sensitivity analysis for the tested parameters

	Tested parameters					
	Baseline	CH ₄ from manure storage	NH ₃ manure processing	NFRV of MC		Heat use AD
				-20%	+20%	
Climate change (kg CO ₂ -eq)						
PRef	33.8	-	-	-	-	-
PSc1	36.9	62.9	36.6	48.2	25.6	-
PSc2	-5.9	20.1	-6.7	5.5	-17.2	-12.8
CRef	69.0	-	-	-	-	-
CSc1	22.9	101	22.8	29.7	16.2	-
CSc2	-2.5	75.3	-3.1	4.2	-9.3	-6.6
Terrestrial acidification (kg SO ₂ -eq)						
PRef	5.0	-	-	-	-	-
PSc1	5.9	-	5.5	6.0	5.8	-
PSc2	5.6	-	5.2	5.7	5.5	-
CRef	1.4	-	-	-	-	-
CSc1	1.8	-	1.6	1.8	1.7	-
CSc2	1.5	-	1.3	1.5	1.4	-
Marine eutrophication (kg N-eq)						
PRef	0.93	-	-	-	-	-
PSc1	0.95	-	0.94	1.08	0.81	-
PSc2	0.95	-	0.94	1.08	0.81	-
CRef	0.61	-	-	-	-	-
CSc1	0.60	-	0.60	0.67	0.52	-
CSc2	0.59	-	0.60	0.67	0.52	-
Particulate matter formation (kg PM ₁₀ -eq)						
PRef	0.62	-	-	-	-	-
PSc1	0.76	-	0.71	0.77	0.74	-
PSc2	0.69	-	0.64	0.71	0.67	-
CRef	0.16	-	-	-	-	-
CSc1	0.24	-	0.21	0.25	0.23	-
CSc2	0.18	-	0.16	0.19	0.17	-
Fossil fuel depletion (kg oil-eq)						
PRef	-6.4	-	-	-	-	-
PSc1	-4.3	-	-4.4	-3.3	-5.3	-
PSc2	-10.2	-	-10.3	-9.1	-11.2	-12.8
CRef	-3.9	-	-	-	-	-
CSc1	0.4	-	0.4	1.0	-0.2	-
CSc2	-3.1	-	-3.2	-2.6	-3.7	-4.7

‘-’ = no change.