Food gels filled with emulsion droplets

Linking large deformation properties to sensory perception

Guido Sala

Structure and Functionality

The 'Structure and Functionality' program aims at elucidating how the sensory characteristics and the stability of foods are related to the molecular properties of food constituents and their mesoscopic interactions and structures.

The research described in this thesis was part of both WCFS projects 'Engineered Textures of Emulsions and Foams' and 'Dynamics of biopolymer networks and textures'.

Project Engineered Textures of Emulsions and Foams

The aim of this project was to provide the industry with tools to simultaneously control the oral perception and the stability of compound food products. To this end, mechanistic knowledge was developed on factors and processes that determine the behaviour of emulsions and foams in the mouth, and how this behaviour translates to perception.

Project Dynamics of biopolymer networks and textures

The long-term goal of this project was to enable the industry to design and manufacture microstructures responsible for specific mouth-feel performance and stability of semi-solid composite food products, based on biopolymer networks. Material and mechanical properties of semi-solid foods and ingredients were related to sensory attributes. The research followed two approaches: the first was related to the identification of parameters having an impact on the oral perception of the food product. The other research line focussed on enabling these parameters to become engineered in food products, such that they become available during oral processing.

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Key words: polymer gels, particle gels, emulsion, large deformation, friction, sensory

Abstract

This thesis reports studies on the large deformation and lubrication properties of emulsionfilled gels and the way these properties are related to the sensory perception of the gels. The design of the studies included polymer and particle gels containing oil droplets of which the interaction with the gel matrix was varied, resulting in droplets either bound or unbound to the matrix. The unique combination of gel matrices and droplet-matrix interactions allowed to obtain a representative overview of the effect of the oil droplets on the properties studied.

The molecular properties of the gel matrices determined the way the large deformation properties of the gels depended on the deformation speed. Polymer gels showed a predominantly elastic behaviour. Particle gels showed a more viscoelastic behavior. The effect of the oil content on the Young's modulus of the gels was modulated by the droplet-matrix interactions, in agreement with existing theories. Bound droplets increased the Young's modulus of the filled gels, whereas unbound droplets decreased it. Oil droplets embedded in the gel matrix acted as stress concentration nuclei. They also increased energy dissipation due to friction between structural elements of the gel (oil droplets and gel matrix). Stress concentration resulted in a decrease of the fracture stress for polymer gels. For gels with non-aggregated bound droplets, a reduction in oil droplet size had the same effect on their rheological properties as an increase in oil volume fraction.

The lubrication properties of the gels strongly depended on both the molecular and functional properties of the gel matrix and the oil content. For each type of gel matrix, the lubrication behaviour was affected by the 'apparent viscosity' of the broken gels, which in turn depended on the droplet-matrix interactions.

The sensory perception of emulsion-filled gels appeared to be dominated by the properties of the gel matrix and by the oil content. Polymer gels were perceived as more melting, whereas particle gels were perceived as more rough. With increasing oil content

both types of gels became more creamy and spreadable. The increase in spreadability and part of the increase in creaminess could be explained with the effect of the oil droplets on the breakdown properties of the gels. Since for all gels the scores for creaminess increased with increasing oil content, the release of oil droplets during oral processing could not completely explain the perception of oil-related sensory attributes. It is therefore concluded that the perception of these attributes is mediated by the lubrication properties of the broken gel. The large deformation and lubrication behaviour of the gels were the most important parameters related to sensory perception. Both parameters were affected by the droplet-matrix interaction. As a matter of fact, the droplet-matrix interaction affected the fracture behaviour of the filled gels, which was related to their spreadability, and the 'apparent viscosity' of the broken gels, which controlled the lubrication properties of these systems.

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Chapter 1

Introduction

1.1 Food gels filled with emulsion droplets

A gel can be described as 'a continuous network of macroscopic dimensions immersed in a liquid medium and exhibiting no steady-state flow' (Ziegler & Foegeding, 1990). This definition applies to many different foods. Flory (1974) classified gels into four categories on the basis of the structural elements of the continuous network:

- 1. Well-ordered lamellar structures.
- 2. Covalent polymer networks.
- 3. Polymer networks formed through physical aggregation.
- 4. Particulate, disordered structures.

The first class comprises inorganic gels from clays or other minerals and soap gels. Good examples of covalent polymer gels are polyacrylamide gels and vulcanised rubbers. Into the third class fall physical gels of entangled polymers, like gelatine and carrageenan gels. Particulate (or particle) gels consist of clusters of aggregated particles forming a continuous structure throughout the enclosing volume. Milk protein gels fall into this class. Only the last two classes of gels are of relevance for food products.

A typical characteristic of foods is their complexity, due to the presence of many different components and ingredients. Several food products can be described as gels filled with emulsion droplets (or emulsion-filled gels). Milk is an emulsion of fat globules in a colloidal suspension of casein micelles. Many different food products of the food industry are based on the gelation of milk, resulting in a continuous matrix of interconnected swollen casein particles entrapping dispersed fat globules. Each application makes use of a specific physicochemical gelation mechanism. In cheese-making, gelation is achieved by the enzymatic activity of rennet, which causes the removal of the hydrophilic moiety of κ -casein. This results in the aggregation of casein by hydrophobic and Van der Waals interactions (Sandra, Alexander & Dalgleish, 2007). Not only fresh curd, but also cheese, the end product derived from further processing of curd, can be described as a (strong) gel containing dispersed fat globules. In the production of yoghurt and other acidified dairy products, inorganic calcium phosphate gradually dissolves as the pH of milk decreases from the natural value of 6.7 (Donato, Alexander & Dalgleish, 2007). Furthermore, as the pH decreases the surface charges of the casein micelles are protonated. This causes the collapse of the hydrophilic moiety of κ -casein, which results in

the destabilisation of the casein colloidal suspension and, eventually, in milk gelation. In several dairy desserts, polymers like gelatin or κ -carrageenan are added as ingredients. These desserts usually contain dairy cream and can therefore be described as emulsion-filled gels. Examples of these products are Bavarois desserts and other kinds of dairy desserts, both whipped of non-whipped. For these products gelation does not involve physicochemical changes of the casein micelles suspension, but it is the result of the solgel transition occurring as the temperature of the system is decreased after dissolution of the polymer (Walstra, 2003). The preparation of a number of meat products, like Frankfurters and Bologna sausage, involves the disintegration of the raw materials, giving rise to aqueous colloidal systems composed of a protein matrix in which solid compounds like insoluble protein and fat particles are dispersed (Carballo, Solas & Colmenero, 1993). When these systems are heated they undergo gelation. These products can also be described as emulsion-filled gels.

Texture and flavour are a main components of the sensory properties of food products. Texture can be defined as 'all the rheological and structural (geometric and surface) attributes of the product perceptible by means of mechanical, tactile and, where appropriate, visual and auditory receptors' (Lawless & Heymann, 1998). Fat plays an essential role in the sensory perception of emulsion-filled gels. This is clearly shown by the decrease in liking and acceptability accompanied by fat reduction in several different foods (van den Oever, 2006). Cheese with reduced fat is perceived as 'more waxy, fracturable, chewy, hard and springy' and 'less sticky, cohesive, meltable and smooth' than full-fat cheese (Gwartney, Foegeding & Larick, 2002). For yoghurt, the fat content is found to affect sensory properties in all the categories, i.e. odour, flavour, taste and texture (Folkenberg & Martens, 2003). Fat reduction results in a decrease of creaminess and sweet taste perception and in an increase of astringency, bitter and sour taste. In frozen dairy desserts creaminess decreases and wateriness and coarseness increase as result of fat reduction (Specter & Setser, 1994). Low fat Frankfurters are drier and tougher than the full-fat version (Sofos & Allen, 1977; Hand, Hollingsworth, Calkins & Mandigo, 1987; Lee, Whiting & Jenkins, 1987).

Despite the important role played by fat in the texture and overall sensory perception of emulsion-filled gels, consumer liking is often not directly and simply related to fat level (van den Oever, 2006). This means that fat is involved in texture and sensory perception mechanisms which can also be influenced by parameters independent of fat level. The control of these mechanisms requires thorough knowledge of both the effect of emulsion droplets on the physicochemical and mechanical properties of emulsion-filled gels, and of the role played by these properties in the sensory perception of these systems. These aspects are at the moment not satisfactorily covered by the scientific literature.

1.2 Rheological characterisation of gels

Rheology deals with the relationships between forces and deformations of materials. In the case of foods the goals are to 'understand the effect of processing on products, to probe the system's structure and to reveal critical aspects of food texture' (Foegeding & Drake, 2007). For rheological measurements of viscoelastic solid foods, three different regimes can be distinguished based on the nature of the relationship between stress (σ) and strain (ϵ) (Figure 1.1). In the first regime (I), called the linear regime, a linear relation between stress and strain can be observed; in other words Hooke's law is obeyed. In the second regime (II) the relationship between stress and strain is nonlinear. Beyond the nonlinear regime fracture of the material occurs (fracture regime, III). Measurements performed in the linear regime are called small-deformation measurements. In the linear regime, the deformation applied does not affect the structure of the strain (van Vliet, 1999). Measurements performed in the nonlinear and fracture regimes are called large-deformation measurements, or, when they are mainly focussed on the determination of the fracture properties of the material, fracture measurements.

The rheological properties of gels have mainly been studied at small deformation. This holds also for the effect of emulsion droplets on the rheological properties of emulsion-filled gels (van Vliet, 1988; Dickinson, 1995, 1996, 1997; Chen, 1998, 1999; Chen & Dickinson, 1999; Chen, Dickinson & Edwards, 1999; Dickinson, 1999). However, when aiming at linking rheological properties to texture characteristics and sensory perception, large deformation measurements are more relevant: eating obviously involves large deformations (Luyten, van Vliet & Walstra, 1992). For certain kinds of food, like cheese, rheological properties determined in the nonlinear and fracture regimes show a high degree of correlation with sensory properties (Foegeding et al., 2007).

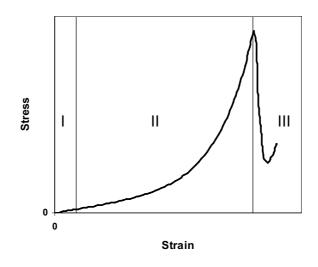


Figure 1.1 – Rheological regimes for viscoelastic solids.

Three different types of deformation can be distinguished: all-sided (isotropic) compression, simple shear and uniaxial compression or extension. The deformation applied in measurements is often not simply one of these types, but a combination of them (Luyten et al., 1992; Hamann, Zhang, Daubert, Foegeding & Diehl, 2006). The four main techniques used for the measurement of large deformation and fracture properties are: uniaxial compression and tension, bending and torsion (Luyten et al., 1992; Hamann et al., 2006; Truong & Daubert, 2000). Uniaxial compression is the most used technique for food products because it is easy to perform. Furthermore, uniaxial compression largely reflects what happens during chewing. With this technique fracture can start both within and at the outside of the sample. Tension tests apply a similar, but opposite deformation as compared to compression measurements. With this technique fracture starts almost always at the outside of the sample, and therefore fracturing can be observed more easily than for uniaxial compression measurements. Tension tests are not frequently used for food products because of the difficulty to grip the sample. Strong attachment of the specimen to the machine and specific specimen shapes are required to relieve the stress at the point of attachment. Both requirements are difficult to achieve with food material, especially with gels. In bending tests the applied deformation consists of a combination of compression, extension and shear. Fracture almost always starts at the surface of the deformed part of the specimen. Torsion measurements produce a pure shear stress, maintaining volume and shape of the specimen during testing. The specimens should be capstan-shaped. This,

together with the need of strong attachment of the specimen to the machine, results in tedious sample preparation. As a consequence torsion tests are not widely used for food products.

For isotropic materials the Young's modulus as determined in the linear region should be independent of the measurement technique (Luyten et al., 1992). However, for fracture parameters differences can be observed between results from different techniques. Fracture stress and fracture strain measured in uniaxial compression and torsion tests are often in good agreement (Hamann et al., 2006). The fracture stress is often independent of the technique applied (Hamann et al., 2006). Fracture stress values observed in tension and bending tests tend to be lower than those measured in compression and torsion tests (Luyten et al., 1992; Hamann et al., 2006). Samples tested by tension and bending usually fracture at lower strain than those tested by compression and torsion.

1.3 Sensory characterisation of gels

Several different methods have been used for the sensory characterisation of food products. Nowadays three main groups of sensory tests can be distinguished: discrimination tests, acceptance (or affective) tests, and descriptive analysis (Stone & Sidel, 2004). Discrimination tests are used to verify whether two products are perceived as different. This can be useful when optimising the production process, or when substituting ingredients of a product already on the market. Some of the methods used for discrimination tests are well known, such as the paired-comparison test and the triangle test. The information that can be obtained with these tests is rather limited. For this reason discrimination tests usually precede other sensory tests. The aim of acceptance tests is to measure the liking of or preference for a product (Stone et al., 2004). Preference can be measured either directly, by comparison between two or more products, or indirectly, on the basis of the scores obtained in a multi-product test. Acceptance tests are often applied during the introduction of new products, usually before a large scale test such as a marketing research. Descriptive analysis is the most sophisticated kind of sensory test presently available (Stone et al., 2004). It provides a complete quantitative sensory description of a set of products. This allows to map product similarities and differences and to determine the sensory attributes relevant for acceptance. Furthermore, the results of descriptive analysis enable researchers to relate specific product properties to specific

sensory attributes. Unlike discrimination and acceptance tests, descriptive analysis requires qualified subjects, having an enhanced ability to perceive taste, aroma and texture differences. Different methodologies are used for descriptive analysis. For research purposes the most powerful methodology is the Quantitative Descriptive Analysis (QDA). This methodology requires only a limited number of subjects (typically 10-12). They should be highly skilled, since they should be able to describe all sensory properties of a product and to evaluate several products in one session. The subjects create a specific sensory vocabulary to describe product properties. For each evaluated product all attributes listed in this vocabulary receive a score. The scores are subsequently analysed by the analysis of variance method or principal component analysis.

The vocabulary created by QDA sensory panels for the description of the properties of gels can vary widely. The odour and taste attributes are mainly related to other ingredients present in the gel than the gelling agents. Mouthfeel terms, describing gel firmness and strength ('deformable', 'elastic', 'firm', 'fracture force', 'chewiness', 'springy', 'cohesive', 'short') are usually present in this vocabulary (Autio, Kuuva, Roininen & Lahteenmaki, 2002; Gwartney et al., 2002; Pereira, Singh, Munro & Luckman, 2003; Barrangou, Drake, Daubert & Foegeding, 2006; Foegeding et al., 2007; van den Berg, van Vliet, van der Linden, van Boekel & van de Velde, 2007). This first group of mouthfeel terms is usually connected to concentration and molecular properties of the gelling agent and to the presence of other ingredients with an effect on firmness and strength. A second group of mouthfeel attributes can be selected by the QDA panel to describe (i) possible release of water from the gel during mastication ('watery', 'separating'), (ii) creation of a coating layer in the mouth after oral processing ('sticky', 'coating'), (iii) melting of the gels during breakdown ('melting'), (iv) presence of particles in the broken gel ('mealy', 'grainy') or (v) other specific sensations ('slippery', 'spreadable', 'smooth', 'creamy', 'fatty') (Autio et al., 2002; Gwartney et al., 2002; Pereira et al., 2003; Foegeding et al., 2007; van den Berg et al., 2007). Mouthfeel attributes of this second group are related to the molecular and functional properties of both gelling agents and other ingredients under oral processing conditions. Afterfeel attributes, i.e. sensory attributes describing the sensations perceived after oral processing of the gels, are directly connected to the second group of mouthfeel attributes.

In literature the sensory characterisation of gels is generally complemented by the study of correlations with instrumental measurements, both at small and large deformations. Instrumental measurements usually correlate well with sensory attributes describing gel firmness and strength (Autio et al., 2002; Gwartney et al., 2002; Pereira et al., 2003; Barrangou et al., 2006; Foegeding et al., 2007; van den Berg et al., 2007). Correlations between instrumental measurements and sensory attributes require a mechanistic link. This is of particular importance for sensory attributes of the second group. Coincidental correlations without a plausible mechanistic link are one of the main obstacles for understanding the sensory perception of foods (Foegeding et al., 2007).

1.4 Aim of the thesis

The emulsion droplets embedded in the matrix remarkably affect the rheological behaviour and the functional properties of the filled gels. So far, the effect of the droplets on rheological properties has been studied mainly at small deformations. The effect of the droplets on large deformation properties is still not completely clear. This makes it difficult to formulate mechanistic hypotheses on the sensory perception of emulsion-filled gels. For instance, it is still not clear whether the emulsion droplets are directly perceived or whether it is their effect on mechanical behaviour that dominates sensory perception. In order to gain control of the sensory perception of emulsion-filled these aspects must be clarified.

The aim of this thesis is to unveil the most important effects of emulsion droplets on the mechanical properties of model emulsion-filled gels resembling real food products, and to formulate a hypothesis on the role played by these properties in sensory perception mechanisms. The envisaged results could represent a tool for the food industry to engineer emulsion-filled gels with desired sensory properties and to overcome the difficulties related to the development of reduced fat foods. The knowledge of sensory perception mechanisms related to the presence of emulsion droplets in the gel matrix is of basic importance to find ingredients able to mimic the effect of the droplets.

1.5 Description of the gel systems studied

1.5.1 Combinations gelling agents-emulsions

For this thesis, several model gel systems resembling real food products were selected. Models for both polymer and particle gels were optimised. As examples for polymer gels, gelatine and κ -carrageenan were chosen. These two polymers were both selected because they represent different breakdown and viscoelastic behaviours. Emulsion-filled gels prepared with these polymers can be compared to several different types of dairy desserts. As an example of particle gels acid-induced, cold-set whey protein isolate (WPI) gels were chosen. The structure of emulsion-filled WPI gels roughly resembles that of set yoghurt and of rennet milk curd.

For emulsion-filled gels, the emulsifying agent adsorbed onto the surface of the oil droplet determines the interactions between oil droplet and gel matrix (Chen & Dickinson, 1999). When, for instance, attractive electrostatic interactions occur between emulsifying agent and gelling agent, the oil droplets will be bound to the gel matrix. Therefore, the droplet-matrix interactions of the filled gels studied were varied by changing the emulsifying agent used for emulsion preparation. In Table 1.1 the various combinations of gel matrices and emulsifying agents are reported.

	Gelling agent		
Emulsifying agent	Gelatin	ĸ-carrageenan	WPI
Native WPI	Bound	Unbound	
WPI aggregates			Bound
Lysozyme		Bound	Bound
Lactoferrin		Bound	
Tween 20	Unbound		

 Table 1.1 – Combinations between gel matrices and emulsifying agents studied in this thesis.

The preparation procedure and the composition of gelatin and κ -carrageenan gels slightly evolved during the period in which the experimental measurements were performed. The ageing time of gelatin gels increased from 24 (chapters 3, 4 and 7) to 48 (chapters 5, 6 and 8) hours. As a result, the latter gels showed slightly higher moduli, but the fracture properties did not significantly change. Therefore, the results obtained with the two different ageing times are comparable. This modification of the preparation procedure was introduced because it facilitates the extraction of the gels from the tubes in which they were prepared. Kappa-carrageenan gels were firstly prepared with a gelling agent concentration of 0.75 wt% and in a 10 mM KCl solution (chapters 3 and 4). The gelling agent concentration was later decreased to 0.60 wt% and the concentration of the KCl solution was increased to 30 mM (chapters 5, 6, 7 and 8). This resulted in a gel with a longer gelation time and facilitated the preparation of gels containing emulsion droplets. The modification of the composition of κ -carrageenan gels did not significantly affect the Young's modulus and the fracture properties of the gels.

1.5.2 Molecular and functional properties of the gelling agent

1.5.2.1 Gelatine

Gelatine is a heterogeneous product derived from the controlled acid or alkaline hydrolysis of collagen (Harris, 1990; Simon, Grohens, Vandanjon, Bourseau, Balnois & Levesque, 2003; Walstra, 2003). Its composition and its functional properties are influenced by source, age and type of collagen. The molecular structure of collagen consists of a triple helix with three discrete α -chains in which glycine residues occupy every third site, leaving a space that on the other two chains can be occupied by hydroxyproline and proline residues. This sequence makes the formation of interchain hydrogen bonds possible.

Commercial gelatines are characterized by two parameters:

- bloom value (function of the gel strength at a certain concentration and at 10°C, measured after keeping the gel at this temperature for 18 hours)
- viscosity of a solution with the same concentration used for the bloom value and at the temperature of 60°C.

Gelatine is insoluble in cold water and liquid foods (e.g. milk, juices). Nevertheless, in these fluids it will swell and absorb water up to its own weight. A presoaking in cold water allows lower temperatures to be used for complete dissolution. The preparation of solutions without presoaking requires temperatures of 60-80°C, whilst after presoaking temperatures of 50-60°C are sufficient. The duration of the presoaking treatment depends on the size of the gelatine granules and on the molecular properties of the gelatine.

Upon cooling, junctions involving triple helices form, and the interactions among helices increase, resulting in gel formation. The formation of junctions is a slow process and the modulus of the gel can keep increasing for several days. The minimum concentration for gel formation is about 1 wt%. The gel strength is affected by gelatine concentration, pH, gelation time and temperature, gelatine and gel composition.

1.5.2.2 <u>Carrageenans</u>

The term carrageenan refers to a group of linear sulphated galactan polysaccharides extracted from red marine seaweeds (*Rhodophyceae*) (Stephen, Phillips & Williams, 2006). The basic unit of carrageenans is a repeating disaccharide sequence consisting of β -d-galactopyranose residues linked through positions 1 and 3 (A residues), and α -galactopyranose residues linked through positions 1 and 4 (B residues). Carrageenans can be differentiated on the basis of content and position of ester sulphated substitutes. From a commercial point of view only kappa (κ), iota (ι) and lambda (λ) are relevant. The substitutions of these carrageenans are as follows (Figure 1.2):

- κ: one sulphate group at C4 of the 1,3 linked residue and presence of the 3,6anhydrobridge linkage;
- u: one sulphate group at C4 of the 1,3 linked residue, one at C2 of the 1,4; presence of the 3,6-ether linkage;
- λ: at C2 of the 1,3 linked residue hydroxyl groups in 30% and sulphate groups in 70% of the cases; one sulphate group at C2 and one at C6 of the 1,4 linked residue; absence of the 3,6-ether linkage.

Native carrageenans from different sources contain mixtures of the polysaccharides variants and intermediate hybrids with different degree of anhydration and 2-sulphation of the 1,4 linked residues.

Kappa-carrageenans form solutions that are gelled by potassium ions. Solutions of ı are gelled by calcium ions. Lambda-carrageenans do not form gels. The functional properties of these carrageenans can be summarized as follows:

- κ: has the highest gelation power and in water and milk it gives strong, brittle gels with remarkable syneresis; for complete solubilisation a temperature of 75°C is required;
- 1: in water and milk it forms elastic gels with low syneresis; heating to 60°C is required for complete solubilisation;
- λ : due to its high sulphate content, it is the most soluble in cold water and milk, providing high viscosity and stability.

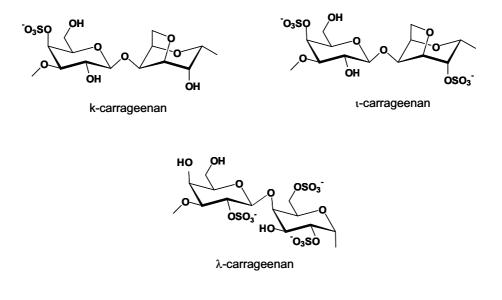


Figure 1.2 – Chemical structure of three types of carrageenans.

On cooling, hot solutions of gelling carrageenans set to gels. This happens because of the association of molecular chains into double helices. At temperatures above the gelling point, the formation of helices is prevented by thermal agitation. In this situation, the polymer assumes a random coil structure. At first the polymer chains associate in double helices to give small ordered domains. In order for these domains to aggregate in a three-dimensional network, the presence of cations (the most effective being potassium for κ -carrageenan and calcium for ι -carrageenan) that lock together helical regions of adjacent domains is required. In presence of calcium ions k-carrageenan gels are rigid and subject to syneresis. With potassium as only counterion, syneresis is prevented.

Electrostatic interactions can occur between the negatively charged carrageenans and positively charged sites on proteins. An example of this phenomenon is the specific interaction between k-carrageenans and k-casein at pH values above the isoelectric point of the protein, which results in the formation of a gel.

1.5.2.3 <u>Whey Protein Isolates (WPI)</u>

The main whey proteins present in milk are β -lactoglobulin (3.2 g/ kg), α -lactalbumin (1.2 g/ kg), immunoglobulins (0.7 g/ kg) and bovine serum albumin (0.4 g/ kg) (Walstra, Wouters & Geurts, 2005). Beta-lactoglobulin (molecular mass: 18.3 kDa) is present in milk and in aqueous solutions with pH in the range 3.5-5.2 as reversible dimer. It consists of 162 amino acid residues and contains one free thiol group and two disulphide bonds (Kinsella, 1984). The isoelectric point (pI) of the protein is 5. This protein is heat sensitive: at 30°C dimers dissociate and above 55°C a progressive unfolding of the globular structure occurs, exposing cysteine and hydrophobic groups and allowing primary and secondary aggregation. Moreover, it undergoes molecular modifications at different pH values. It is stable to denaturation at pH 2, it forms octomers in the same pH range at 0°C and it becomes unstable and prone to denaturation at pH higher than 8.

Alpha-lactalbumin (molecular mass 14.2 kDa) is a calcium-binding metalloprotein, consisting of 123 amino acids residues and with a pI of 4.2-4.5. It is an almost spherical, very compact globular protein whose structure is stabilised by four disulphide bonds. Calcium binding induces major changes in the tertiary structure of the protein. The molecule is stable between pH 5.4 and 9.0. Between pH 4.0 and 5.0 it shows low solubility and below 4.0 and above 9.0 it undergoes molecular changes. Alphalactalbumin is the most heat-stable of the main whey proteins. Removal of calcium reduces its heat stability.

Immunoglobulins are large, extremely heat-sensitive globular proteins. A treatment at 70°C for 30 minutes denatures them completely. They exist either as monomer or as polymer, the basic unit consisting of four polypeptide chains molecules, two identical light chains (molecular mass about 20 kDa) and two identical heavy chains (molecular mass 50-60 kDa). The chains are linked by disulphide bonds. The different types of immunoglobulins are distinguished by differences in amino acid sequences in the constant regions of the heavy chains.

The molecular structure of bovine serum albumin (molecular mass 66.2 Da) is stabilised by 17 disulphide groups. Only one free thiol group is present. This globular protein is essentially monomeric, even though dimers and higher polymers occur. At pH lower than 4 the molecule undergoes acid denaturation because of charge repulsion.

By ultrafiltration and diafiltration techniques whey protein concentrate (WPC) powders with high protein content (> 80 %) can be obtained. Further purification with these techniques results in WPI with protein concentration \geq 98%. Gelation of solutions of whey proteins can be induced in several ways (Totosaus, Montejano, Salazar & Guerrero, 2002). Heat-induced gelation is one of the most studied phenomena in food science. Whey protein gels can also be formed by acid and salt induced cold gelation of heat-denatured dispersions, high-pressure treatment, urea addition and transglutaminase-catalysed covalent cross-linking.

Heat-induced gelation occurs at 70-80°C, provided that the protein content is sufficient. Gel formation does not occur at protein concentration lower than 5% and firm gels are prepared only with concentrations higher than 8%. Gelation temperature and gel strength are influenced by:

- ionic strength;
- protein content;
- pH;
- type of ions present;
- total solid content.

The pH assumes a particular role in the heat induced gelation of whey protein. With regard to gel strength, the optimal value is 7. At this pH and between the range 6-7, a white, curdy gel is formed. Below pH 5 and above 7 not only the gelation time/ temperature increases, but translucent gels are obtained. Translucent gels are firmer and less prone to syneresis. Gel produced at pH 6.0-6.5 can sustain a considerable compression (80%) without fracturing and partially recovering the original shape. Being easily compressed, the gel strength of these systems is limited. Gels prepared by addition of phosphates and at pH 7 are much more rigid and gelatin-like, but more susceptible to fracture. Variations of the temperature, both above 100°C and at freezing temperature, have limited effects on gel characteristics.

Cold gelation has been studied for preheated solutions of β-lactoglobulin, WPC and WPI (Vreeker, Hoekstra, Den Boer & Agterof, 1992; Barbut & Foegeding, 1993; Barbut, 1995; Sato, Nakamura, Nishiya, Kawanari & Nakajima, 1995; Hongsprabhas & Barbut, 1996; Roff & Foegeding, 1996; Elofsson, Dejmek, Paulsson & Burling, 1997; Hongsprabhas, Barbut & Marangoni, 1999; Alting, 2003). In cold gelation the heatinduced activation step is uncoupled from gel formation. In the first step of the cold gelation process a solution of native whey proteins is heated at pH far from the pI, at low ionic strength and at concentrations too low for gel formation. This results in a stable dispersion of protein aggregates. The protein concentration during heating determines the physicochemical properties of the aggregates and, therefore the rheological properties of the gels. In a second step gelation of the diluted aggregates dispersion occurs at ambient temperature by decreasing the pH or increasing the ionic strength of the solvent.

The preparation of emulsion-filled whey protein gels by heat induced gelation implies the addition of the emulsion to the whey protein solution before heating. This means that also the added emulsion undergoes a severe heat treatment, which could cause modifications of the emulsifying agents used for emulsion preparation. When proteins are chosen as emulsifying agent, this could result in the denaturation of the proteins adsorbed on the surface of the emulsion droplets. In the preparation of emulsion-filled whey protein gels by cold gelation the emulsion is added to the protein aggregates dispersion before acidification of salt addition. Therefore, the emulsion does not undergo heating and possible modifications of the emulsifying agents are prevented. This represents an important advantage. Therefore, in this thesis whey protein gels were prepared by acidinduced cold gelation.

1.6 Outline of the thesis

This thesis reports studies on the effect of oil droplets on both the mechanical and sensory properties of emulsions-filled gels resembling real food products.

In chapter 2 the optimisation of the preparation of WPI emulsion-filled gels is described. In this chapter the difficulties to achieve stable systems and the physicochemical mechanisms causing phase separation in emulsion-filled gels are discussed. The rheological properties both at small and large deformations are presented.

Chapter 3 deals with the large deformation properties at constant compression speed of gelatin, κ -carrageenan and WPI gels containing emulsion droplets with varying interactions with the gel matrix. The microstructure of these gels, as studied by Confocal Scanning Laser Microscopy (CLSM), is discussed in relation to the physicochemical

mechanisms leading to oil droplet aggregation. The effect of oil droplet aggregation on large deformation properties of gelatin and WPI gels is also studied.

Chapter 4 reports the results of an explorative sensory study in which gelatin, κ carrageenan, mixed κ/ι -carrageenan and WPI gels containing emulsion droplets with
varying interactions with the gel matrix are characterised. The effect of both oil content
and kind of gel matrix on sensory perception is discussed. An attempt is made to correlate
the scores of mouthfeel attributes with instrumental measurements performed at constant
compression speed. For gelatin gels the effect of oil droplet aggregation on sensory
perception is covered.

In chapter 5 the large deformation and viscoelastic properties of gels with increasing oil concentration are studied with particular attention to the rate of deformation. In chapter 6 the same properties are studied for gels with constant oil concentration, but varying gelling agent concentration and oil droplet size. For both chapters the gels studied were gelatin, κ -carrageenan and WPI gels containing emulsion droplets with varying interactions with the gel matrix.

Chapter 7 deals with the role of the release of oil droplets during oral processing in the sensory perception of gelatin, κ -carrageenan and WPI gels containing emulsion droplets with varying interactions with the gel matrix. The analytical method optimised for the quantification of the release of oil droplets *in vitro* upon gel shearing is presented in detail.

Finally, in chapter 8 the friction properties of emulsion-filled gels are studied. The roles played by the individual gel components and by saliva are discussed. Furthermore, the mechanism relating the interaction between oil droplets and gel matrix to the friction properties of the gels is explained. In this study the gels were broken so as to resemble a sheared gel resulting from oral processing.

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Chapter 2

Gelation of emulsions stabilised by whey protein aggregates

P. Rosa, G. Sala, T. van Vliet, F. van de Velde (2006). Cold gelation of whey protein emulsions, *Journal of Texture Studies*, 37, 516-537.

Abstract

Stable and homogeneous emulsion-filled gels were prepared by cold gelation of whey protein isolate (WPI) emulsions. A suspension of heat denatured WPI (soluble WPI aggregates) was mixed with a 40 wt% oil-in-water emulsion to obtain gels with varying concentrations of WPI aggregates and oil. For emulsions stabilised by native WPI, creaming was observed upon mixing of the emulsion with a suspension of WPI aggregates, likely as a result of depletion flocculation induced by the differences in size between the droplets and aggregates. For emulsions stabilised by soluble WPI aggregates, the obtained filled suspension was stable against creaming and homogeneous emulsionfilled gels with varying protein and oil concentrations were obtained. Large deformation properties of the emulsion-filled cold-set WPI gels were determined by uniaxial compression. With increasing oil concentration the fracture stress increased slightly, whereas the fracture strain decreased slightly. Small deformation properties were determined by oscillatory rheology. The storage modulus after 16 hours of acidification was taken as a measure of the gel stiffness. Experimental results were in good agreement with predictions according to the van der Poel's theory for the effect of oil concentration on the stiffness of the filled gels. Especially, the influence of the modulus of the matrix on the effect of the oil droplets was in good agreement with the van der Poel's theory.

2.1 Introduction

Upon handling and consumption of food, large deformation and fracture properties are more important than the behaviour at small deformation (van Vliet & Walstra, 1995; van Vliet, 2002). Both functional properties, such as shaping, cutting, slicing and spoonability, and eating characteristics are related to large deformation and fracture properties. The firmness of a gel depends, for example, on the apparent modulus at large deformation and on fracture or yield stress. Some eating characteristics are related to the yield and fracture properties and to the apparent large deformation modulus at the relevant strain rate.

In spite of the relevance of large deformation properties of food products for their sensory characteristics, the theories presently available for the modelling of the rheological properties of emulsion-filled gels are based on small deformation measurements. The van der Poel method for calculating the shear modulus of particulate composites (van der Poel, 1958; Smith, 1974; Smith, 1975) has been also applied for the characterisation of emulsion-filled gels (van Vliet, 1988). Since the method only holds for composites with homogeneously distributed fillers, the agreement between experimental results and calculated data varies widely. Van Vliet (1988) reported that for acid milk gels with emulsion droplets behaving as active fillers, the experimental effect of the oil concentration was largely underestimated by the van der Poel method. On the other hand, the effect of filler concentration was well predicted for polyvinyl alcohol – Congo red gels (van Vliet, 1988). The discrepancy between the predicted effect of the filler concentration on gel modulus and experimental results for heat-set whey protein gels was also attributed to the aggregation of the emulsion droplets (Chen & Dickinson, 1998).

The rheological properties of gels filled with emulsion droplets depend on the mechanical properties of both the gel matrix and the filler particles, the emulsion droplet concentration and the nature of the filler-matrix interactions (Tolstoguzov & Braudo, 1983; van Vliet, 1988). Depending on their effect on gel rheology, filler particles can be classified as either active of inactive (Ring & Stainsby, 1982). Active fillers interact with the gel matrix and increase the gel strength. Inactive fillers have little chemical affinity for the molecules forming the gel matrix and do not strengthen the material. The possibility of interaction between filler and gel matrix depend on the surface properties of the filler matrix, especially the nature of the stabilising agent (Dickinson & Chen, 1999). The effect of the filler also depends on the modulus of the filler particles, the higher the elastic

modulus of the filler the higher the effect of the filler (van der Poel, 1958; van Vliet, 1988). Anisometric particles have a larger effect on the elastic modulus than spherical particles. Furthermore, in the case of filler particles aggregation, the effective size of the particles and their anisometry increase. In some cases the formation of an intermediate layer with a depleted polymer concentration and, thus, a lower modulus, is observed around the particle, see for example (van Vliet, 1988).

Protein gels, in particular whey protein gels, have numerous applications in food products, often in combination with other ingredients. Since gelation is an important functional property that contributes to the appearance, water-holding capacity and texture of food, considerable attention has been paid to protein gelation. Protein gels can be obtained in different ways (Totosaus *et al.*, 2002). Heat-induced gelation is the most common way to produce protein gels. Cold gelation of globular proteins, especially whey proteins, is a method to prepare protein gels with varying textures in a controllable way (Alting *et al.*, 2004; Weijers *et al.*, 2006). This two-step process allows controlling the properties of the protein aggregates and final gel texture independently.

The cold gelation process involves two steps: firstly the preparation of protein aggregates by heating a protein suspension and secondly gelation of these aggregates by gradually lowering the pH of the suspension to a pH below the iso-electric point of the proteins. The heating step has two critical parameters: the protein concentration and the temperature/time profile. The concentration is kept below the gelation concentration to obtain soluble protein aggregates. The heating temperature and time are selected to yield 95 to 100% protein aggregates. The protein concentration during this heating step determines the physical / chemical properties of the aggregates and, thereby, the rheological properties of the final gel (Alting *et al.*, 2003b). In the next step the protein aggregates are diluted to an appropriate concentration to obtain a desired texture of the gel upon acidification the control of the oil content and droplet size of the filler particles independently from the textural properties of the protein matrix (van de Velde, 2004).

Emulsion-filled heat-set gels have attracted enormous attention in the scientific literature over the last decades. Not only filled whey protein gels have been described, but also soy protein (Kim *et al.*, 2001) and egg yolk gels (Koidis *et al.*, 2002). Recently, the first paper on cold gelation of oil-in-water emulsions was published (Sok Line *et al.*, 2005). The authors used calcium-induced gelation of β -lactoglobulin to obtain emulsion-filled gels. Reactive β -lactoglobulin aggregates, obtained after heat treatment, were used

to prepare the oil-in-water emulsion, which gelled upon addition of calcium chloride. The effect of the oil and $CaCl_2$ concentration were studied at constant overall protein concentration.

The aim of this chapter was to study the effect of the concentration of emulsion droplets on the small and large deformation properties of emulsion-filled WPI gels prepared by cold gelation. Acid-induced cold gelation of whey protein isolate was used to prepare emulsion-filled gels in which oil content and droplet size were independently varied from the mechanical properties of the protein matrix. Therefore, well characterised o/w emulsions stabilised with native WPI or heat-denatured WPI dispersions and different droplet sizes were mixed with the active protein aggregates before acidification The rheological properties of these acid-induced cold-set whey protein emulsion-filled gels were determined at small and large deformations. The elastic modulus of the gels measured at small deformation was compared to predictions based on the van der Poel method. The microstructures of these gels were determined by Confocal Laser Scanning Microscopy (CLSM) to monitor the distribution of the oil droplets in the gel matrix.

2.2 Materials and methods

2.2.1 Materials

Whey protein isolate (WPI) was purchased from Davisco International Inc. (BiproTM, La Sueur, MN, USA). Glucono- δ -lactone (GDL) and Rhodamine B were obtained from Sigma Chemicals. BODIPY® 581/591 C₁₁ (4,4-difluoro-5-(4-phenyl-1,3-butadienyl)-4-bora-3a,4a-diaza-s-indacene-3-undecanoic acid) was purchased from Molecular Probes (Leiden, The Netherlands). Commercial peanut oil of food grade quality (density 0.92) was obtained from a local retailer. All ingredients were used without purification. Water purified by reverse osmosis (RO) was used in all cases.

2.2.2 Preparation of WPI aggregates

WPI aggregates were prepared according to published methods (Alting, 2003). WPI was dissolved in RO water at a concentration of 9 wt% and stirred for at least 2 hours at room temperature, until all protein was dissolved. Reactive WPI aggregates were prepared by heating the solution in a water bath for 2 hours at 68.5 °C and cooling to room temperature

by running tap water. This heat treatment results in over 95% aggregation of the proteins (Alting *et al.*, 2003b). The WPI aggregates solutions were stored at 4 °C until use (typically within 1 week).

2.2.3 Preparation of O/W emulsions

Four different oil-in-water emulsions were prepared, their compositions are given in Table 2.1. A 2.7 wt% WPI solution was prepared by dissolving the powdered protein in RO water at room temperature and stirring until all protein was dissolved (typically within 1h). This solution was used without further treatment. A 9 wt% WPI aggregates solution was prepared as described above, and diluted to a 2.7 wt% solution with an appropriate amount of RO water. Oil-in-water emulsions were prepared at room temperature by homogenising weighed amounts of peanut oil (40 wt%) and aqueous phase (60 wt%). Pre-emulsions were prepared with an Ultra Turrax Polytron (KINEMATICA AG, Switzerland). The pre-emulsions were homogenized using a Laboratory Homogenizer Ariete (Model NS1001L – PANDA, Niro Soavia S.P.A., Italy) operating at a pressure as indicated in Table 2.1.

The droplet size distribution of the different emulsions was measured using a Malvern MasterSizer X (Malvern Instruments Ltd., Malvern, UK) and the mean droplet size is reported as the volume-to-surface diameter:

$$d_{32} = \frac{\sum_{i=1}^{N} n_i d_i^3}{\sum_{i=1}^{N} n_i d_i^2},$$
(2.1)

where n_i is the number of droplets with diameter d_i and N is the total number of droplets.

Emulsion	WPI	Concentration WPI (wt%) ^a	Pressure (bar) ^b	$d_{3,2} (\mu { m m})^{ m c}$	Creaming rate (μm/ day)
Emulsion A	Native	2.7	300	1.36±0.12	80
Emulsion B	Aggregates	2.7	300	2.00±0.23	320
Emulsion C	Aggregates	9	300	1.29±0.11	14
Emulsion D	Aggregates	9	400 + 440	0.77±0.07	1

Table 2.1 - Some characteristics of the preparation and properties of the different emulsions (60 wt% aqueous phase, 40 wt% oil) prepared under different experimental conditions.

a) Protein concentration in the aqueous phase;

b) Homogenisation pressure;

c) Volume-surface average diameter;

d) Creaming rate at 1xg.

2.2.4 Determination of the interfacial tension

The equilibrium interfacial tension (γ_{OW}) between peanut oil and WPI aggregates dispersion (9 wt%) was determined using an automated drop tensiometer, ADT, (IT Concept, Longessainge, France). With this method, an oil droplet is formed in an aqueous solution, and the γ_{OW} is determined by axi-symmetric drop-shape analysis. This experiment was performed in the rising drop configuration at 25 °C. The γ_{OW} value determined after 50 min equilibration is reported.

2.2.5 Preparation of emulsion-filled acidified protein gels

Emulsion-filled acidified protein gels with different protein and oil concentrations were prepared according to the method described below. First, the 9 wt% WPI aggregates solution was diluted with RO water to the desired concentration of WPI aggregates. Next, GDL was added as a powder in the appropriate amount to induce cold gelation and to reach a final pH of around 4.8 (concentrations according to Alting *et al.* (2003a), as indicated in Table 2.2). After stirring for about 2 min, the required amount of emulsion was added. The final composition of the filled protein gels was 3% to 8.9 wt% WPI aggregates in the aqueous phase and between 0% and 35 wt% peanut oil in the total sample.

Test pieces for the compression tests were formed in 60mL syringes (diameter of 26.4 mm) coated with a thin layer of paraffin oil, while gels for small deformation rheology were formed in the measuring device. Acidification took place for at least 16 hours at 25°C. Aliquots for microstructural analysis were mixed with a dye solution and poured into special glass cells.

WPI concentration in the aqueous phase (wt %)	GDL concentration in the aqueous phase (wt %)	Concentration peanut oil based on the total sample (wt %)
3	0.22	0 - 15
5	0.36	0 - 25
7	0.49	0 - 30
8.9	0.62	0 - 35

 Table 2.2 - Composition of the emulsion-filled gels and applied GDL concentration.

2.2.6 Creaming behaviour

Emulsion-filled suspensions with the same composition as the emulsion-filled gels (see above) were prepared without the addition of GDL. The stability against creaming of the four different emulsions, the filled suspensions, and the filled gels were measured at room temperature with two methods. Following the first method, the back scattering intensity of incident laser light was measured along the height of an optical glass tube at different times, using a Turbiscan MA 2000 (Ramonville St. Agne, France). Following the second method, the transmission profiles along the height of a LUM PC rectangular synthetic cell at different times were obtained using a LUMiFuge[®] 116 at a speed of 3000 rpm (1147×g) and 1772 rpm (400×g), and using a factor light of 3.00. These profiles give a qualitative indication of the distribution of the oil droplets along the height of the tube.

2.2.7 Large deformation experiments

After acidification (~ 20 h) the gels were removed from the syringe and cut with a wire (specimen height: 25 mm). Uniaxial compression tests were performed with an Instron

universal testing system (model 5543, Instron Corp.) between two parallel plates (diameter: 150 mm) lubricated with a thin layer of paraffin oil. Fracture measurements were done at ambient temperature ($23 \pm 1^{\circ}$ C), applying compression at a crosshead velocity of 1.0 mm/s up to a linear strain of 95%. Eight replicates were measured and the mean values for fracture stress and strain were calculated. The specimen's absolute deformation is expressed as the Hencky's or true strain (ε_H) (Peleg, 1987):

$$\varepsilon_{H} = \int_{H_{o}}^{H} \frac{1}{H} dH = \ln\left(\frac{H}{H_{o}}\right)$$
(2.2)

where *Ho* is the initial specimen height and *H* is the final height after deformation. The overall stress acting on the sample during compression is expressed as the so-called true stress σ_i :

$$\sigma_t = \frac{F}{A} \tag{2.3}$$

where F is the force measured during compression and A is the cross-sectional area of the sample. The true stress accounts for the continuous change in the cross-sectional area assuming no change in cylindrical shape and constant volume during the compression.

2.2.8 Small deformation experiments

Small deformation properties of the filled gels were determined in dynamic oscillation with a Carrimed CSL^2 500 Rheometer (TA Instruments a division of Waters, Etten-Leur, The Netherlands) using a concentric cylinder geometry (inner radius 8.60 mm, outer radius 9.33 mm). Immediately after GDL addition, the samples were transferred to the rheometer and their surface was covered with a thin layer of paraffin oil to prevent evaporation. The development of the storage modulus (G') and the loss modulus (G'') during gelation was recorded during 16 hours at 25 °C at a strain of 1% and a frequency of 1 Hz. After this step, a strain sweep was recorded at increasing strain from 0.1% to 500% to verify the linear region. The loss tangent, tan δ was calculated by (van Vliet, 1995):

$$\tan \delta = \frac{G''}{G'}.$$
(2.4)

2.2.9 Confocal Laser Scanning Microscopy (CLSM)

Samples for microstructural analysis were stained with Rhodamine B (0.2% solution; 10 μ L per mL sample) to visualise the protein phase or with BODIPY® 581/591 C₁₁ (1 mg mL⁻¹ solution; 10 μ L per mL sample) to visualise the oil phase. CLSM-images were recorded on a LEICA TCS SP Confocal Laser Scanning Microscope (Leica Microsystems CMS GmbH., Manheim, Germany), equipped with an inverted microscope (model Leica DM IRBE), in the single photon mode with an Ar/Kr visible light laser. A Leica objective lens (63x/UV/1.25NA/water immersion/PL APO) was used. The excitation wavelength was set at 568 nm. The emission maxima of Rhodamine B and BODIPY® 581/591 C₁₁ are respectively 625 nm and 591 nm (Haugland, 2002; van de Velde *et al.*, 2003). Digital image files were acquired in multiple tif formats and in 1024x1024 pixel resolution.

2.2.10 Statistical analysis

Analysis of variance (ANOVA) was calculated using STATISTICA (release 7.0; StatSoft Inc., USA, 2004).

2.3 Results and Discussion

2.3.1 Characterisation of the emulsions

Both native WPI and WPI aggregates were used to prepare WPI-stabilised stock emulsions. The different stock emulsions were prepared according to the compositions and process conditions indicated in Table 2.1. To obtain emulsions with a comparable droplet size distribution, a higher concentration of WPI aggregates was required compared to native WPI (compare emulsions A to C). Emulsions with smaller droplets were prepared by applying a higher homogenisation pressure (compare emulsions C and D). Under the conditions applied, e.g. 9 wt% WPI aggregates and a droplet size around 1 μ m, the protein concentration was sufficient to cover all oil droplets. After removal of the oil droplets by centrifugation the aqueous phase still contained protein (data not shown). CLSM images showed that the emulsions were homogeneous and non-aggregated (Figure 2.1). Moreover, the emulsions were stable for more than one week as determined by the backscattering profiles measured using the Turbiscan (data not shown) and by the creaming rates obtained upon centrifugation (Lumifuge; Table 2.1). The latter has been recalculated to creaming rates under normal gravity forces. No aggregation of the emulsion droplets was observed upon storage of the stock emulsions during one week (CLSM imaging and droplet size distribution). The letter code used throughout this paper to identify the different stock emulsions is described in Table 2.1.

2.3.2 Stability and instability of emulsion-filled gels

As described in the introduction, emulsion-filled cold-set protein gels were obtained by acidification of an emulsion-filled suspension of protein aggregates. This emulsion-filled suspension was obtained by mixing an emulsion with a concentrated WPI aggregate suspension. Remarkable differences were observed upon mixing WPI aggregates with emulsions stabilised by either native WPI or WPI aggregates. The native WPI stabilised emulsions exhibited creaming of the emulsion droplets, whereas the WPI aggregate stabilised emulsions were stable.

The back scattering profiles (Turbiscan; data not shown) at different times for the emulsion-filled suspensions (before acidification) were typical for creaming of a flocculated emulsion. Over time the oil droplets moved upward due to gravity, which caused an increase in the back scattering at the top of the sample and a decrease at the bottom. After a certain time, all the oil droplets reached the upper phase and became closely packed together, forming a creamed layer. Likely, the mixture of WPI aggregates and native WPI stabilised emulsion became unstable due to the differences in size and shape between the aggregates and the oil droplets, leading to depletion-flocculation. This caused phase separation in a few hours or minutes depending on WPI and oil concentrations.

When the mixed suspensions were acidified by addition of GDL, the creaming of the system was retarded. Moreover, the mixture gelled before phase separation was complete. Acidification of the filled suspension resulted in an increase of the viscosity of the aqueous phase due to the reduction of the electrostatic repulsion between the protein aggregates. Next, the gel formed and the emulsion droplets became entrapped in the matrix. This process resulted in a heterogeneous filled gel (Figure 2.1).

The emulsion-filled gels prepared from emulsions stabilised with WPI-aggregates were stable, as shown by their back scattering profiles (Turbiscan; data not shown). The

microstructure of these filled-gels as determined by Confocal Laser Scanning Microscopy (CLSM; Figure 2.1) showed a homogeneous distribution of the emulsion droplets over the height of the sample.

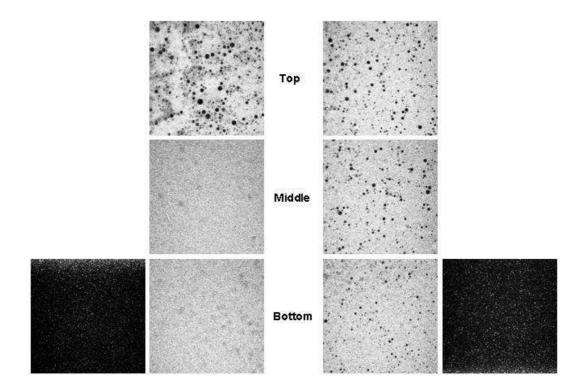


Figure 2.1 - CLSM images taken along the height of emulsion-filled gels containing emulsions droplets stabilised by native WPI (left; emulsion A) and by WPI-aggregates (right; emulsion C); images stained with Rhodamine B showing the protein; total height of the cuvet 38 mm. On the left and right side: the original emulsions stained with Bodipy C_{11} showing the oil phase. Image size: $160\mu m \times 160 \mu m$.

As the filled gels containing WPI aggregates stabilised emulsions were stable during the gelation period, the creaming rates of the emulsion droplets in the filled suspensions, i.e. before acid-induced gelation, were determined at 1147xg using the LUMiFuge. Figure 2.1 shows the creaming rate at $1 \times g$ as a function of WPI and oil concentration. The creaming rate of these filled suspensions was very low (below 0.2 mm/ day). For higher WPI / oil concentrations the creaming rate was lower, indicating that the dispersions with a higher protein and oil concentration were more stable. Thus the emulsion-filled suspension prepared from emulsions stabilised with WPI-aggregates were stable during the gelation period of 16 hours.

The decrease in creaming rate at increasing protein and oil concentrations can be related to an increase in the viscosity of the suspensions and to the repulsion between protein aggregates and protein adsorbed on the oil droplet surface. Unfortunately, the conformation of the protein aggregates absorbed on the droplet surface is not elucidated. Furthermore, the thickness of the absorbed protein layer on the droplet surface is higher in the case of aggregated proteins (d is around 60 to 80 nm) compared to native proteins (size is around 3 nm). Therefore, the density of an aggregate-stabilised emulsion droplet is higher than that of a native protein stabilised emulsion droplet. Thus in the case of aggregate stabilised emulsions the density differences is lower, which results in a lower creaming rate.

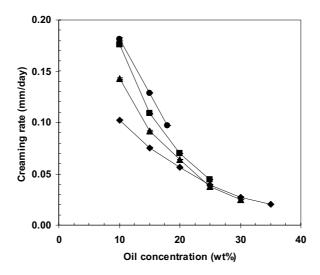


Figure 2.2 - Creaming rates at $1 \times g$ of the filled solutions prepared from emulsion stabilised by WPI-aggregates (Emulsion C) with different concentrations of WPI and oil (\bigcirc 3 wt% WPI, \blacksquare 5 wt% WPI, \blacktriangle 7 wt% WPI, \blacklozenge 8.9 wt% WPI).

2.3.3 Small deformation properties

The development of the dynamic moduli of the emulsion-filled protein gels with 5 wt% WPI and different oil fractions was followed during gelation. In Figure 2.3A results for the storage modulus (G') are shown. The initial increase in storage modulus did not differ remarkably between gels with and without oil. Over time, with decreasing pH, the storage modulus started to increase, indicating that a gel was formed. The storage modulus of the emulsion-filled gels increased faster than that of the gel without oil. After gelation, a strain sweep was recorded to verify the strain value selected for the gelation measurements.

Figure 2.3B shows that the storage modulus of the gels was not affected by the strain up to a strain of 4 to 10% depending on the oil fraction. Thus, the gelation measurements carried out at 1% strain fall within the linear region. Moreover, Figure 2.3B shows that the critical strain decreases with increasing oil content.

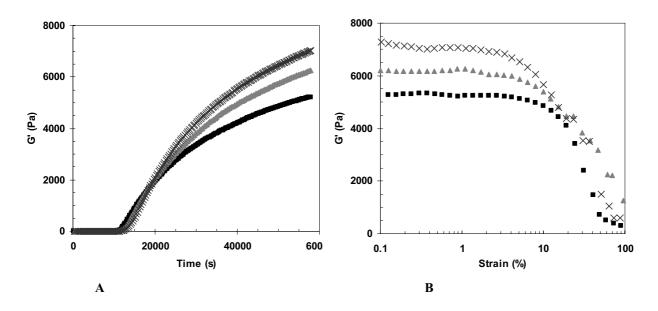


Figure 2.3 - Storage modulus (G') of the emulsion-filled gels with 5 wt% WPI aggregates for different oil concentrations (Emulsion C ($d_{32} = 1.3 \mu m$)): A: Gelation followed in time; B: Strain dependency ($\blacksquare 0$ wt% oil, $\blacktriangle 10$ wt% oil, $\times 20$ wt% oil).

The values for the dynamic moduli and the loss tangent $(\tan \delta)$ 16h after GDL addition were used to evaluate the effect of both protein and oil concentration on the properties of emulsion-filled gels. The measured storage moduli (G') are given in Figure 2.4 and Table 2.3. The final values of the loss tangent $(\tan \delta)$ were about the same for the different gels (values around 0.14), implying visco-elastic behaviour.

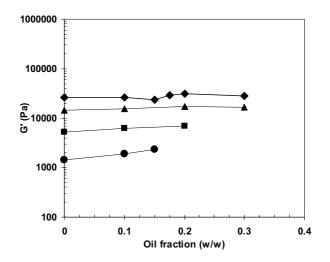


Figure 2.4 - Storage modulus (G') of emulsion-filled gels with different protein concentrations as a function of the oil fraction (Emulsion C ($d_{32} = 1.29 \ \mu m$)); (\bullet 3 wt% WPI, \blacksquare 5 wt% WPI, \blacktriangle 7 wt% WPI, \diamond 8.9 wt% WPI).

	WPI concentration (wt%)						
- Oil (wt %) _	3 5		7	8.9			
	1.3 μm	0.8 μm	1.3 μm	1.3 μm	0.8 µm	1.3 μm	
8	1.4	5.2	5.2	14.5	26.5	26.5	
10	1.9	7.4	6.3	15.3	31.0	26.2	
15	2.3					23.8	
17.5						28.7	
20		8.7	7.0	17.1	32.7	31.0	
30				16.8	36.6	28.5	

Table 2.3 - Storage modulus, G' (kPa), of the emulsion filled WPI gels.

The storage modulus (Figure 2.4) increased strongly with protein concentration. This increase can be explained by an increase in protein-protein interactions, which gave rise to a stronger network (Alting *et al.*, 2003a). At higher oil concentration the storage modulus was slightly larger. This means that the dispersed oil droplets did not act as space fillers, but helped to build up the gel matrix structure through interaction between protein molecules at the droplet surface and those in the gel matrix, so they behaved as active

fillers (van Vliet, 1988). During gel formation, the GDL added gives a pH-decrease to a pH below the isoelectric point of the WPI (5.1 for β -lactoglobulin), which leads to reduction of the electrostatic repulsion between the aggregates and thereby promotion of aggregation through non covalent interactions (Alting *et al.*, 2000). Apparently, the WPI aggregates adsorbed at the O/W interface of the droplets are able to interact with those present in the bulk. In addition, even at low pH, covalent cross links between aggregates in the protein matrix are formed via thiol-disulfide rearrangements (Alting *et al.*, 2003b). Covalent interaction may also occur between protein aggregates on the oil droplet surface and those in the gel matrix.

2.3.4 Modelling of the experimental results

The experimentally observed effect of oil fraction on the storage modulus was compared with theoretical predictions according to van der Poel's theory. This theory allows to calculate the shear modulus of composite materials containing particles non-interacting with each other. The original theory was simplified by Smith (Smith, 1975). The increase in gel modulus with filler content depends among others on the ratio (M) between the storage modulus of the filler material (G'_f) that of the gel matrix (G'_m):

$$M = \frac{G'_f}{G'_m}.$$
(2.5)

In the case of emulsion-filled gels, the storage modulus of the dispersed oil droplets depends on their size and interfacial tension according to (van Vliet, 1988):

$$G'_f = \frac{2\gamma}{R},\tag{2.6}$$

where γ is the oil/ water phase interfacial tension and *R* is the radius of the droplet.

The relation between the modulus of the composite (G') and that of the matrix (G'_m) as a function of the oil concentration can be obtained using the second-order solution of the van der Poel's formula as simplified by Smith:

$$\frac{G'}{G_m} - 1 = \frac{15(1 - \nu_m)(M - 1)\phi}{Q - (8 - 10\nu_m)(M - 1)\phi},$$
(2.7)

where ϕ is the volume fraction of oil droplets and $Q = (8-10v_m)M + 7 - 5v_m$ (v_m is the Poisson ratio of the matrix, which was taken to be equal to 0.5).

Equation 7 was used to calculate the ratio between the storage modulus of the filled gels (G') and the storage modulus of the matrix gel (G'_{matrix}) as a function of oil and protein concentration. Figure 2.5 shows the results of these calculations together with the experimental results. The oil/ water phase (9 wt% WPI aggregates at pH 6.7) interfacial tension was measured using an automated drop tensiometer. Values between 1 mN.m⁻¹ and 10 mN.m⁻¹ were obtained. These values are very low for a system consisting of an oil and a protein solution. They may be caused by the possible presence of mono- and diglycerides in the peanut oil, that was used without previous purification. In order to calculate the modulus of the oil droplets, a value of 6 mN.m⁻¹ was used.

The van der Poel's theory correctly predicted the effect of the stiffness of the protein matrix on the stiffness of the emulsion-filled gels. As shown in Figure 2.5, the increase in storage modulus with oil concentration was more pronounced for lower protein concentrations, i.e. matrices with a lower stiffness. Moreover, for the emulsion-filled gel containing 9 wt% WPI in the water phase a slight decrease in the modulus was observed. Figure 2.6 shows the storage modulus of the protein matrix as a function of the protein concentration in the aqueous phase. From this curve it was calculated that at a protein concentration of 7.8 wt% the moduli G'_{matrix} and G'_{filler} were equal. G'_{filler} of emulsion C was calculated to be 18.6 kPa. This value agrees well with the results for the filled gels containing 7 wt% WPI aggregates in the aqueous phase (Figure 2.5). Thus, the ratio between the moduli of the matrix (G'_{matrix}) and filler (G'_{filler}) is an important parameter determining the properties of emulsion-filled gels.

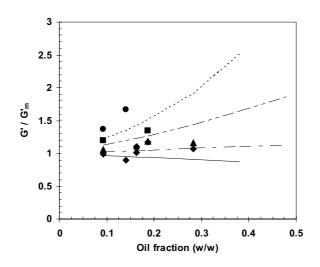


Figure 2.5 - Influence of oil fraction on the ratio (G' / G_m') for emulsion-filled gels with different protein concentrations in the aqueous phase (Emulsion C $(d_{32} = 1.3 \ \mu\text{m})$). The points are experimental results and the lines are calculated results from van der Poel's theory ($\odot \cdots 3 \ \text{wt\%}$ WPI, $\blacksquare \cdots 5 \ \text{wt\%}$ WPI, $\blacktriangle \cdots 7 \ \text{wt\%}$ WPI, $\blacklozenge \cdots 8.9 \ \text{wt\%}$ WPI).

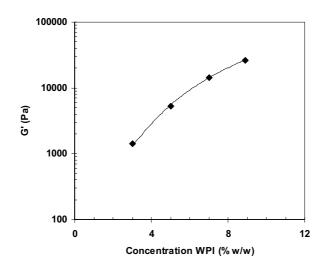


Figure 2.6 - Storage modulus (G') of the protein matrix plotted as a function of the concentration of WPI aggregates in the aqueous phase.

As the size of the emulsion droplets is directly related to their stiffness, the effect of the droplet size was also investigated. As can be derived from equation 6, smaller emulsion droplets are stiffer and thus should result in a more pronounced increase in the stiffness of the composite. Figure 2.7 shows the storage moduli of two emulsion-filled gels with different droplet sizes. A reduction of the droplet size from 1.3 μ m to 0.8 μ m had only a slight effect on the observed increase in the storage modulus of the 5 wt% and 9 wt% WPI gel. As predicted, the gels with smaller oil droplets were slightly stiffer compared to those with the bigger droplets.

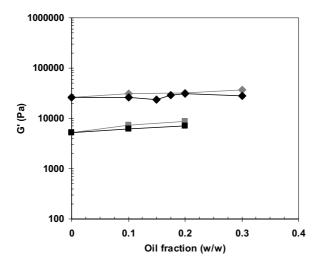


Figure 2.7 - Storage modulus (G') of emulsion-filled gels as function of the oil fraction for different protein concentrations and droplet sizes (Emulsions C and D) (Black symbols: $d_{3,2} = 1.29 \mu m$, Grey symbols: $d_{3,2} = 0.77 \mu m$, \blacksquare 5 wt% WPI, \blacklozenge 8.9 wt% WPI).

Concluding, the van der Poel's theory correctly predicted the effects of both the matrix stiffness and droplet properties on the stiffness of the emulsion-filled gels. However, Figure 2.5 also shows that for all protein and oil concentrations studied, the experimental values of the ratio (G' / G_m ') were slightly higher than predicted by the van der Poel's theory. This small discrepancy between the experimental results and theory may be caused by several factors such as errors in the calculated droplet stiffness. The estimate of the interfacial tension used for this calculation may have played an important role in this respect.

2.3.5 Large deformation properties

2.3.5.1 Effect of homogenisation on WPI gels

In the case of emulsions stabilised with WPI-aggregates, the aggregates in the stock emulsion will take part in the protein matrix forming the filled-gel. As these aggregates are homogenised during the preparation of the emulsion, the effect of this homogenisation step on the fracture properties of WPI gels was studied. WPI-aggregate solutions were homogenised under the conditions used for the emulsion preparation and subsequently used to prepare emulsion-free protein gels. The fracture properties of the gels prepared from homogenised aggregates were compared with of those of the untreated aggregates (Table 2.4). An analysis of variance did not show any statistical differences between the reference gels and the gels prepared from homogenised aggregates. Therefore, we concluded that the homogenisation step did not affect the properties of the aggregates used to stabilise the emulsions.

Gel type	Property	Mean value reference	Mean value homogenised	p-value
WPI 9-3	Modulus (kPa)	3.4	3.2	0.361
	Fracture stress (kPa)	3.7	3.4	0.119
	True fracture strain (-)	1.10	1.05	0.112
WPI 9-5	Modulus (kPa)	9.5	9.3	0.693
	Fracture stress (kPa)	8.6	7.4	0.419
	True fracture strain (-)	1.29	1.17	0.158
WPI 9-7	Modulus (kPa)	23.7	23.5	0.831
	Fracture stress (kPa)	17.7	19.3	0.556
	True fracture strain (-)	1.30	1.57	0.065

Table 2.4 - Fracture properties of WPI gels.

2.3.5.2 Filled gels

Fracture stress and strain, which are a measure of the strength of the material and its deformability before fracture occurs, are important quality characteristics of solid and solid-like food products (Kim *et al.*, 2001). Therefore, the fracture properties of the emulsion-filled protein gels with different protein and oil concentrations were studied for two droplet sizes ($d_{32} = 1.3 \mu m$ and $d_{32} = 0.8 \mu m$; see Table 2.2) by uniaxial compression. A crosshead speed of 1 mm/s was selected to be relevant for compression speeds that occur in the mouth during palating of semi-solid foods. A detailed study on the effect of compression speed on the fracture properties of emulsion filled gels will be described in chapter 5 (Sala et al., to be published). Figure 2.8 shows the fracture stress and strain of the emulsion-filled protein gels as a function of the oil fraction for different protein concentrations. The observed increase in the true stress with increasing protein concentration is in agreement with the published data for the cold gelation of globular proteins (Alting *et al.*, 2003a).

In general, Figure 2.8 shows a slight effect of the addition of emulsion droplets on the fracture properties of the emulsion-filled gels. In the case of the highest protein concentrations (7% and 8.9% WPI), a small increase in the fracture stress is observed with increasing oil concentration. On the other hand, at low protein concentrations (3% and 5% WPI) the fracture stress slightly decreases with increasing oil concentration. The fracture strain decreases with the increase of the oil concentration, so that the gels with higher oil content are somewhat more brittle. This is in agreement with the observed decrease in critical strain as measured by small deformation measurements (Figure 2.3B). Although the effect of the oil concentration on fracture properties was small, the differences were statistically significant. Moreover, Figure 2.8 shows that the size of the oil droplets did not have a large effect on fracture properties.

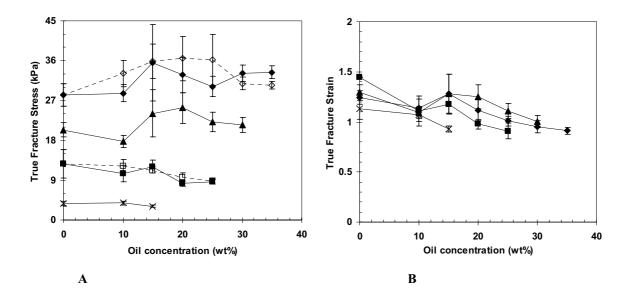


Figure 2.8 - Effect of oil droplet size and WPI concentration on fracture properties of emulsionfilled protein gels as a function of oil concentration (Emulsions C and D): A: True fracture stress; B: True fracture strain (\times 3 wt% WPI, $\blacksquare \Box$ 5 wt% WPI, \blacktriangle 7 wt% WPI, \blacklozenge 8.9 wt% WPI). $d_{32} =$ 1.3µm (closed symbols) and $d_{32} = 0.8$ µm (open symbols). Error bars represent the standard deviation of the 8 replicates.

2.4 Conclusions

Stable and homogeneous emulsion-filled gels with different protein and oil concentrations can prepared by cold gelation of emulsions obtained by mixing suspensions of soluble WPI aggregates with 40 wt% oil-in-water stock emulsions stabilised with the same WPI aggregates. With increasing oil concentration the fracture stress of these gels increases slightly, whereas the fracture strain slightly decreases. The experimental results for the storage modulus (G') after 16 hours of acidification are in good agreement with predictions for the influence of oil and protein concentration on the stiffness of filled gel according to the van der Poel's theory for calculating the shear modulus of particulate composites.

2.5 Acknowledgements

Saskia de Jong-Kok (WCFS/NIZO food research) is acknowledged for her help with the rheological experiments and helpful discussions. Jan Benjamins (WCFS) is acknowledged for performing the interfacial tension measurements at Wageningen University.

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2.7 Appendix

Van der Poel developed a formula to estimate the shear modulus of a particulate composite (van der Poel, 1958), which was simplified by Smith (Smith, 1975). According to this theory, the storage modulus of the filled gels can be calculated using the following equation:

$$\alpha X^2 + \beta X + \delta = 0, \qquad (2.A1)$$

where α , β and δ are given by:

$$\alpha = \left[8P - \phi^{7/3}S\right]\left[Q - 3(M-1)\phi\right] - 126P(M-1)\phi\left(1 - \phi^{2/3}\right)^2$$
(2.A2A)

$$\beta = 17.5P[(3M+4.5) - 3(M-1)\phi] - 7.5[8P - S\phi^{7/3}](M-1)\phi \qquad (2.A2B)$$

$$\delta = -131.25P(M-1)\phi$$
 (2.A2C)

where ϕ is the volume fraction of oil droplets, P = 9.5M + 8, S = 166.25M - 9.5P and $Q = (8-10v_m)M + 7 - 5v_m$ (v_m is the Poisson ratio which was taken to be equal to 0.5) (Chen *et al.*, 1998). When this equation is solved for X the positive root is equal to (G' / G_m ') - 1.)

The second-order solution can be written as (Smith, 1975):

$$\frac{G'}{G'_m} - 1 = \frac{15(1 - v_m)(M - 1)\phi}{Q - (8 - 10v_m)(M - 1)\phi}.$$
(2.A3)

Chapter 3

Effect of droplet-matrix interactions on large deformation properties of emulsion-filled gels

G. Sala, G.A. van Aken, M. Cohen Stuart, F. van de Velde (2007). Effect of droplet-matrix interactions on large deformation properties of emulsion-filled gels, *Journal of Texture Studies*, 38, 511-535.

Abstract

The aim of this chapter was to identify the effect of droplet-matrix interactions on the large deformation properties of emulsion-filled gels. A study was carried out on the behaviour in compression of gelatine, whey protein isolate (WPI) and κ -carrageenan gels containing bound and unbound emulsion droplets. For gelatine gels, emulsions stabilised with WPI and lysozyme induced an increase of the modulus, while emulsions stabilised with Tween induced a decrease of the modulus. It was concluded that in the first two cases the oil droplets were bound to the gel matrix and that in the latter case the oil droplets were unbound. For WPI gels, emulsions stabilised with WPI aggregates, lysozyme and a low concentration of Tween induced an increase of the modulus (bound droplets). The modulus variations observed for κ -carrageenan gels were mainly related to interactions between κ -carrageenan and the emulsifying agent present in the aqueous phase. Theories based on the effect of the oil content on modulus satisfactorily fitted the trend of the experimental results, both for bound and unbound droplets. The fracture strain decreased with increasing oil concentration for droplets bound to the matrix and remained constant for unbound droplets. The fracture stress was unaffected by bound droplets and decreased in the case of unbound droplets. Theories describing the effect of filler content on fracture strain and stress failed to predict the experimental results. This was attributed to the small size of the oil droplets of the emulsions used in this study, which was similar to the size of the inherent defects present in the gel network.

3.1 Introduction

3.1.1 Filled gels

The rheological properties of emulsion-filled gels systems depend on the properties of both the gel matrix and the oil droplets, the oil droplet concentration and the nature of the droplet-matrix interactions (Tolstoguzov & Braudo, 1983; van Vliet, 1988). Oil droplets entrapped in a gel matrix behave as particles. Typically, a protein-stabilised oil droplet with a diameter of 1 µm has a shear modulus of about 40 kPa (van Vliet 1988). Depending on their effect on gel modulus, filler particles were classified as either active or inactive (Ring & Stainsby, 1982). Active fillers are bound to the gel matrix and, depending on the ratio between their modulus and that of the matrix, they either increase or decrease the gel modulus. Inactive fillers have little chemical or physical affinity to the molecules forming the gel matrix and always decrease the gel modulus. This terminology can be confusing. As a matter of fact, when the modulus of the fillers is smaller than that of the matrix both bound and unbound fillers have the same effect on gel modulus (i.e. the gel modulus decreases at increasing filler concentration). Therefore, in this study the terms bound and unbound will be used instead of active and inactive.

The interactions between filler and gel matrix depend on the surface properties of the filler particles, in particular the nature of the stabilising agent (Dickinson & Chen, 1999). This aspect has been studied in different kinds of food gels matrices.

Most data available in literature on emulsion-filled gels concern heat-set whey protein gels and acid-induced skimmed milk/casein gels. Both small and large deformation properties of these gels have been studied. In heat-set whey protein gels, oil droplets stabilised by whey protein were found to behave as active fillers, whereas oil droplets stabilised by a non-ionic surfactant (polyoxyethylene sorbitan monolaurate, Tween 20) weakened the gel (Dickinson, Hong & Yamamoto, 1996; Yang, Chen & Chang, 1998; Chen & Dickinson, 1999; Dickinson et al., 1999; Chen, Dickinson, Langton & Hermansson, 2000). Compression measurements on heat-set whey protein gels showed similar phenomena (McClements, 1993). For heat-induced whey protein gels (Langley, 1989) the introduction of glass spheres resulted in different behaviour, depending on the surface properties of the glass. Spheres with a hydrophilic surface induced a larger increase of the fracture stress than hydrophobic spheres. Furthermore, gels with hydrophobic particles fractured adjacent to the sphere surface, indicating weak interaction

between the sphere and the gel matrix. For gels with hydrophilic spheres, fracture occurred within the gel matrix. This showed that the spheres were strongly bound to the gel matrix. In acid-induced skimmed milk/casein gels emulsions stabilised by caseinate, whey protein or skimmed milk powder behaved as active fillers, increasing modulus (van Vliet, 1988; Xiong, Aguilera & Kinsella, 1991a; Xiong & Kinsella, 1991b; Chen, Dickinson & Edwards, 1999) and compression stress (Aguilera & Kinsella, 1991; Xiong et al., 1991a; Xiong et al., 1991b) as compared to gels without emulsions. Washed natural milk fat globules decreased the modulus of these gels (van Vliet, 1988), whilst emulsions stabilised by Tween 80 only slightly increased modulus and compressive stress (Xiong et al., 1991b).

Fewer studies are available with regard to other gel matrices. In transglutaminaseinduced soy protein gels (Matsumura, Kang, Sakamoto, Motoki & Mori, 1993) and heatset soy protein gels (Kim, 2001), oil droplets stabilised with the same protein behaved as active filler. In agar gels containing emulsion droplets stabilised by fatty acids of polyglycerolesters (Kim, 1996) an increase of the droplet size and concentration resulted in a decrease of the fracture stress and strain measured in compression tests.

Literature data on the rheological properties of emulsion-filled gels mostly analyse the effect of oil droplets on the properties of a particular kind of gel, but do not offer much consistent insight in the underlying mechanisms. In this chapter, we fill this gap by studying the effects of the interactions between oil droplets and gel matrix on the large deformation properties of both particle and polymer gels. The systems studied consisted of acid-induced cold-set WPI, gelatine, and κ -carrageenan gels to which emulsions stabilised with native WPI, WPI aggregates, lysozyme and Tween were added. This approach allowed to systematically vary the interactions between oil droplets and the gel matrix. Moreover, for WPI and gelatine gels it was possible to control the aggregation of the oil droplets. Therefore, the effect of oil droplet aggregation on large deformation properties could also be studied for samples with constant composition. The validity of theories describing the effect of filler content on elastic modulus, fracture strain and fracture stress of composite materials was tested by comparing experimental data and theoretical predictions.

3.1.2 Theories predicting the effect of filler content on modulus

Most studies published in literature on emulsion-filled gels describe the effect of oil droplets on storage modulus as determined by small deformations rheological measurements. For the prediction of the experimental results, both the van der Poel (van der Poel, 1958; Smith, 1974, 1975) and the Kerner (Kerner, 1956; Lipatov, 1977) theories have been applied (Brownsey, Ellis, Ridout & Ring, 1987; van Vliet, 1988). These theories were chosen because of their wide applicability and the good prediction of experimental data for polymer dispersions containing filler particles. Both theories assume the matrix to be completely adherent to the fillers (i.e. the fillers to behave as bound fillers) and the filler particles to be non-interacting with each other and homogeneously distributed through the gel network. The similarity between the two theories can be seen in Figure 3.1.

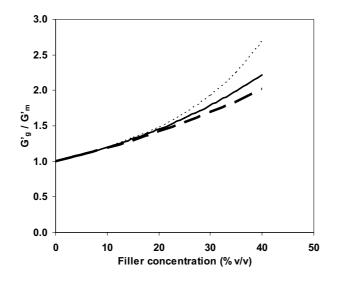


Figure 3.1 – Effect of filler concentration on modulus as calculated according to the van der Poel theory (continuous line), the Kerner theory (broken bold line) and the Kerner theory corrected for the maximum packing of the fillers (dotted thin line). (G'_g : modulus of the filled gel; G'_m :modulus of the matrix; ratio between filler and matrix modulus: 7.5).

The theories predict the modulus of filled gels at a given filler concentration (volume fraction), for given moduli of gel matrix (G'_m) and filler particles (G'_f) . In the case of bound fillers, three different situations can be described:

- $G'_f > G'_m$: under deformation, the filler particles deform less than the matrix; as a consequence, the modulus of the filled gel is higher than that of the matrix;

- G'_f = G'_m: under deformation, the filler particles deform equally to the matrix; as a consequence, the modulus of the filled gel is equal to that of the matrix and independent of the filler concentration;
- $G'_f < G'_m$: under deformation, the filler particles deform more than the matrix; as a consequence, the modulus of the filled gel is lower than that of the matrix.

Following van Vliet (1988), the modulus of the oil droplets can be estimated by the Laplace pressure, $2\gamma/R$, where γ is the interfacial tension and R the droplet radius. Van Vliet proposed a modification of the van der Poel theory for the calculation of the modulus of gels containing unbound oil droplets by setting the effective filler modulus to zero. In Figure 3.2 the effect of filler concentration on the modulus of filled gels is shown for the different situations as described above.

Oil droplet aggregation is usually held responsible for deviations between the experimental data and the theories. This was reported for acid milk gels (van Vliet, 1988) and for heat-set whey protein gels (Chen & Dickinson, 1998) with emulsion droplets bound to the gel matrix. In both cases, the effect of oil droplet aggregation on the modulus was ascribed to a higher effective volume fraction of the fillers as compared to non-aggregated oil droplets.

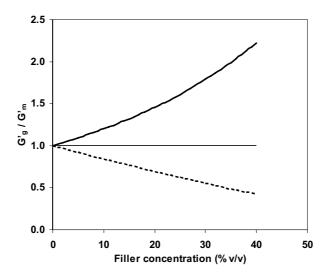


Figure 3.2 – Effect of filler concentration on modulus as calculated according to the van der Poel theory (G'_g : modulus of the filled gel; G'_m : modulus of the matrix; $G'_f = 7.5 G'_m$: bold line; $G'_f = G'_m$: thin line; $G'_f < G'_m$: dotted line).

3.1.3 Theories predicting the effect of filler content on fracture properties

The theory for filled polymers of Nielsen (1966) describes the effect of filler particles bound to the polymer matrix on fracture strain. The fillers are assumed to be rigid, non-deformable particles, while the polymer matrix is assumed to be deformable. Shear effects around the filler, triaxial stresses in the polymer and effects due to the Poisson ratio are neglected. Furthermore, the size of the fillers is not taken into consideration. The theory is developed for tensile measurements and assumes the polymer to break at the same elongation in the filled system as the bulk unfilled polymer does. Under these conditions, the actual (fracture) strain in the matrix is larger than the nominal strain (i.e. the strain applied to the sample) by a factor which depends on the filler volume. Therefore, the nominal fracture strain will decrease with increasing filler phase volume as shown in Figure 3.3. By combining his own theory on the effect of fillers on fracture stress with the theory of Sato and Furukawa on the effect on modulus, Nielsen described also the effect of fillers on the fracture strain in the case of no adhesion between filler and polymer (unbound droplets) (Nielsen, 1966). The theory of Nielsen on fracture stress contains a not well defined 'stress concentration function'(S), which should be estimated. This stress concentration function can have a maximum value of 1 when there is no concentration and is usually expected to have a value of the order of 0.5. Unfortunately, Nielsen did not describe the criteria necessary to estimate S. This introduces a subjective element that makes the theory unsuitable for predictive purposes. The curve reported in Figure 3.3 for the case of unbound droplets was calculated assuming a stress concentration function of 1.

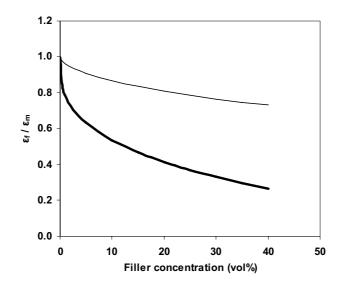


Figure 3.3– Effect of filler concentration on fracture strain as calculated according to the Nielsen theory for perfect adhesion (thick line) and no adhesion (thin line) between filler and polymer phase ($\varepsilon_{\rm f}$: fracture strain of the filled gel; $\varepsilon_{\rm m}$: fracture strain of the gel matrix).

Ross-Murphy and Todd (1983) proposed a theory to describe the effect of filler concentration on fracture stress. This theory is a combination of the Nielsen theory on fracture strain and the Landel theory on modulus. Like the Nielsen theory on fracture strain, it assumes the matrix to be deformable and the filler particles to be completely non-deformable and perfectly adherent to the matrix (bound droplets). Furthermore, this theory assumes the modulus to be constant at all deformations (strain-hardening is not taken into account) and always to increase with increasing filler concentration. Therefore, the fracture stress can either increase or decrease with increasing phase volume of the filler, depending on the relative effect of the filler on modulus and strain. This theory was used to explain the effect of glass beads in gelatine gels. The effects of particle size on fracture stress depended upon volume fraction. At low volume fraction small effects were observed. At increasing volume fraction, samples containing larger particles showed lower fracture stress.

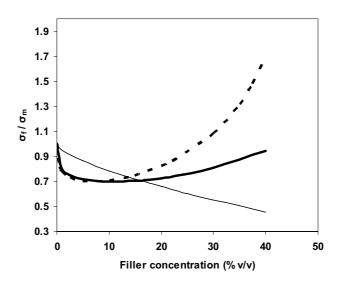


Figure 3.4 – Effect of filler concentration on fracture stress as calculated according to the Ross-Murphy and Todd theory (continuous bold line) and the Langley and Green theory (broken line) for the case of perfect adhesion between filler and polymer phase and the Nielsen theory (continuous thin line) for the case of no adhesion (σ_f : fracture stress of the filled gel; σ_m : fracture stress of the gel matrix).

Langley and Green (1989), in a study on whey protein gels filled with glass beads and emulsion droplets, proposed a modification of the Ross-Murphy and Todd formula which takes into account the maximum packing volume of the filler. Furthermore, they modified the theory to account for the variation of the maximum packing of the glass beads due to protein adsorption, in this way introducing the effect of the filler particle size. Figure 3.4 shows a comparison between the Ross-Murphy and Todd and the Langley and Green theories. In the same figure, a curve describing the effect of filler on fracture stress following the theory of Nielsen for fillers unbound to the matrix is shown. For this curve, a stress concentration function of 1 was assumed.

3.2 Materials and methods

3.2.1 Materials

Powdered whey protein isolate (WPI, BiproTM) was obtained from Davisco International Inc. (La Sueur, MN, USA). Kappa-carrageenan was kindly donated by CP Kelco (Lille Skensved, Denmark). The κ-carrageenan sample consisted of 93% mol κ-units and 7% mol 1-units, as determined by NMR spectrometry (van de Velde, Pereira & Rollema, 2004). The counter-ions present in the product consisted of a mixture of potassium, sodium and calcium (de Jong & van de Velde, 2007). Porcine skin gelatine PBG 07 (bloom 280, isoelectric point 8-9) was kindly provided by PB gelatines (Vilvoorde, Belgium). Tween 20 (Polyoxyethylene sorbitan monolaurate, in the text referred to as Tween) and lysozyme were obtained from Sigma (Sigma-Aldrich Chemie BV, Zwijndrecht, The Netherlands). Dimodan HR (distilled saturated monoglycerides) was obtained from Danisco International Inc. (Aarde, Denmark). Medium Chain Triglycerides (MCT) MIGLYOL 812N oil was purchased from Internatio BN (Mechelen, Belgium). Potassium chloride (p.a.) was obtained from Merck (Darmstadt, Germany). Glucono-δlactone (GDL) was kindly donated by Purac (Gorinchem, The Netherlands). All materials were used without further purification. All solutions were prepared with demineralised water.

3.2.2 Sample preparation

3.2.2.1 Emulsions

WPI solutions were prepared by adding the weighed protein to the required amount of water. Subsequently, the solutions were gently stirred for 2 hours. Stock emulsions, consisting of 40 wt% MCT oil and 60 wt% aqueous phase containing 1 wt% WPI, were prepared by pre-homogenising the ingredients using an Ultra Turrax (Polytron, Kinematica AG, Lucerne, Switzerland) homogeniser. Pre-emulsions were further processed using a laboratory homogeniser (Ariete, Model NS1001L 2K – Panda 2K, Niro Soavi S.p.A, Parma, Italy). KCl was added to the emulsion used for the preparation of κ -carrageenan, up to a concentration of 10 mM in the aqueous phase.

The same procedure was used for the preparation of the emulsion stabilised with Tween and lysozyme. The concentrations of emulsifying agent in the aqueous phase were 0.5 and 2 wt% for Tween and 2 wt% for lysozyme.

Emulsions stabilised with WPI aggregates were prepared as described above, but using a 3 wt% WPI aggregates dispersion as continuous phase. This dispersion was prepared by heating a 9 wt% WPI solution at 68.5°C for 2 hours and subsequent cooling to room temperature with tap water and diluting to 3 wt%.

Emulsions stabilised with WPI aggregates in the water phase and Dimodan HR in the oil phase were prepared by dissolving 1 wt% Dimodan in the oil at 80°C for 1 hour. After cooling the oil to 50°C and heating a 3 wt% WPI aggregates dispersion to the same temperature, the emulsion was prepared by Ultra Turrax pre-homogenisation followed by a homogenisation step in the homogenizer, which was preheated at 50°C.

The droplet size distribution of the obtained emulsions was measured using a Malvern Mastersizer 2000 (Malvern Instruments Ltd., Malvern, UK). The volume-surface average or Sauter diameter $(d_{3,2})$ of the droplets of the emulsions used for the preparation of the filled gels is reported in Table 3.1.

Emulsifying agent in the water phase	Emulsifying agent in the oil phase	d _{3,2} (μm)
1 wt% WPI	<u> </u>	1.13±0.05
3 wt% WPI aggr.	-	1.10±0.05
3 wt% WPI aggr.	1 wt% Dimodan HR	0.95±0.05
2 wt% Lysozyme	-	1.31±0.05
0.5 wt% Tween	-	1.40±0.05
2 wt% Tween	-	1.26±0.05

Table 3.1 - Volume-surface average diameter (Sauter diameter) of the emulsions used for the preparation of the filled gels.

3.2.2.2 Gels

WPI (3 wt%) and gelatine (4 wt%) gels were prepared in demineralised water. Kappacarrageenan (0.75 wt%) gels were prepared in a 10 mM KCl solution. Samples were prepared without emulsion and with different oil concentrations (5, 10, 20 wt%). In all samples the concentration of the gelling agent in the aqueous phase was kept constant.

The gelation of the WPI gels was induced by addition of GDL (0.22 wt% in the case of a WPI aggregates dispersion with a concentration of 3 wt%) to the WPI dispersion and to the WPI dispersion/emulsion mix and incubation at 25°C for 17 hours. The WPI dispersion was prepared as described above.

For the carrageenan and gelatine gels, the gelling agent was allowed to hydrate for 2 hours under gentle stirring at room temperature. The samples were subsequently dissolved by heating at 80°C for 30 minutes and cooled to 45°C. Prior to emulsion addition, the emulsion was heated to 45°C. After mixing, the samples were allowed to gel at room temperatures in 60 ml plastic syringes (internal diameter 26.4 mm) coated with a thin paraffin oil film. By mixing the emulsion with the gelatine solution at 20°C, gelatine samples with non-aggregated emulsion droplets were prepared.

In order to distinguish the effect of oil droplets on gel properties from that of the residual emulsifying agent present in the aqueous phase of the emulsions added to the gels, emulsion-free samples were prepared containing the same amount of emulsifying agents as present in the filled gels with 20 wt% emulsion.

3.2.3 pH measurement

The pH of the gels was measured with a Knick Portamess 911 pH pH-meter (Knick Elektronische Messgeräte, GmbH & Co. KG, Berlin, Germany), by inserting the electrode directly into the gel and waiting until a constant value was reached. The measurement was performed at room temperature. The experimental error was within 0.05 pH units.

3.2.4 Large deformation experiments

Uni-axial compression tests were performed on gel pieces of 25 mm height with an Instron universal testing machine (Model 5543, Instron International Ldt., Edegem , Belgium) equipped with a plate-plate geometry. In order to prevent friction between the 58

plates and the samples, the plates were lubricated with a thin layer of paraffin oil. The measurements were performed at a constant deformation speed of 1 mm/s and up to a compression strain of 80%.

3.2.5 Confocal Laser Scanning Microscopy (CLSM)

Samples for microstructural analyses were stained with Rhodamine B (0.2 wt% solution; 10 μ L per mL sample) to visualise the protein phase. CLSM-images were recorded on a LEICA TCS SP Confocal Laser Scanning Microscope (Leica Microsystems CMS GmbH., Manheim, Germany), equipped with an inverted microscope (model Leica DM IRBE), used in the single photon mode with an Ar/Kr visible light laser. A Leica objective lens (63x/UV/1.25NA/water immersion/PL APO) was used. The excitation wavelength was set at 568 nm. The emission maximum of Rhodamine B is at 625 nm. Digital image files were acquired in tagged image file format and at 1024x1024 pixel resolution.

3.3 Results

3.3.1 Effect of emulsifying agents on large deformation properties of the gel matrix

The modulus and the fracture properties of gel samples without emulsion but containing the same amount of emulsifying agents as that present in filled gels with 20 wt% emulsion were compared to those of gels without emulsifying agents (Table 3.2).

Lysozyme was the emulsifying agent with the largest effect on the gel properties. The different effects of lysozyme on the three gels can be explained by the different molecular interactions of this ingredient with the gelling agents. For gelatine gels, at the measured pH (Table 3.3) both gelatine (isoelectric point 8-9) and lysozyme (isoelectric point \sim 10) display a net positive charge. Consequently, electrostatic repulsion is expected between gelatine and lysozyme, which would disturb the formation of the gelatine gel network, explaining the observed decrease in modulus and fracture stress. For WPI gels, lysozyme induced a decrease of both fracture strain and stress. At the pH of these gels (Table 3.3), which was slightly lower than the isoelectric point of whey protein (\sim 5), both proteins have a positive net charge and would repel each other. This could explain the observed weakening of the gel.

Gel type	Emulsifying agent	Modulus (kPa)	Fracture stress (kPa)	Fracture strain (mm/mm)
Gelatin	No emulsifier	3.2 ± 0.2	10.9 ± 2.5	1.28 ± 0.12
	WPI	3.2 ± 0.2	11.3 ± 1.1	1.25 ± 0.03
	Lysozyme	2.7 ± 0.1	7.9 ± 0.5	1.25 ± 0.02
	2% Tween	3.1 ± 0.2	8.3 ± 0.9	1.18 ± 0.07
WPI	No emulsifier	5.2 ± 0.1	5.7 ± 1.2	1.09 ± 0.05
	Lysozyme	5.7 ± 0.6	3.4 ± 0.5	$0.72{\pm}0.11$
	0.5% Tween	4.5 ± 0.4	6.7 ± 0.7	1.23 ± 0.08
к-carrageenan	No emulsifier	5.2 ± 0.5	9.5 ± 1.2	0.56 ± 0.03
	WPI	5.2 ± 0.4	9.1 ± 1.6	0.59 ± 0.06
	WPI aggreg.	3.5 ± 0.5	7.7 ± 1.3	0.61 ± 0.05
	Lysozyme	25.4 ± 0.9	8.3 ± 0.3	0.44 ± 0.05
	2% Tween	5.2 ± 0.6	7.5 ± 1.4	0.57 ± 0.03

Table 3.2 – Effect of emulsifying agents (at the same concentration as that present in the gel with 20 wt% emulsion) on modulus and fracture properties.

When adding a lysozyme solution to a solution of κ -carrageenan, fibrous structures were formed instantaneously within the gel network. These structures were probably similar to the coacervates formed by lysozyme and κ -carrageenan as reported by Yang et al. (1998). The presence of these fibres led to a strengthening of the gel matrix, which was responsible for an increase in modulus of the filled gels.

Regarding κ -carrageenan gels, WPI aggregates affected the gel modulus (Table 3.2), but the fracture properties remained unchanged. At the pH of the gels (Table 3.3), κ -carrageenan is negatively charged. Therefore, WPI aggregates, which are negatively charged spherical particles with a diameter around 50-60 nm, are not incorporated in the three-dimensional structure of the gel.

In general, the emulsifying agents appeared to have only a limited direct effect on the rheological properties of the gels. Only for lysozyme a clear effect on the properties of all gelled matrices was observed. This was taken into account when interpreting the effect of lysozyme-stabilised emulsions on large deformation properties.

				Emulsif	ying agent		
Gel type	Oil content (wt%)	WPI	WPI aggr.	WPI aggr.+ Dimodan	Lysozyme	0.5 wt% Tween	2 wt% Tween
Gelatin	0	5.37	-	-	5.57	5.42	5.43
	5	5.43	-	-	5.43	5.50	5.42
	10	5.61	-	-	5.47	5.48	5.43
	20	5.73	-	-	5.39	5.48	5.44
WPI	0	-	4.95	4.95	4.97	4.95	-
	5	-	4.93	4.92	4.92	4.91	-
	10	-	4.92	4.90	4.98	4.93	-
	20	-	4.92	4.91	4.84	4.93	-
ĸ-carrageenan	0	8.42	8.50	-	8.73	8.81	8.81
	5	8.10	8.01	-	8.65	8.90	8.77
	10	7.95	7.73	-	8.38	8.93	8.74
	20	7.62	7.56	-	7.65	8.77	8.63

Table 3.3 – pH of the gels samples (the experimental error is 0.05 pH units).

-: not studied

3.3.2 Effect of oil droplets on gel modulus

The Young's modulus of gels containing different emulsions is shown in Figure 3.5 as a function of the oil concentration. This figure also shows the curves representing the data as predicted by the van der Poel theory (for the filler concentrations studied, the van der Poel and the Kerner theories give comparable results) for bound fillers with a diameter comparable to that of the added emulsion droplets and for unbound fillers. For the calculations of van der Poel theory, the shear modulus of the gel matrix is normally used. The estimation of the modulus of the oil droplets (bound droplets) by the Laplace pressure as suggested by van Vliet provides a value of shear modulus (van Vliet 1988). With the large deformation measurements carried out in this work, the Young's modulus of the gels was obtained. Therefore, the shear modulus of the oil droplets as calculated following van Vliet (a value of 20 mM/m was assumed for the surface tension between oil and water phase) was multiplied by a factor 3 in order to obtain an estimate of their Young's modulus (assuming a Poisson ratio of 0.5, the Young's modulus is 3 times larger than the shear modulus).

By using various emulsifying agents, a variation in gel modulus was observed, especially for gelatine gels (Figure 3.5A). In gelatine and WPI gels the emulsion droplets were mainly bound to the gel matrix, inducing an increase in gel modulus. This occurred also in cases where no interactions between oil droplets and gel matrix were expected, like in samples containing lysozyme-stabilised emulsions. In gelatine gels, emulsion droplets stabilised with 2 wt% Tween were unbound to the matrix and induced a decrease of the gel modulus. In WPI gels, emulsions stabilised with 2 wt% Tween caused extensive phase separation during gel formation, which made it impossible to produce suitable samples. For κ -carrageenan gels, most emulsions induced a slight decrease of the gel modulus, indicating that the oil droplets were not bound to the matrix. The increase of the modulus for samples containing lysozyme-stabilised emulsions could entirely be ascribed to the effect of the fibrous structures formed by κ -carrageenan and the lysozyme present in the water phase of the emulsion (Table 3.2, Figure 3.5C).

The deviations between the experimental results and the van der Poel theory as observed in the present work were similar to those previously reported by other authors for both bound and unbound fillers. Because of the similarity between the van der Poel and the Kerner theories in the oil content range considered, this holds also for the Kerner theory. The discrepancy between experimental results and theory was mostly within the standard deviation of the experimental data.

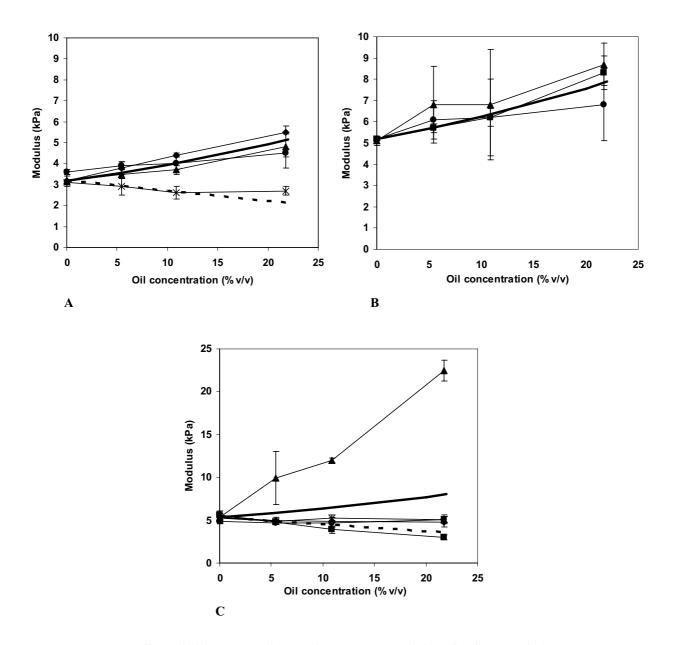


Figure 3.5 - Effect of oil concentration on the Young's modulus of gels (A: gelatine; B: WPI; C: κ -carrageenan) containing emulsions stabilised with different emulsifying agents (\bullet : WPI; \blacksquare WPI aggregates; \blacktriangle : lysozyme; \bullet : 0.5 wt% Tween; X: 2 wt% Tween). In all graphs the bold line represents the data predicted with the van der Poel theory for gels containing emulsion droplets with a diameter of 1 μ m. The broken line of figure A and C represent the data predicted with the van der Poel theory by using a filler modulus of zero.

3.3.3 Effect of oil droplets on fracture properties

Increasing the oil concentration in the case of bound droplets (e.g. gelatine gels with WPI-stabilised emulsions, WPI gels with WPI aggregates-stabilised emulsions) led to a decrease of the fracture strain (Figure 3.6). On the other hand, an increase of the oil concentration for unbound droplets (e.g. gelatine gels with Tween-stabilised emulsions, κ -

carrageenan gels with WPI stabilised emulsions) induced only slight variations in fracture strain (Figure 3.6). For bound droplets, the effective fracture strain increased with increasing oil concentration, resulting in a decrease of the nominal fracture strain. As a result, the gels became more brittle. For both gel systems with oil droplets bound and unbound to the matrix, the Nielsen theory overestimated the effect of oil droplets on fracture strain (Figure 3.6).

Figure 3.7 shows the effect of oil concentration on fracture stress, together with the curves representing the expected values as calculated with the Langley and Green theory for bound droplets and with the Nielsen theory for unbound droplets. For gelatine (Figure 3.7A) and WPI gels (Figure 3.7B), the fracture stress was unaffected by the oil content. An exception was found for gelatine gels containing 2 wt% Tween stabilised emulsion (unbound droplets), for which a decrease of the fracture stress with increasing oil concentration was observed. The minor effect observed for gelatine and WPI gels with bound droplets qualitatively agrees with the Langley and Green, although the stress decrease at low filler concentrations was not observed. The Nielsen theory on the effect of unbound droplets on fracture stress underestimated the experimental results for gelatine gels containing a 2% Tween stabilised emulsion. For κ -carrageenan gels, a decrease in fracture stress with increasing emulsion concentration was observed (Figure 3.7C), roughly following the trend predicted by the Nielsen theory for unbound droplets.

Bound droplets seem to cause a slight decrease of the fracture strain and not to affect the fracture stress, whereas unbound droplets have no effect on fracture strain and induce a decrease of the fracture stress. However, the observed effects are relatively small and in general are not correctly predicted by the existing theories.

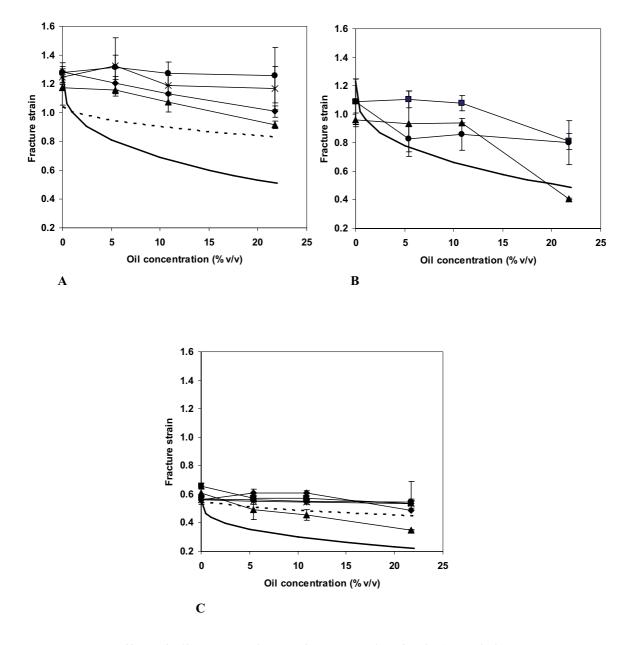


Figure 3.6 - Effect of oil concentration on fracture strain of gels (A: gelatine; B: WPI; C: κ -carrageenan) containing emulsions stabilised with different emulsifying agents (\bullet : WPI; \blacksquare WPI aggregates \blacktriangle : lysozyme; \bullet : 0.5 wt% Tween; X: 2 wt% Tween). The continuous bold line represents the trend expected for bound droplets and the broken line that expected for unbound droplets based on the Nielsen theory (for the case of unbound droplets calculated a stress concentration function S=1 was assumed).

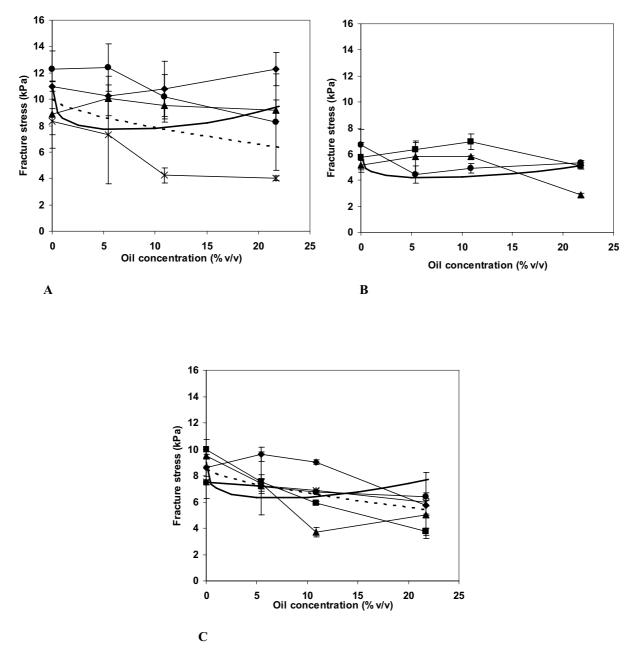


Figure 3.7 - Effect of oil concentration on fracture stress of gels (A: gelatine; B: WPI; C: κ -carrageenan) containing emulsions stabilised with different emulsifying agents (\bullet : WPI; \blacksquare WPI aggregates; \blacktriangle : lysozyme; \bullet : 0.5 wt% Tween; X: 2 wt% Tween). The continuous bold line represent the trend expected based on the Langley and Green theory for bound droplets and the broken line the trend expected based on the Nielsen theory for unbound droplets (calculated assuming a stress concentration function S=1).

3.3.4 Effects of oil droplet aggregation on gel properties

Aggregation of emulsion droplets is reported to affect the rheological properties of emulsion-filled gels by inducing an increase of the effective volume of the fillers (Walstra, 2003). Also the anisometry of the aggregates affects the rheological properties of the gels. Anisometric particles tend to result in a higher storage modulus than spherical particles. Large deformation properties are remarkably influenced by the shape of the fillers, but published data are conflicting (Walstra, 2003).

For gelatine and WPI gels, simple variations of the gel preparation procedures, taking advantage of the gel formation kinetics and the modification of the oil-water interface composition, allowed control of the oil droplet aggregation. For these gels the effect of droplet aggregation on modulus and breakdown properties could be studied by comparing samples with aggregated droplets to others with non-aggregated droplets. The oil droplet size in these two types of gels was comparable.

Gelatine gel samples with non-aggregated and aggregated emulsion droplets were obtained by changing the temperature at which a native WPI stabilised emulsion was mixed to the gelatine solution. A decrease of the temperature of a gelatine solution induces both an increase of the viscosity and a decrease of the time required for gel formation. These two phenomena both retard the aggregation of emulsion droplets driven by van der Waals and depletion interactions. By mixing at 20°C, a gel with non-aggregated droplets was obtained, while by mixing at 45°C the droplets present in the sample appeared clustered into large aggregates with loose structure and an average diameter of 20-40 µm (Figure 3.8). Taking into account the attractive interaction between gelatine and the droplets, the presence of gelatine within these weak, large aggregates would be expected. The Young's modulus of gelatine gels with aggregated droplets was consistently higher than that of gels with non-aggregated droplets (Figure 3.10A). No effects were observed on fracture properties. The presence of these aggregates result in an increase of the effective volume of the droplet aggregates due to the entrapped matrix.

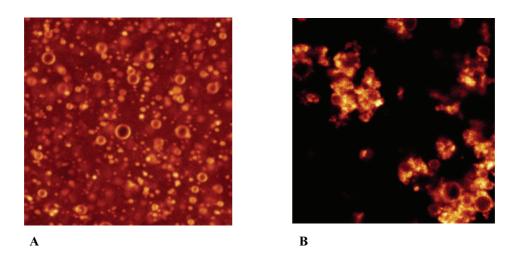
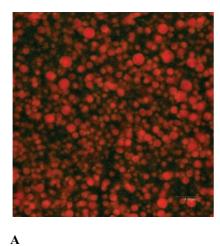
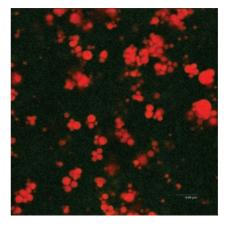


Figure 3.8 - CLSM images of gelatine gels containing a WPI stabilised emulsion mixed with the gelatine matrix at different temperatures (5 wt% oil; A: 20°C; B: 45°C) (image size 39.7 X 39.7 μ m).

In order to prepare WPI emulsion-filled gels with non-aggregated oil droplets the procedure described in chapter 2 (Rosa, Sala, van Vliet & van de Velde, 2006) was followed. This work showed that addition of WPI-stabilised emulsions to a WPI aggregates dispersion results in phase separation because of depletion-flocculation phenomena. This could be prevented by using a certain concentration of WPI aggregates instead of native WPI to prepare the emulsion. A possible explanation for this effect is a thicker layer of protein adsorbed at the oil/ water interface, which would increase the steric repulsion between the droplets. To assess the effect of emulsion droplet aggregation on the properties of WPI gels, an oil-soluble emulsifier (a mixture of saturated monoglycerides) was added to the oil phase. Thereby it was assumed that the oil-soluble emulsifying agent would partially displace protein from the oil/water interface, creating patches with less or even no protein, where the droplets could make contact with others by hydrophobic interactions (Benjamins, Zoet & van Aken, submitted). Figure 3.9 shows a comparison between a gel prepared with a 3 wt% WPI aggregates-stabilised emulsion and one with an emulsion prepared with the same concentration of WPI and with 1 wt% monoglycerides in the oil phase. The oil droplet aggregates present in samples prepared with monoglycerides had an average diameter of 5-10 µm and consisted of 6-20 droplets. For WPI gels, the modulus of samples with non-aggregated droplets was not significantly different from that of gels with aggregated droplets (Figure 3.10B). Also, for these gels no

effects were observed on fracture properties. For these gels, the lack of effect of droplet aggregation on the modulus as compared to gelatine gels could be related to the small size of the aggregates, resulting in a more limited increase of the effective volume of the droplet aggregates. An alternative explanation could be the weakness of the oil droplet aggregates. The aggregation could induce also in this case an increase of the effective volume of the fillers. Nevertheless, the Young's modulus of the aggregates could be lower than that of the oil droplets, counterbalancing the effect of the increase in effective volume.





B

Figure 3.9 - CLSM images of WPI gels containing emulsions prepared with different emulsifying agents (5 wt% oil; A: 3 wt% WPI aggregates; B: 3 wt% WPI aggregates + 1 wt% Dimodan HR in the oil phase) (image size 39.7 X 39.7 μ m).

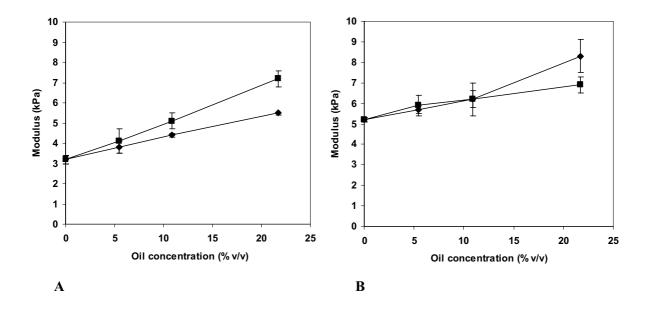


Figure 3.10 - Effect of oil droplet aggregation on gel modulus at different oil concentrations: A: gelatine with a WPI stabilised emulsion; B: WPI with a WPI aggregates stabilised emulsion (\diamond : non-aggregated droplets; \blacksquare : aggregated droplets).

3.4 Discussion

The typical shear modulus of a protein-stabilised oil droplet with a diameter of 1µm is about 40 kPa. The shear modulus of real food products varies from 0.5-5 kPa in dairy puddings to 140-2000 kPa in pressed semi-hard cheeses. This thesis focuses on the first type of food products, in which the modulus of the oil droplets exceeds that of the matrix. For this type of foods, a clear difference can be expected between systems in which the oil droplets are bound to the gel matrix and systems in which the droplets are unbound.

The van der Poel and the Kerner theories, normally used to predict the effect of oil droplets on the shear modulus of filled gels, can also be used for the prediction of the effect of oil droplets on the Young's modulus of filled gels as obtained in large deformation compression measurements. The use of these theories requires knowledge on the interactions between oil droplets and gel matrix. For droplets bound to the matrix, a droplet modulus as derived from the Laplace equation can be used for the calculations. To calculate the effect of droplets on the Young's modulus of filled gels, the modulus of the droplets as obtained from the Laplace equation can be multiplied by a factor 3. For unbound droplets, a modulus of zero can be used for the calculations. The interactions

between oil droplets and gel matrix are related to the interactions between the emulsifying agents used for emulsion preparation and the gelling agents. The prediction of the interactions between emulsifying agents and gelling agents based on their molecular properties is difficult. Therefore, the van der Poel and the Kerner theories can be used for the prediction of the effect of oil concentration on gel modulus after ascertaining the type of interactions between oil droplets and gel matrix by means of rheological measurements.

For droplets with a modulus exceeding that of the matrix, only two extremes (bound or unbound) could be obtained by varying the surface properties of the emulsion droplets. A slight variation of the interactions between droplets and matrix for a given type of filler does not have a noticeable effect on gel modulus. Hence, a modification of the surface properties of the emulsion droplets will not result in a variation of the gel modulus as measured at large deformation within a range between the maximum (bound droplets) and minimum (unbound droplets) values that can be obtained. Similarly, in reverse, the strength of the binding between droplets and matrix can not be deduced from measurements of the modulus at large deformation. Rheological measurements at small deformation are likely to be more suitable to detect differences in the modulus of emulsion-filled gels related to different interactions between oil droplets and gel matrix.

The fracture strain decreases with increasing oil content for gels with bound droplets and is unaffected by the oil content in the case of gels with unbound droplets. A qualitatively similar indication is supplied by the theory of Nielsen (1966). Following Nielsen, in the case of perfect adhesion between filler and matrix (bound droplets) a larger decrease of the fracture strain with increasing filler concentration would be expected as compared to the case of no adhesion (unbound droplets) and without stress concentration. Nevertheless, Nielsen still predicts a decrease of the strain with increasing filler concentration also in the case of no adhesion (Figure 3.3). Furthermore, in case of stress concentration (S<1) the decrease in fracture strain for unbound droplet could be even larger than for bound droplets. The Nielsen theory, which largely overestimated the experimental results, assumes a homogeneous structure of the gel matrix. The observed limited effect of fillers on strain may indicate that the size of the emulsion droplets used in this study was comparable to (or smaller than) that of the inherent structure defects present in the gel matrix. Oil droplets fitting in existing structure defects or creating defects with similar size would not significantly disrupt the gel network. This would impair the basic assumption of the Nielsen theory, i.e. that the actual strain induced in the matrix is larger

than the nominal strain by a factor which depends on the filler volume. Concerning the case of gels with unbound fillers, the lack of physical foundation for the concentration function S undermines this specific part of the theory and makes it a mere fit model.

The fracture stress is unaffected by an increase of the concentration of bound droplets and decreases with increasing concentrations of unbound droplets. For bound droplets, the minor effects observed with increasing oil concentration above a few percent qualitatively agree with both the theory of Langley and Green (1989) and that of Ross-Murphy and Todd (1983). Nevertheless, the sharp stress decrease at low filler concentrations predicted by both theories was not observed in this work. Actually, this sharp decrease is also not shown in the experimental data reported in the work of Langley and Green. As a matter of fact, these authors did not analyse gel samples without fillers, missing the effect of addition of a low amount of fillers on fracture parameters. An analysis of both the theories of Langley and Green and that of Ross-Murphy and Todd reveals that the sharp decrease of the fracture stress at low filler concentration is directly related to the sharp decrease in fracture strain described by the Nielsen theory. Therefore, the failure of both the theories of Langley and Green and that of Ross-Murphy and Todd in predicting the effect of fillers on fracture stress is related to the failure of the Nielsen theory in predicting the effect of fillers on fracture strain. For unbound droplets, the Nielsen theory only qualitatively predicts the experimental results. Also for the fracture stress, the discrepancy between experimental results and theoretical predictions can likely be related to the small size of the emulsion droplets as compared to the size of structure defects in the gel matrix. From these findings can be concluded that the Nielsen theory on fracture strain and the theories of Langley and Green and Ross-Murphy and Todd on fracture stress are not suitable for the prediction of the effect on fillers on the fracture properties of gels containing emulsion droplets. For gels with bound droplets, the most evident effect of the decrease of fracture strain with increasing oil concentration is an increased brittleness. For gels with unbound droplets, the decrease of fracture stress with increasing oil concentration results in an increased spreadability of the gels.

The forces responsible for the formation of emulsion droplet aggregates present in the gels studied in this work can be mainly attributed to hydrophobic, van der Waals and depletion interactions. For gels containing bound droplets, aggregation of the oil droplets present in the gel matrix only affects the gel modulus, to an extent related to the size and to the stiffness of the aggregates. Larger aggregates induce an increase of the effective volume of the fillers, resulting in an increase of the modulus. A similar effect can be expected when aggregation occurs in gels containing unbound droplets. In this case, larger aggregates are likely to induce a decrease of the modulus and of the fracture strain of the gels.

3.5 Conclusions

In this study the modulus of emulsion-filled gels with three different gelling agents is varied by changing the interactions between oil droplets and gel matrix. As a result, the modulus varies between two extremes: with bound droplets the modulus increases, whereas with unbound droplets it decreases. The experimental results can be well fitted by available theories, but the predictive value of the theories depends on knowledge about the interactions between oil droplet and gel matrix. The effect of oil droplets on fracture properties is minor, and theories previously applied to similar systems fails to predict the experimental data. The aggregation of oil droplets present in the gel only affects the gel modulus. The extent of the effect of aggregation is related to the size and the stiffness of the aggregates.

3.6 Acknowledgments

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3.7 References

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Chapter 4

Effect of matrix properties on the sensory perception of emulsion-filled gels

G. Sala, R.A. de Wijk, F. van de Velde, G.A. van Aken (2008). Matrix properties affect the sensory perception of emulsion-filled gels, *Food Hydrocolloids*, 22 (3), 353-363.

Abstract

The breakdown properties and sensory perception of emulsion-filled gels with different matrices were studied at varying emulsion concentrations. The gel matrices used were cold-set whey protein isolate (WPI), gelatine, κ -carrageenan and a mixture of κ carrageenan and *i*-carrageenan. The oil-in-water emulsions added to the gels were either stabilised by native WPI or WPI aggregates. The emulsion droplets were homogeneously distributed in WPI gels, slightly aggregated in mixed $\kappa/1$ -carrageenan and extensively aggregated in κ -carrageenan gels. For gelatine, gels with equal composition but with either non-aggregated or aggregated emulsion droplets could be prepared by changes in processing conditions. The gel modulus as determined by large deformation experiments increased at increasing emulsion concentration for WPI and gelatine gels, but decreased for κ -carrageenan gels. For mixed κ/t -carrageenan no effect of the emulsion concentration on gel modulus was observed. Based on these observations, we concluded that the emulsion droplets were bound to the matrix in WPI and gelatine gels and unbound in carrageenan gels. Most of the mouthfeel attributes generated by a Quantitative Descriptive Analysis (QDA) sensory panel discriminated between emulsion concentrations and different types of gel matrix. At increasing emulsion concentration the perceived creaminess of the samples increased. For gelatine, κ -carrageenan and mixed κ/t carrageenan gels, i.e. for gels that melt at the oral processing temperature or containing unbound oil droplets, the creaminess scores were consistently higher than for WPI gels, which were perceived as more rough. For gelatine gels, no effect of oil droplet aggregation on sensory perception was found.

4.1 Introduction

The effect of oil content and droplet size on the rheological and breakdown properties of emulsion-filled gels has been studied in several systems. The study of the connection between sensory and rheological properties has been attempted for gels, emulsions, and semi-solid complex foods with yielding behaviour, but for emulsion-filled gels this aspect did not receive much attention. For these systems, the perception of the gel matrix and that of the emulsion droplets are likely to influence each other. Furthermore, also the interaction between gel matrix and emulsion droplets is likely to affect the overall perception.

The sensory perception and mechanical properties of gelatine gels were studied at varying gelatine concentration (Munoz, Pangborn & Noble, 1986a). By increasing the gelatine concentration, the firmness and cohesiveness as assessed by manual and oral shear and compression increased, while the extent of breakdown in the mouth decreased. The manual compression and biting with the front teeth could discriminate well across gelatine concentrations. An increased gelatine concentration induced an increase of the maximum force applied during breakdown measurements, but did not affect elasticity, cohesiveness or the strain at yielding and fracture. The same research group studied also the sensory and mechanical properties of sodium alginate and κ -carrageenan gels (Munoz, Pangborn & Noble, 1986b). Gelatine was the most elastic and firmest of the considered gels and broke down during mastication in a few large pieces. Kappa-carrageenan was the least elastic and least firm and broke down during mastication in several small pieces.

In agar gels an increase of the oil content and of the size of the oil droplets stabilised by fatty acids polyglycerol esters induced a decrease of fracture stress and strain measured by compression tests (Kim et al., 1996). The sensory evaluation indicated the gels with larger droplets to be softer and oilier, showing that the fillers were not bound to the gel matrix.

Non-oral sensory attributes (e.g. *surface water, flowability, firmness, give, resistance*) of milk gels with different texture properties and containing emulsions prepared with different oils were well correlated to data obtained from compression test and syneresis measurements (Pereira, Singh, Munro & Luckman, 2003). The texture characteristics of the gels were modulated by changing the preparation procedure (heat-treatment and total solids). Nevertheless, the approach followed in this study did not

provide information on the link between textural and rheological properties and consumer sensory perception.

In a comparison between stranded and particulate WPI emulsion-filled gels, only the firmness as sensed with the first bite, the number of chews and the time to swallow were correlated to the oil content of the gels. The other sensory texture attributes were all correlated to the gel structure type (Gwartney, Larick & Foegeding, 2004). In the systems studied, an increase of oil content was related to an increase of gel firmness.

Literature data on the sensory perception and breakdown properties of emulsionfilled gels mostly analyse the effect of oil droplets on the properties of a particular kind of gel, but do not offer an explanation for the mechanisms linking gel characteristics and sensory attributes. In this chapter, we want to fill this gap by unravelling the role of the gel matrix and that of the interaction between oil droplets and matrix in the sensory perception of emulsion-filled gels. To this end, gels with matrices with different rheological properties were evaluated by a sensory panel trained according to the principles of Quantitative Descriptive Analysis (QDA). Kappa-carrageenan, a mixture of κ carrageenan and ι -carrageenan, cold-set whey protein isolate and gelatine gels were chosen as matrices with a wide variety of parameters concerning elasticity, brittleness and yielding properties.

4.2 Materials and methods

4.2.1 Materials

Powdered whey protein isolate (WPI; BiproTM) was obtained from Davisco International Inc. (La Sueur, MN, USA). Kappa-carrageenan and ι-carrageenan were kindly donated by CP Kelco (Lille Skensved, Denmark). The κ -carrageenan sample consisted of 93% mol κ units and 7% mol ι-units, while the ι-carrageenan sample consisted of 100% ι-units, as determined by NMR spectrometry (van de Velde, Pereira & Rollema, 2004). Gelatine PBG 07 (bloom 280, 5.41 mPa s) was kindly provided by PB gelatines (Vilvoorde, Belgium). Medium Chain Triglycerides (MCT) MIGLYOL 812N oil was purchased from Internatio BN (Mechelen, Belgium). KCl (p.a.) was obtained from Merck (Darmstadt, Germany). Glucono-δ-lactone (GDL; GluconalTM) was kindly donated by Purac (Gorinchem, The Netherlands). Saccharin was from Acatris Netherlands B.V. (The Netherlands). Vanilla flavour was donated by Danisco (Grinsted, Denmark). All materials were used without further purification. All solutions were prepared with demineralised water.

4.2.2 Sample preparation

4.2.2.1 <u>Emulsions</u>

WPI solutions were prepared by adding the protein to the required amount of water. Subsequently, the solutions were gently stirred for 2 hours at room temperature. Stock emulsions, containing 40 wt% MCT oil and 1 wt% WPI in the water phase, were prepared by pre-homogenising the ingredients using an Ultra Turrax (Polytron, Switzerland). Preemulsions were further processed using a laboratory homogenizer (Ariete, Model NS1001L – Panda, Niro Soavi S.p.A, Italy). The volume-surface average or Sauter diameter ($d_{3,2}$) of the droplets of this emulsion was $0.62 \pm 0.05 \mu m$. To the emulsion used for the preparation of κ -carrageenan and mixed κ/ι -carrageenan gels, KCl was added to reach a concentration of 10 mM in the water phase.

Emulsions stabilised with WPI aggregates were prepared as described above, but using a 3 wt% WPI aggregates dispersion as continuous phase. This dispersion was prepared by heating a 9 wt% WPI solution at 68.5° C for 2 hours and subsequently cooling to room temperature with tap water and diluting to 3 wt%. This preparation procedure induces a denaturation of the whey protein >95% (Alting, 2003). The Sauter diameter of the droplets of this emulsion was $0.92 \pm 0.05 \,\mu$ m.

The droplet size distribution of the stock emulsions was measured using a Malvern MasterSizer X (Malvern Instruments, USA).

4.2.2.2 <u>Gels</u>

Gels were prepared with the following concentrations of the gelling agents in the aqueous phase:

- κ -carrageenan: 0.75 wt% (in 10 mM KCl);
- mixed κ/ι-carrageenan: 0.5 wt% κ- carrageenan + 0.5 wt% ι-carrageenan (in 10 mM KCl);

- acid-induced, cold-set WPI gels: 3 wt% (in water);
- gelatine: 4 wt% (in water).

The concentrations of the gelling agents were chosen in such a way that the gels had similar apparent firmness. As shown further on, this appeared to correspond to similar fracture stress rather than similar elasticity. As sweetening agent saccharin (0.012 wt%) was added to emulsions and gels solutions. As tasting agent vanilla (0.033 wt%) was used in both emulsions and gels.

The cold gelation of the WPI gels was induced by addition of a suitable amount of GDL (0.22 wt% WPI aggregates dispersion with a concentration of 3 wt%) to the WPI dispersion and to the WPI dispersion/emulsion mix and incubation at 25°C for 17 hours (Rosa, Sala, van Vliet & van de Velde, 2006). The WPI dispersion was prepared as described above.

For carrageenan and gelatine gels, the gelling agent was allowed to hydrate for 2 hours under gentle stirring at room temperature. The samples were subsequently dissolved by heating at 80°C for 30 minutes and cooled to 45°C. Prior to emulsion addition, the emulsion was also heated to 45°C. After mixing, the liquid samples were allowed to gel at room temperature. Gelatine samples with non-aggregated emulsion droplets were prepared by mixing the emulsion with the gelatine solution at 20°C. The final pH of the gels is reported in Table 4.1.

The samples for breakdown measurements were allowed to gel in 60 ml plastic syringes (internal diameter 26.4 mm) coated with a thin paraffin oil film. The samples for the QDA evaluation, prepared under food-grade and sterile conditions, were allowed to gel in lidded plastic cups with a capacity of 50 ml.

		рН	
Oil content	0	5	20
WPI	4.88	4.77	4.67
к-carrageenan	8.35	7.88	7.51
к/ 1-carrageenan	8.21	7.93	7.59
Gelatin	5.34	5.33	5.68

Table 4.1 - pH of the studied gels.

4.2.3 Large deformation experiments

Uni-axial compression tests were performed approximately 24 hours after preparation at the same moment of the QDA evaluation. Gel pieces of about 25 mm height were used for the measurements with an Instron 5543 machine (Instron Corporation, USA) equipped with a plate-plate geometry. The plates were lubricated with a thin layer of paraffin oil. The measurements were performed at room temperature, at a constant deformation speed of 1 mm/s and up to a compression strain of 80%. The mentioned deformation speed was already used for the study described in chapter 2 (Rosa et al., 2006), after ascertaining the limited effect of compression speed on fracture parameters. For gelatine gels 4 pieces per specimen and 2 specimens were analysed. For the other gels at least 4 pieces per specimen and 1 specimen were used for measurement.

4.2.4 Confocal Laser Scanning Microscopy (CLSM)

Samples for microstructural analyses were stained with Rhodamine B (0.2 wt% solution; 10 μ L per mL sample) to visualise the protein phase. CLSM-images were recorded on a LEICA TCS SP Confocal Laser Scanning Microscope, equipped with an inverted microscope (model Leica DM IRBE), used in the single photon mode with an Ar/Kr visible light laser. A Leica objective lens (63x/UV/1.25NA/water immersion/PL APO) was used. The excitation wavelength was set at 568 nm. The emission maximum of Rhodamine B is at 625 nm. Digital image files were acquired in multiple tif formats at 1024x1024 pixel resolution.

4.2.5 Quantitative Descriptive Analysis

4.2.5.1 <u>Assessors/ sensory attributes</u>

The sensory characteristics of the gels were investigated with the use of a sensory panel trained according to the principles of Quantitative Descriptive Analysis (QDA) (Stone & Sidel, 1985). The panel consisted of nine females aged between 22 and 49 and with above-average scores on all selection tests. These tests included tests of odor identification, odor memory, and verbal creativity, and a series of texture tests in which the ability of the panelist to assess fattiness, roughness, and particle size was measured. All panelists had previously been trained for the assessment of the sensory properties of oil-in-water

emulsions. Panelists were seated in sensory booths with appropriate ventilation and lighting. The products were assessed semi-monadically in duplicate on visual analogue scales. The presentation order was randomly assigned per panellist. Acquisition of the panelist's responses was done by computer using FIZZ software (Biosystemes, 1998). In 4 2-hr sessions the panel was presented and trained with a set of 8 samples of emulsionfilled gels. During these training sessions descriptive attributes were generated that were used to profile 10 emulsion-filled gel samples with 4 reference samples without emulsion. Each gel was served in portions of 40 ml in plastic beakers (volume 50 ml) at an average rate of one sample per 5 minutes. The attributes were generated in Dutch and subsequently translated in English. During profiling the attributes appeared per category on a monitor placed in front of the panelist with the attributes on the left and a 100-point response scale anchored at the extremes on the right. The panelist used a mouse to indicate the perceived strength of each attribute. Each product was first smelled after which the odor attributes were rated. Next, the product was taken into the mouth after which the taste/flavor and mouthfeel attributes were rated in the order in which they were perceived. Finally, the product was spat out. The after feel attributes were rated and the panelists rinsed their mouths with acidified water before evaluating the next sample.

4.2.5.2 Data analysis

The relationships between sensory attributes and gel samples characteristics were summarized using Principal Component Analysis (PCA) (Unscrambler, Camo Inc., Corvallis, U.S.A). PCA facilitates the identification of attribute synonyms and covariate attributes. Relationships between specific attributes were statistically modeled using Partial Least Squares Regression or PLSR (Unscrambler Vs. 7.5, Camo Inc., Corvallis, U.S.A). The effects of changes in ingredient composition on individual sensory attributes were analyzed using a factorial ANOVA (SPSS, SPSS Inc, Chicago, U.S.A.), carried out on the raw sensory data. In addition to the four gelling agents main effects and second order interactions, the ANOVA included a random panelist effect and a session effect. Because the ANOVA was carried out on the raw sensory data, it was possible to carry out tests of significance for all effects.

4.3 Results and Discussion

4.3.1 Microstructure

Microstructure analysis was carried out to determine the distribution of the oil droplets in the gel matrix. Oil droplets were homogeneously distributed in the matrix of WPI gels (Figure 4.1A), whereas droplet aggregates were observed in κ -carrageenan (Figure 4.1B) and mixed κ/ι -carrageenan (Figure 4.1C) gels. In κ -carrageenan gels the aggregation was much more extensive than in mixed κ/ι -carrageenan gels. For gelatine gels, the oil droplet aggregation was successfully varied by changing the temperature at which the emulsion was mixed with the gelatine solution. When this operation was performed at 45°C, droplet aggregation was observed (Figure 4.2A). By decreasing the temperature of both the emulsion and the gelatine solution to 20°C prior to mixing, the aggregation of the oil droplets was prevented (Figure 4.2B). A decrease of the temperature of a gelatine solution resulted in both an increase of the viscosity and a decrease of the gel setting time. Hence, droplet aggregation caused by weak forces, such as van der Waals interactions, could be avoided by decreasing the mixing temperature.

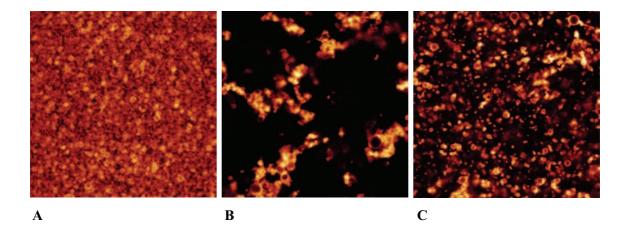


Figure 4.1 – CLSM image of WPI (A), κ -carrageenan (B) and κ / ι -carrageenan (C) gels with 5 wt% emulsion (image size 39.7 X 39.7 μ m).

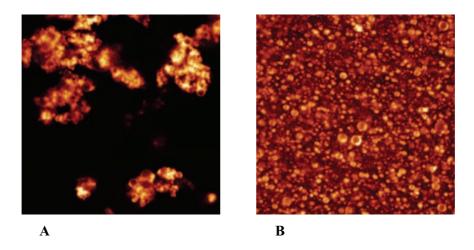


Figure 4.2 – CLSM image of gelatine gel with 5 wt% emulsion (A= prepared at 45°C; B= prepared at 20°C; image size 39.7 X 39.7 μ m).

4.3.2 Elastic modulus

Figure 4.3 shows the stress vs. strain curves of the studied gels without emulsion droplets. Samples with comparable elastic modulus (initial slope of the curve), but different fracture properties were successfully prepared for κ -carrageenan and WPI gels, but not for gelatine and κ/ι -carrageenan gels. For κ -carrageenan, at concentrations lower than 0.75 wt% the obtained gels were too weak to be handled. For gelatine gels a modulus comparable to that of κ -carrageenan could not be achieved because at gelatine concentrations higher than 4 wt% extremely elastic and tough samples that were difficult to chew were obtained. The high viscosity of κ/ι -carrageenan gels prepared at concentrations higher than 1 wt% restrained the mixing of the emulsion with the gel matrix. The chosen gel types covered a wide range of breakdown behaviours. This allowed a broad comparison among gel matrices and yielded conclusive results of the effects of oil droplets on both the breakdown and sensory properties of emulsion-filled gels.

In Figure 4.4 the effect of emulsion content on modulus is shown for all the studied systems. For WPI and gelatine an increase of the modulus was observed at increasing emulsion concentration. For gelatine samples with aggregated emulsion droplets, this increase was larger than for the gels with non-aggregated droplets. In κ -carrageenan gels, an increase of emulsion content induced a substantial decrease of the modulus. In mixed κ/ι -carrageenan gels the modulus appeared independent of the emulsion concentration.

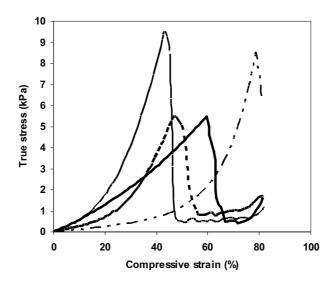


Figure 4.3 – Breakdown curves of the gels without emulsion (— WPI; ––– κ -carrageenan; κ/ι -carrageenan; — gelatine).

Van Vliet (1988) defined emulsion droplets present in a gel as active fillers when they are bound to the matrix. At increasing concentration of active filler the gel modulus increases. Oil droplets unbound to the gel matrix and inducing a decrease of the gel modulus were defined as inactive fillers. Based on these definitions, the emulsion droplets present in WPI and gelatine gels behaved as active fillers and those present in κ carrageenan gels as inactive fillers. The interactions between oil droplets and gel matrix were unclear for mixed κ/ι -carrageenan gels. A detailed explanation of the interactions between oil droplets and gel matrix in the different gels is given below.

The pH has a large effect on the protonation and charge of the biopolymers at the droplets surfaces and in the gel matrix and, consequently, determines the electrostatic interactions between the surface of oil droplets stabilised with protein and the gel matrix. Therefore, for all studied samples the pH was measured (Table 4.1). The isoelectric point of whey proteins is about 5. At pH above this value, the net charge of whey proteins is negative. At pH lower than the isoelectric point, the net charge of whey proteins is positive.

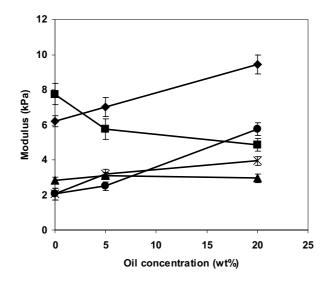


Figure 4.4 - Effect of oil concentration on modulus (\blacklozenge : WPI; $\blacksquare \kappa$ -carrageenan; \blacktriangle : κ/ι -carrageenan; \blacklozenge : gelatine aggregated droplets; \times : gelatine non-aggregated droplets).

For WPI gels, the oil droplets were stabilised with the same protein material as the gel matrix. As a consequence, no strong electrostatic interaction can occur between the emulsion droplets and the gel matrix. The interactions between these two elements of the gel systems are of the same nature as those responsible for gel formation, i.e. hydrophobic interactions and sulphur bridges (covalent cross linking). The emulsion droplets present in the gel act as active fillers because of these forces and bonds.

Gelatine gels had a pH around 5.3. At this pH, gelatine (isoelectric point~ 8.7) and the whey protein adsorbed on the surface of the emulsion droplets are oppositely charged and attractive electrostatic interactions occur. This explains the observation that the droplets of the emulsion used for the filled gelatine gels acted as active fillers, inducing an increase of the gel modulus. The droplet aggregates present in the gels prepared by mixing gelatine solution and emulsion at high temperature (Figure 4.2) were probably formed by relatively weak forces, such as van der Waals interactions. Taking into account the attractive interaction between gelatine and oil droplets, the presence of gelatine within these weak, large aggregates can be expected. The presence of these aggregates results in an increase of the effective volume of the droplet aggregates due to the entrapped matrix. This can explain the fact that the elastic modulus of gelatine gels with aggregated droplets was higher than that of gels with non-aggregated droplets (Figure 4.4). The pH of κ -carrageenan gels was about 8. Kappa-carrageenan is a polyanionic polymer whose negative charge is determined by the presence of sulphur groups in the polysaccharide chain. At the mentioned pH, the κ -carrageenan gel matrix and the WPI protein covering the oil droplet are both negatively charged. Therefore, repulsive electrostatic interactions are expected. Depletion forces are also likely to be involved in the formation of droplet aggregates in these κ -carrageenan gels. Similar considerations can be made for mixed κ/ι -carrageenan gels. For these samples, the lower degree of aggregation of the emulsion droplets can be related to the lower sensitivity of β -lactoglobulin (main component of WPI) stabilised emulsions to ι -carrageenan induced depletion-flocculation phenomena as compared with κ -carrageenan (Gu, Decker & McClements, 2005). This property of ι -carrageenan, more densely charged than κ -carrageenan, was related to its ability to form highly charged interfacial membranes on the droplet surface.

Using only two different emulsions prepared both with the same basic emulsifier, a wide range of interactions oil droplets-gel matrix could be obtained. This was possible because of the different physicochemical properties of the gel matrices under study. Even though the mechanisms responsible for interactions were different, basically two gel systems with oil droplets bound (WPI and gelatine) and unbound (κ -carrageenan and κ /icarrageenan) to the gel matrix could be obtained.

4.3.3 Fracture behaviour

The effect of oil content on fracture stress is shown in Figure 4.5A. For κ -carrageenan and mixed κ/ι -carrageenan gels, increasing the oil content caused a decrease of the fracture stress. This further demonstrates that in κ -carrageenan gels, as well as in mixed κ/ι -carrageenan gels, the emulsion droplets are not connected to the matrix and weaken the gel network. In WPI gels a slight increase of the fracture stress was observed at increasing emulsion concentration. For gelatine gels no clear correlation was found between fracture stress and emulsion content.

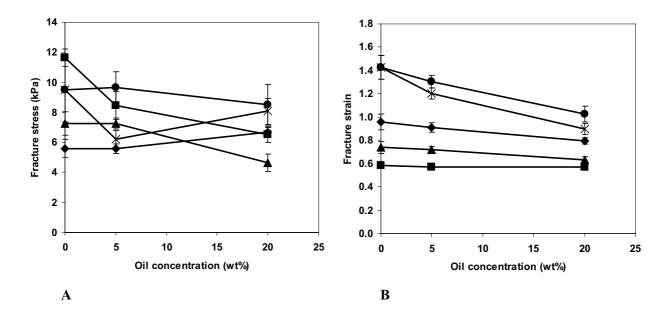


Figure 4.5 - Effect of oil concentration on fracture stress (A) and fracture strain (B) (\diamond : WPI; $\blacksquare \kappa$ -carrageenan; \blacktriangle : κ/ι -carrageenan; \diamond : gelatine aggregated droplets; \times : gelatine non-aggregated droplets).

The effect of emulsion concentration on fracture strain is shown in Figure 4.5B. The presence of emulsion droplets in the gel matrix caused all the tested gels, except κ -carrageenan gels, to become more brittle. This phenomenon is in accordance with the data reported by other authors (Langley et al., 1989; Kim et al., 1996) and it is caused by stress concentration at the filler surface during fracture propagation. In gels in which the droplets are not connected, as in κ -carrageenan gels, this does not appear to happen. The higher the fracture strain of the gel without oil droplets, the larger the effect of the emulsion on brittleness. For gelatine gels the aggregation of the emulsion droplets was related to a larger decrease of the fracture strain as compared to the samples with non-aggregated oil droplets.

In Table 4.2 the distribution on the oil droplets within the gel matrix and the qualitative effects of the emulsion droplets on the rheological and breakdown properties of the different gels are summarized.

Gel matrix	Droplet status	Droplet- matrix interactions	Effect on modulus	Effect on fracture properties	
				Stress	Strain
WPI	Non-aggregated	Bound	Increase	Increase	Decrease
к-carrageenan	Aggregated	Unbound	Decrease	Decrease	No effect
к/ 1-carrageenan	Aggregated	Unbound	No effect	Decrease	Decrease
Gelatine	Aggregated/ non-aggregated	Bound	Increase	No effect	Decrease

Table 4.2 – Distribution of the oil droplets within the matrix, droplet-matrix interactions and effects of oil droplets on rheological and breakdown properties of the gels.

4.3.4 Sensory properties

During the training sessions the QDA panel generated a set of 44 attributes describing odour (7), taste (9), mouthfeel (15), and after taste/feel (13) sensations (Table 4.3; odour attributes not reported). This set of attributes was used to rate 8 emulsion-filled gel samples and 4 reference samples without emulsion. For the present study only mouthfeel and the after feel attributes were taken in to consideration.

Almost all mouthfeel and after feel attributes, except *crumbly, melting, oily* mouthfeel and *astringent* after feel varied with oil concentration (Table 4.4). All attributes, except *filling* mouthfeel and *tacky* after feel, varied with gel type (Table 4.4). Interestingly, while the mouthfeel attribute *creamy* varied with fat content as well as with gel type, the attribute *oily* varied only with gel type. In custard and custard-like semi-solid foods a correlation was found between the attributes *creamy* and *oily* (de Wijk, R.A., Terpstra, M.E.J , Janssen, A.M. & Prinz, J. F., 2006). Apparently, the inclusion of emulsion droplets in a gel matrix prevents the increase in oiliness at increasing fat content to be perceived. This masking effect did not occur for creaminess perception.

None of the sensory attributes generated by the QDA panel varied for gelatine gels with aggregated and non-aggregated emulsion droplets (Table 4.5). The interactions responsible for droplet aggregation in these gels were weak and induced only limited changes in the rheological and fracture properties of the samples. However, we cannot exclude that such an effect exists if the bonds among droplets within aggregates would be stronger. When compared to the analysis comprising all gels, fewer parameters (4 mouthfeel attributes and 3 afterfeel attributes) could discriminate between gelatine gels

with emulsion concentrations of 5 and 20 wt%. This is partly due to the fact that the samples without emulsion were not taken into consideration in the analysis of gelatine gels.

The principal components analysis of the samples illustrates the relationships between gel samples and sensory attributes (Figure 4.6). Principal component 1 (PC1) is clearly related to the fat content, running from *watery* to *creamy*, while principal component 2 (PC2) relates to gel types and runs from *crumbly* to *melting* and *slippery*. In the sensory space the studied gel samples are separated in two groups along PC2, with gelatine and carrageenan gels at the positive scale and WPI gels at the negative scale. The gels of the former group are gels that either contain unbound oil droplets (carrageenan gels) or melt at body temperature (gelatine). This results in the perception of soft, smooth and creamy mouthfeel. WPI gels, on the other hand, contain unbound droplets, do not melt and their oral processing results in the formation of gel crumbs. For both the gelatine and carrageenan gels, it can be anticipated that the disappearance of the gelled matrix in the mouth or the breakdown of the gel will lead to a relatively fast release of the emulsion droplets. This may explain why fat-related attributes are perceived more strongly and more rapidly for gelatine and carrageenan gels than for WPI gels. As mentioned above, for gelatine gels 4 mouthfeel attributes and 3 afterfeel attributes were affected by an increase in oil concentration from 5 wt% to 20 wt% (Table 4.5). This resulted in a remarkable shift in the PCA plot along the *watery-creamy* axis, indicating a noticeable difference in sensory perception (Figure 4.6).

Group	Attribute	Description
Taste	Tintensity	intensity of the taste; taste-explosion
	Tsweet	sugar like, sweet
	Tsour	citrus-like
	Tsalty	little salt; liquorice like, seawater
	Tvanilla	taste of vanilla
	Tpotatostarch	tastes like wall paper glue
	Talgae	taste of algae, like in spirulina
	Tartificialcream	taste of artificial cream
	Tcaramel	caramel
Mouthfeel	Mfirm	stiff, effort to compress, compact
	Melastic	elastic, degree of spring back
	Mslippery	slippery feeling of the product, easily gliding
	Mcreamy	velvety; warm; full; soft
	Moily	oily; fatty layer
	Mspreadable	how the sample spreads between tongue and palate
	Mmelting	sample melts in the mouth, structure disappears
	Mcrumbly	(small) pieces in the mouth
	Mcrumbling effort	effort needed to break the sample into pieces
	Mrough crumbles	crumbles feel rough, fibrous and stiffly
	Mcooling	gives a cold feeling in the mouth
	Mmouthfilling	feeling that whole the mouth is filled up, feel the product everywhere
	Msticky	sticky like peanut butter and gingerbread
	Mwatery	product itself feels damp, humid
	Mdry	dry feeling in the mouth; saliva is absorbed
After Taste	ATsweet	sugar like, sweet
	ATsweetener	artificial sweetener; aspartame; saccharine
	ATbitter	bitter
	ATcardboard	cardboard
	ATcreamy	velvety; warm; full; soft
	AToxidised	metal; iron like; synthetic fat; rubber (gum)
After feel	AFclean	no remaining lumps
	AFastringent	astringent; contracting afterfeel
	AFdry	saliva absorbing; dry tongue
	AFrough	rough feeling on the teeth
	AFraw tongue	raw feeling; sandpaper or pussycat-tongue
	AFcoating	fatty coating on tongue, lips or cheek
	AFtacky	sticky like "post-it"

 Table 4.3 – Attributes generated by the QDA panel.

Table 4.4 – ANOVA analysis on the effect of emulsion concentration and gel type (p-values lower than 0.05, i.e. highly significant, are underlined).

Attribute	Emulsion concentration	Gel type	
Mfirm	0.00	0.00	
Melastic	0.00	0.00	
Aslippery	<u>0.01</u>	<u>0.00</u>	
Acreamy	<u>0.00</u>	<u>0.00</u>	
Moily	0.25	<u>0.00</u>	
Aspreadable	<u>0.01</u>	<u>0.00</u>	
Imelting	0.91	<u>0.03</u>	
Acrumbly	0.13	<u>0.00</u>	
/Irough	<u>0.00</u>	<u>0.00</u>	
Icooling	<u>0.01</u>	<u>0.03</u>	
Imouthfilling	<u>0.00</u>	0.06	
Isticky	<u>0.00</u>	<u>0.00</u>	
Iwatery	<u>0.00</u>	<u>0.00</u>	
Idry	<u>0.00</u>	<u>0.00</u>	
Fclean	<u>0.00</u>	<u>0.00</u>	
AFastringent	0.13	0.01	
AFdry	<u>0.00</u>	<u>0.00</u>	
Frough	<u>0.03</u>	<u>0.00</u>	
Fraw tongue	<u>0.00</u>	<u>0.00</u>	
Fcoating	<u>0.01</u>	<u>0.00</u>	
AFtacky	<u>0.01</u>	0.06	

Table 4.5 – ANOVA analysis on the effect of emulsion droplet aggregation in gelatine gels with 5 and 20 wt% oil (p-values lower than 0.05, i.e. highly significant, are underlined).

Attribute	Emulsion concentration	Aggregation	
Mfirm	0.59	0.75	
Melastic	0.03	0.25	
Mslippery	0.11	0.39	
Mcreamy	<u>0.01</u>	0.22	
Moily	0.04	0.55	
Mspreadable	0.17	0.95	
Mmelting	0.81	0.11	
Mcrumbly	0.48	0.29	
Mrough	0.07	0.30	
Mcooling	0.12	0.82	
Mmouthfilling	<u>0.00</u>	0.06	
Msticky	<u>0.04</u>	0.75	
Mwatery	0.08	0.63	
Mdry	0.09	0.96	
AFclean	<u>0.02</u>	0.31	
AFastringent	0.33	0.77	
AFdry	0.15	0.98	
AFrough	<u>0.01</u>	0.32	
AFraw tongue	<u>0.01</u>	0.49	
AFcoating	0.10	0.66	
AFtacky	0.21	0.23	

p-values

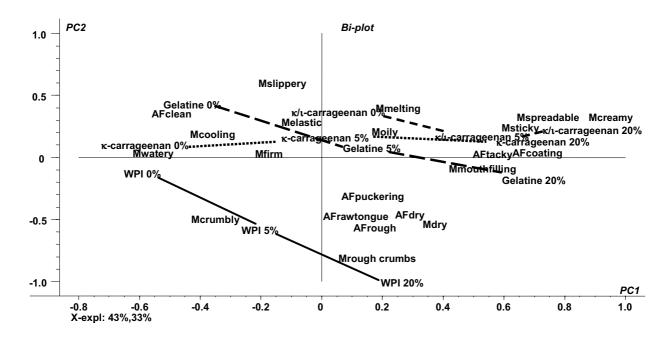


Figure 4.6 – Principal component plot of the sensory data.

For a number of sensory attributes, that were considered to be of particular interest, the relation between emulsion concentration and score of the individual samples was investigated. Figure 4.7A shows the effect of emulsion concentration on creaminess. Although the creaminess increases at increasing oil concentration for all gels, the increase is relatively small for WPI gels. Probably, the higher scores consistently observed for mixed κ/ι -carrageenan could be related to the low elastic modulus and fracture strain of this gel.

The mouthfeel attributes *rough* and *melting* varied strongly between gels melting at human body temperatures and non-melting gels (Figures 4.7B and 4.7C). Gelatine, κ carrageenan and mixed κ/ι -carrageenan gels gave similar scores for the attribute *melting*, while WPI gels scored substantially lower. For the attribute *rough*, a clear effect of emulsion concentration on perception was found only for WPI and gelatine gels, the effect for the first gel type being much larger. Moreover, the roughness scores of gelatine and carrageenan gels were consistently lower than for WPI gels.

The gels with the higher modulus were evaluated by the QDA panel as less firm (Figure 4.7D) than the gels with lower modulus (Figure 4.4). Furthermore, a negative correlation was found between the attribute *firm* and the gel modulus (Table 4.6).

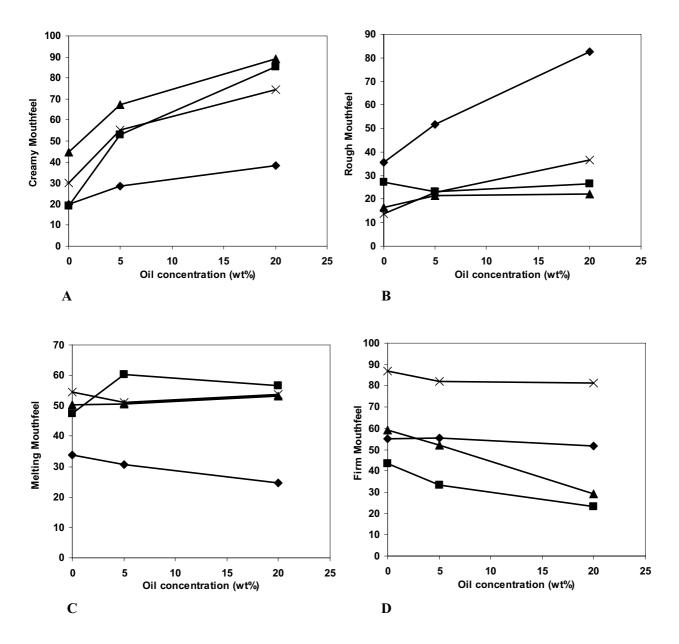


Figure 4.7 – Effect of oil content on mouthfeel attributes creamy (A), rough (B), melting (C) and firm (D) (\diamond : WPI; $\blacksquare \kappa$ -carrageenan; \blacktriangle : κ/ι -carrageenan; \times : gelatine).

	Modulus (kPa)	Fracture stress (kPa)	Fracture strain (True) (mm/mm)	Energy to fracture (mJ)
Mfirm	-0.34	0.30	0.87	<u>0.85</u>
Melastic	-0.62	0.27	<u>0.89</u>	0.71
Mslippery	-0.51	0.17	-0.13	-0.33
Mcreamy	-0.41	-0.31	-0.26	-0.42
Moily	-0.70	-0.02	0.08	-0.11
Mspreadable	-0.37	-0.26	-0.48	-0.62
Mmelting	-0.65	0.32	-0.07	-0.20
Mcrumbly	<u>0.84</u>	0.17	-0.19	0.17
Mcrumbling effort	-0.38	0.25	<u>0.93</u>	<u>0.87</u>
Mrough crumbs	<u>0.77</u>	-0.21	-0.06	0.20
Mcooling	0.10	0.27	-0.19	-0.15
Mmouth- filling	0.12	-0.41	-0.61	-0.59
Msticky	-0.56	-0.23	0.04	-0.12
Mwatery	0.29	0.33	-0.03	0.09
Mdry	0.35	-0.33	0.10	0.21

Table 4.6 – Correlation between rheological/breakdown parameters and mouthfeel attributes (R^2 values higher than 0.75 are underlined).

This is in line with the absence of correlations between firmness at first bite and modulus found for WPI emulsion gels with different gel matrix structure, as determined by torsion breakdown experiments (Gwartney et al., 2004). The order of the samples with regard to firmness was almost the opposite of what was expected based on the data collected for the modulus (Figure 4.4). Furthermore, for all samples a decrease of the firmness was perceived at increasing emulsion concentration. This could perhaps be expected for κ -carrageenan and mixed κ/ι -carrageenan gels, for which a decrease of modulus and fracture stress was observed, but not for WPI and gelatine gels. For the latter gels, the modulus was larger at higher emulsion concentration (Figure 4.4). For WPI gels also the fracture stress at the highest emulsion concentration was higher than that of the reference samples (Figure 4.5A). The sequence of curves observed for firmness at increasing emulsion concentration is similar to that found for the fracture strain (Figure 4.5B). In fact, gelatine showed the highest fracture strain among the samples and was judged as the firmest, while the gel with the lowest fracture strain, κ -carrageenan, received the lowest scores.

R² values

Furthermore, a high correlation was found between fracture strain and firmness (Table 4.6). In spite of the low correlation between fracture stress and firmness, the energy to fracture (that is the product between fracture stress and fracture strain or the area below the stress vs. strain curve delimited by the perpendicular from the fracture stress) correlated well with this sensory attribute (Table 4.6). This indicates that the panel members evaluated the gel firmness as the effort to obtain structure breakdown.

4.4 Conclusions

This study explores the effects of both oil concentration and the gel type on the sensory perception of emulsion-filled gels. Creaminess increases with the oil concentration for all tested systems, but the extent varies with the kind of gel matrix. The effect of melting behaviour of the gel and droplet-matrix interactions on sensory properties is more important than the fracture properties. Gels containing unbound droplets and melting at temperatures typical of oral processing conditions are creamier and show a larger effect of the emulsion content on creaminess perception. Furthermore, for these gels the scores for creaminess and roughness do not remarkably differ between gels, in spite of the large differences in fracture behaviour and droplet-matrix interactions. WPI gels, which do not melt at the oral processing temperature and in which the oil droplets are bound to the gel matrix by covalent interactions, are perceived as rougher and more crumbly. For gelatine gels, no effect of oil droplet aggregation on sensory attributes is found. However, the interactions responsible for droplet aggregation in these gels are weak and induce only limited changes in the rheological and fracture properties of the samples.

Chapter 7 describes the behaviour of different gels under processing conditions comparable with mastication, focussing on the effect of melting properties and dropletmatrix interactions on droplets release.

4.5 Acknowledgements

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Chapter 5

Deformation and fracture of emulsion-filled gels. Effect of oil content and deformation speed.

G. Sala, T. van Vliet, M. A. Cohen Stuart, G.A. van Aken, F. van de Velde, Deformation and fracture of emulsion-filled gels. 1 Effect of oil content and deformation speed, submitted for publication.

Abstract

The large deformation properties of gelatine, κ -carrageenan and whey protein isolate (WPI) gels filled with bound and unbound oil droplets were studied at different compression speeds. The rheological properties of the gel matrices controlled the compression speed dependency of the gels containing oil droplets. Polymer gels (gelatine and κ -carrageenan gels) showed a predominantly elastic behaviour. Their Young's modulus was not affected by the compression speed. The increase of fracture stress and strain observed with increasing compression speed was related to friction between the structural elements of the gels and, for gelatine, to the unzipping of physical bonds. Particle gels (WPI gels) showed a more viscoelastic behavior. Their Young's modulus and fracture stress increased with compression speed. This was attributed to the viscous flow of the matrix and friction phenomena between structural elements of the gel. The effect of an increase in the oil volume fraction (φ) on the Young's modulus was for all gels according to the van der Poel theory. Oil droplets embedded in the gel matrix acted as stress concentration nuclei and increased friction. The relative impact of these two effects was related to the viscoelastic properties of the gels and to droplet-matrix interaction. For polymer gels and gels with bound droplets stress concentration phenomena played a relatively larger role. For particle gels and gels with unbound droplets friction phenomena were relatively more important, increasing the viscoelastic character of the gels. As a result, an increase in φ resulted in a decrease of both fracture stress and fracture strain for polymer gels and in an increase of the fracture stress for particle gels.

5.1 Introduction

In Chapter 3 we showed that the droplet-matrix interactions have mainly an effect on the Young's modulus of the filled gels determined at constant deformation speed. The van der Poel theory developed for small amplitude oscillatory measurements in shear also holds for the Young's modulus determined by large deformation measurements. Under the experimental conditions chosen, the fracture strain decreased with increasing oil volume fraction (ϕ) for droplets bound to the matrix and remained constant for unbound droplets. The fracture stress was unaffected by ϕ for bound droplets and decreased with increasing ϕ for unbound droplets.

The way food products behave when they are eaten is better described by their large deformation and fracture properties than by their small deformation properties (van Vliet & Walstra, 1995; van Vliet, 2002). The sensorial firmness of gels, for instance, depends on the apparent modulus at large deformation and on the fracture or yield stress (van Vliet et al., 1995). In order to establish the relation between mechanical properties and sensory characteristics, the measurement of the mechanical properties should be carried out under experimental conditions mimicking oral processing as much as possible. The fracture properties of many food materials strongly depend on deformation speed (van Vliet, Luyten & Walstra, 1993). Therefore, when measuring the large deformation properties of gels in compression experiments, a compression speed comparable to that encountered under oral conditions (10-40 mm/s) should be applied (Peyron, Mioche, Renon & Abouelkaram, 1996). However, most data reported in literature on the large deformation and fracture properties of emulsion-filled gels have been obtained at much lower compression speeds (Table 5.1).

Gel systems	Extension/compression speed (mm/s)	Reference
Gelatine gels with glass beads.	Extension; 0.016- 16.666.	Ross-Murphy, 1983.
Heat-induced whey protein gels with glass beads and emulsions.	Compression; 0.833.	Langley, 1989.
Skimmed milk gels with different emulsions.	Compression; 0.166.	Xiong, 1991b.
Different types of milk proteins gels with recombined cream.	Compression; 0.166.	Xiong, 1991a.
Heat-induced WPI gels with emulsions stabilised with WPI or non-ionic surfactants.	Compression; 0.166.	McClements, 1993.
Heat-induced WPI gels with emulsions stabilised with WPI.	Compression; unknown.	Yost, 1993.
Agar gels with emulsions stabilised with fatty acids polyglycerolesters.	Compression; 0.5.	Kim, 1996.
Gelatine gels with whey protein particles.	Compression; 0.0016- 0.833	Bot, 1996a.
Gelatine-maltodextrin composite gels.	Extension and compression; 0.83.	Normand, 2001.
Soybean protein isolate gels with soybean protein stabilised emulsions.	Compression; 20.	Kim, 2001.
Heat-induced gels of fractionated whey proteins with fractionated milk fat emulsions.	Compression; 0.833.	Mor-Rosenberg, 2004.
Acid-induced, cold set WPI gels with WPI aggregates stabilised emulsions	Compression; 1.	Rosa, 2006.
Gelatine, κ-carrageenan and acid-induced, cold set WPI gels with different emulsions.	Compression; 1.	Sala, 2007.

 Table 5.1 – Compression speeds reported in literature for breakdown experiments with filled gels.

At present, relatively few data are available in literature on the effects of deformation speed and droplet-matrix interaction on the large deformation properties of emulsion-filled gels. Also the strain-hardening and viscoelastic behaviour of these systems at large deformation are not well described in literature. We believe that understanding these aspects is the key to link rheological and fracture properties of emulsion-filled gels to their sensory characteristics, which motivated us to undertake the present study. Gelatine, κ -carrageenan and whey protein isolate (WPI) were chosen as gel matrices. Emulsions made of medium-chain triglyceride oil, and stabilised with different emulsifying agents (WPI, Tween 20, Lactoferrin and WPI aggregates) were added to these matrices to control droplet-matrix interaction.

5.2 Large deformation and fracture behaviour of gels

In this section an overview is given of the mechanisms responsible for the large deformation and fracture behaviour of different types of gels, including emulsion-filled gels. Particular attention is given to the effect of deformation speed and oil volume fraction (φ). The strain-dependency of the modulus is also described.

5.2.1 Energy balance and role of defects in the large deformation behaviour of viscoelastic materials

To better understand the deformation speed dependency of the fracture properties of food materials, both the energy balance related to fracture and the role of defects present in the structure should be taken into consideration. The energy applied to deform a material (W) can be elastically stored (W'), dissipated either by viscous flow of the material (W"_v) or by friction between components of the system (W"_c) or used for fracture (W_f) (van Vliet et al., 1993):

$$W = W' + W''_{v} + W''_{c} + W_{f}$$
(5.1)

When a piece of material is deformed, the stress at the tip of cracks and around weak spots will be higher than in the rest of the structure (van Vliet et al., 1993). This phenomenon is called stress concentration. For fast fracture to occur, two requirements should be fulfilled. Firstly, the stress at the tip of the cracks should be higher than the adhesive or cohesive stresses between the structural elements. This will sooner be the case as the size of the cracks and inherent defects in the material is larger. Once this requirement is fulfilled, the cracks start to grow. Secondly, the amount of strain energy released per unit time during crack growth should be higher than the amount of energy required for crack growth. If this requirement is also fulfilled, fast crack propagation will occur and the material will fracture.

5.2.2 Large deformation properties of different types of gels

Polymer and particle gels respond differently to changes in deformation rate (van Vliet et al., 1995). Moreover, polymer gels with covalent cross-links and gels with physical crosslinks also respond differently. For both types of gels, the way in which they fracture depends on the gel structure and the strength of the bonds. Homogeneous polymer gels with stochastically distributed covalent cross-links have no inherent defects larger than the distance between the cross-links, and therefore behave purely elastically during deformation. Furthermore, due to the low permeability of these gels, the energy dissipation rate due to flow of liquid through the matrix will be low. Therefore, the fracture properties of these gels are almost independent of the deformation rate. For polymer gels with physical cross-links, such as gelatine gels, large deformation may lead to unzipping of the cross-links. Unzipping takes a certain time, and this may result in timedependency of the fracture parameters. For gelatine gels, fracture stress and strain both depend on deformation rate. Both parameters initially decrease with increasing deformation speed at speeds lower than 2 mm/s and at higher speed increase (McEvoy, Rossmurphy & Clark, 1985). In a study on the effect of several experimental parameters on the large deformation properties of gelatine gels Bot et al. (1996a, 1996b) found an increase in fracture stress and strain with increasing compression speed (0.0016-0.83 mm/s) and no effect of the compression speed on the modulus.

In particle gels, such as casein and whey protein gels, the storage modulus and the loss modulus depend on the type of bonds connecting the particles within one cluster, as well as those connecting the different clusters (Mellema, Walstra, van Opheusden & van Vliet, 2002). Clusters can be connected by (i) flexible strands, (ii) hinged connections or (iii) straight strands. Straight strands will result in stiffer gels. Large deformations of particle gels will induce straightening of the strands. Therefore, the flexibility and tortuosity of the strands will have a larger effect on the Young's modulus than on the fracture stress. Moreover, the flexibility and tortuosity of the strands, as well as the deformability of the particles during deformation, will affect the fracture strain. Flexible strands and deformable particles will result in higher fracture strains.

5.2.3 Rheological properties of the gels studied

The ratio between the energy dissipated as viscous flow and the energy elastically stored can be expressed by the ratio between loss modulus (G'') and the storage modulus (G') as determined in dynamic sinusoidal oscillation test in the linear region (van Vliet et al., 1993). This ratio is known as the loss or damping factor or tan δ . Even though the validity of tan δ is limited to the linear region, this parameter can help in the interpretation of phenomena observed at large deformation.

Gelatine gels are typically elastic polymer gels of flexible, random coil protein chains. For gelatine gels the linear region is up to strains of about 0.5 and the gels break at true fracture strains of 1-1.5. For gelatine tan δ of 0.01 and lower were reported (Takahashi, Myojo, Yoshida, Yoshimura & Hattori, 2004). Kappa-carrageenan gels are also elastic polymer gels of stiff, rather straight chains with a linear region below a strain of 0.1. These gels break at true fracture strains of 0.4-0.5. For κ -carrageenan gels prepared in demineralised water tan δ increased from 0.07 to 0.09 when the gelling agent concentration was increased from 0.3 to 1.2 wt% (Bayarri, Duran & Costell, 2004). Acidinduced, cold set WPI gels are typically viscoelastic particle gels, with a relatively small viscous component (tan $\delta \approx 0.14$). The linear region is up to a true strain of 0.1 (Rosa, Sala, van Vliet & van de Velde, 2006).

5.2.4 Effect of compression speed on Young's modulus and fracture properties

The effects of the compression speed on Young's modulus and fracture properties of gels can be explained on the basis of a set of basic physical phenomena related to their viscoelastic character and taking into account the energy balance discussed above.

For gels behaving elastically, the energy supplied during deformation is stored in the gel network and provides the stresses required to regain the original shape after removing the deformation. In this case no energy dissipation occurs as a result of relaxation of cross-links/ bonds due to thermal movement. Therefore, the Young's modulus does not change with increasing compression speed. In viscoelastic gels bonds relaxation due to thermal movement, leading to energy dissipation on deformation, will occur already in the linear region. The compression speed dependency of the Young's modulus of viscoelastic gels indicates a more viscous behaviour at low deformation speed (**mechanism A**). This behaviour can be visualised by the Maxwell rheological model, consisting of a combination of an elastic spring and a viscous dashpot in serial connection. When the combination of these two elements is stressed over a short timescale, the resulting deformation is mainly due to the elongation of the spring (van Vliet, 1999). Stressing the combination of the two elements over a longer timescale results in a deformation due to the displacement of the piston in the dashpot. In other words, when applying high deformation speeds, the system will behave more elastically. When low deformation speeds are applied, the system will show a more viscous character. In this second case, part of the energy supplied to the system will be dissipated for the relaxation of cross-links/bonds. As a result, measurements performed at low deformation speed will give lower values of the Young's modulus.

The presence of structural inhomogeneities and defects in the gel network induces stress concentration upon deformation (**mechanism B**) (Luyten, Ramaker & Vliet, 1992; van Vliet et al., 1993; van Vliet et al., 1995). This occurs at the tip of cracks or at the surface of tiny holes. Stress concentration phenomena will result in a lower fracture stress and fracture strain and will be more important in particle gels, which contain relatively more structural defects. For viscoelastic material, deformation causes blunting of the crack tips until the stress required for crack propagation is reached. At higher deformation speed the blunting of the crack tips will be less, leading to (slightly) faster crack propagation.

Upon deformation viscous flow additional to that described by mechanism A may occur as a result of local yielding, leading to energy dissipation (**mechanism C**) (Luyten et al., 1992; van Vliet et al., 1993; van Vliet et al., 1995). This energy dissipation will also be relatively more important at low deformation speed, but absolutely higher at high deformation speeds. This leads to lower fracture strain and higher fracture stress at higher deformation speed. With regard to the studied gels, the energy dissipation for viscous flow will be more relevant for particle gels as compared to the polymer gels.

Energy dissipation also occurs due to friction processes between structural elements of the gel network (Luyten et al., 1992; van Vliet et al., 1993; van Vliet et al., 1995). Energy dissipation by friction processes will be relatively higher at higher

deformation speeds, compared with the other terms in equation 5.1. This gives higher fracture strain and higher fracture stress at higher deformation speed (crack growth takes time) (mechanism D).

For polymer gels with physical cross-links (e.g. gelatine gels), unzipping of physical cross-links and formation of new bonds can be regarded as a kind of viscous flow as a result of (local) yielding under stress and gives somewhat higher fracture strain and fracture stress at higher deformation speed (mechanism E) (McEvoy et al., 1985).

Table 5.2 shows a summary of the mechanisms explaining the effect of compression speed on Young's modulus and fracture properties.

Table 5.2 – Mechanisms related to the compression speed and affecting the large deformation behaviour in the gels studied.

	Affected parameter		
-	$\sigma_{ m f}$	٤ _f	$\mathbf{E}_{\mathbf{y}}$
A: viscoelastic behaviour			++
B: stress concentration	-	-	
C: induced viscous flow of the matrix	+	-	
D: friction between structural elements	++	++	
E: unzipping of physical bonds*	+	+	

 σ_{f} : fracture stress; ϵ_{f} : fracture strain; Ey: Young's modulus. + denotes an increase of the parameter with speed. - indicates a decrease of the parameter. More + or – correspond to a stronger effect. *: relevant for gelatin at low compression speed.

5.2.5 Effect of the volume fraction of the droplets on Young's modulus and fracture properties

The presence of the oil droplets in the gel matrix affects all the phenomena described in the previous section. Moreover, the oil droplets will affect the gel modulus, in a way which will depend on the interaction between the oil droplets and the gel matrix. The effect of the oil droplets on the Young's modulus can be explained by van der Poel theory plus extensions (**mechanism F**) (van der Poel, 1958; Smith, 1974, 1975; van Vliet, 1988; Sala et al., 2007).

Oil droplets embedded in a gel network represent structural defects which induce stress concentration upon deformation (mechanism B) (Luyten et al., 1992; van Vliet et al., 1993; van Vliet et al., 1995). An increase in φ represent an increase of the number of structural defects. At small deformation and for spherical holes the effective stress will increase by a factor 3. For large deformations the situation becomes more complex. For droplets less deformable than the gel matrix and bound to the matrix, the region between the droplets will be extended more than the gel matrix at the sides of the droplets. This gives stress concentration between the droplets and there the gel will start to fracture as a result of de-bonding of the gel matrix from the droplets or due to fracture of the gel matrix itself. This will result in lower fracture strain and lower fracture stress with increasing φ for bound droplets (mechanism B1). For unbound droplets fracture is likely to occur at the droplet gel matrix interface. Besides, for unbound droplets and especially at low deformation speeds, the extent of stress concentration between the droplets will be smaller since the gel matrix can move more freely with respect to the hard droplets (nevertheless the droplets are not completely free due to friction effects). For unbound droplets this will result in lower fracture strain and lower fracture stress with increasing φ , but the effect will be smaller than for bound droplets (mechanism B2). The deformation speed effect will give lower fracture strain and fracture stress at higher speeds.

If droplets are present in a gel matrix, viscous flow (**mechanism C**) is likely to locally be more intense (Luyten et al., 1992; van Vliet et al., 1993; van Vliet et al., 1995). Therefore, the energy dissipation due to viscous flow and the related dependency on compression speed will increase. Boundary layers between droplets and matrix can be relatively more viscous (van Vliet, 1988). The volume involved is small but may still have an effect on stress.

The presence of oil droplets embedded in the gel matrix also affects the friction phenomena occurring upon deformation (**mechanism D**) (Luyten et al., 1992; van Vliet et al., 1993; van Vliet et al., 1995). As a result of inhomogeneous deformation of the gel, causing displacement of the gel matrix with respect to the droplet surfaces, the energy dissipated by friction will increase in filled gels as compared to gels without oil droplets.

Table 5.3 shows a summary of the mechanisms explaining the effect of φ on Young's modulus and fracture properties.

	Affected parameter					
-	Bound droplets (1)		Unbound droplets (2)		s (2)	
-	σ_{f}	ε _f	Ey	σ_{f}	ε _f	Ey
F: van der Poel			+++*			
B: stress concentration						
C: induced viscous flow of the matrix	+	-		+	-	
D: friction filler/ matrix				++	++	

Table 5.3 – Mechanisms affecting the large deformation properties of emulsion-filled gels related to the presence of oil droplets in the gel matrix.

 σ_f : fracture stress; ϵ_f : fracture strain; Ey: Young's modulus. + denotes an increase of the parameter with ϕ . - indicates a decrease of the parameter. More + or – correspond to a stronger effect. *: assuming $E_{filler} >> E_{matrix}$.

5.2.6 Strain dependency of the modulus

For several polymeric materials, the stress upon deformation increases more than linearly with strain, a phenomenon known as strain-hardening. Various molecular theories were discussed to explain the strain dependency of the modulus of polymer gels and were compared to experimental results obtained for gelatine gels (Groot, Bot & Agterof, 1996). The molecular structure of a gel was described in terms of cross-links connected by entropic springs. The strain-hardening of gelatine gels could be explained by several mechanisms: a finite polymer length, a fractal nature of the polymer strands, the presence in the gel network of both stiff rods and swollen coils or strain-induced crystallisation. Strain-hardening was also observed for heat-set β -lactoglobulin gels, i.e. particle gels (Pouzot, Nicolai, Benyahia & Durand, 2006). In this case the experimental data were well described by a model of interconnected fractal clusters with randomly oriented elastic backbones. Deformation would induce the elongation of the backbones. As a consequence, each structural unit would redistribute into more structural units of smaller size. The strain-hardening was found to decrease with increasing gel modulus, until for gels with G' higher than 2 kPa no strain-hardening was observed.

5.3 Materials and methods

5.3.1 Materials

Porcine skin gelatine PBG 07 (bloom 280, isoelectric point 8-9) was kindly provided by PB gelatines (Vilvoorde, Belgium). Kappa-carrageenan was kindly donated by CP Kelco (Lille Skensved, Denmark). The κ -carrageenan sample consisted of 93% mol κ -units and 7% mol ι -units, as determined by NMR spectrometry (van de Velde, Pereira & Rollema, 2004). Powdered whey protein isolate (WPI, BiproTM) was obtained from Davisco International Inc. (La Sueur, MN, USA). Tween 20 (Polyoxyethylene sorbitan monolaurate, in the text referred to as Tween) was obtained from Sigma (Sigma-Aldrich Chemie BV, Zwijndrecht, The Netherlands). Lactoferrin were kindly donated by DMV International, (Veghel, The Netherlands). Medium Chain Triglycerides (MCT, MIGLYOL 812N) oil was purchased from Internatio BN (Mechelen, Belgium). Potassium chloride (p.a.) was obtained from Merck (Darmstadt, Germany). Glucono- δ -lactone (GDL) was kindly donated by Purac (Gorinchem, The Netherlands). All materials were used without further purification. All solutions were prepared with demineralised water.

5.3.2 Sample preparation

5.3.2.1 <u>Emulsions</u>

WPI solutions were prepared by adding the protein to the required amount of water. Subsequently, the solutions were gently stirred for 2 hours. Stock emulsions, consisting of 40 wt% MCT oil and 60 wt% aqueous phase containing 1 wt% WPI, were prepared by pre-homogenising the ingredients using an Ultra Turrax (Polytron, Kinematica AG, Lucerne, Switzerland). Pre-emulsions were further processed using a laboratory homogeniser (Ariete, Model NS1001L 2K – Panda 2K, Niro Soavi S.p.A, Parma, Italy). The same procedure was used for the preparation of the emulsions stabilised with Tween and lactoferrin, only the emulsifying agent concentration in the aqueous phase was 2 wt%. WPI-stabilised emulsions were used for the preparation of filled gelatine and κ -carrageenan gels. Tween-stabilised emulsions were used for the preparation of filled κ -carrageenan gels. KCl was added to the emulsions used for the preparation of κ -carrageenan gels, up to a concentration of 30 mM in the aqueous phase. Emulsions stabilised with WPI aggregates were prepared as described above, but using a 3 wt% WPI aggregates dispersion as continuous phase. This dispersion was prepared by heating a 9 wt% WPI solution at 68.5°C for 2 hours and subsequent cooling to room temperature with tap water and diluting to 3 wt%. WPI aggregates-stabilised emulsions were used for the preparation of filled WPI gels.

The droplet size distribution of the obtained emulsions was measured using a Malvern Mastersizer 2000 (Malvern Instruments Ltd., Malvern, UK). The droplet volume-surface average or Sauter diameter $(d_{3,2})$ and other characteristics of the emulsions used for the preparation of the filled gels are reported in Table 5.4.

Emulsifier in the water phase	d _{3,2} (μm)	G' droplet (kPa)	E _y droplet (kPa)	рН
1 wt% WPI	1.15	69	207	7.06
2 wt% Tween	1.00	20	60	4.30
2 wt% Lactoferrin	1.85	43	129	5.10
3 wt% WPI aggr.	1.45	55	165	6.64

Table 5.4 – Volume-surface average diameter (Sauter diameter) and pH of the emulsions used forthe preparation of the filled gels.

The G'of the droplet was calculated by G'= $4\gamma/d$ whereby the surface tension γ was taken to be 20 mN/m for protein stabilised droplets and 5 mN/m for Tween stabilised droplets. $E_v = 3G'$.

5.3.2.2 <u>Gels</u>

Gelatine (4 wt%) and WPI (3 wt%) gels were prepared in demineralised water. Kappacarrageenan (0.6 wt%) gels were prepared in a 30 mM KCl solution. Samples were prepared without emulsion and with different φ (0.05, 0.11, 0.21 corresponding to oil concentrations of 5, 10 and 20 wt%). In all samples the concentration of the gelling agent in the aqueous phase was kept constant.

For κ -carrageenan and gelatine gels, the gelling agent was allowed to hydrate for 2 hours under gentle stirring at room temperature. The samples were subsequently dissolved by heating at 80°C for 30 minutes and cooled to 45°C. In the case of κ -carrageenan gels, the emulsion was heated to 45°C prior to addition to the gelling agent solution. For

gelatine gels, the gelling agent solution was allowed to cool to 20° C prior to mixing with the emulsion. This procedure was followed to prevent depletion flocculation of the emulsion droplets before gel formation (Sala et al., 2007). After mixing, the samples were allowed to gel at room temperatures in 60 ml plastic syringes (internal diameter 26.4 mm) coated with a thin film of paraffin oil. Gelatine gels containing Tween-stabilised emulsions were allowed to gel in a refrigerator (7°C) for 6 hours before analysis.

Gelation of the WPI gels was induced by addition of GDL (0.22 wt% in the case of WPI aggregates dispersion with a concentration of 3 wt%) to the WPI dispersion and to the WPI dispersion/emulsion mix and incubation at 25°C for 17 hours. The WPI dispersion was prepared as described above. The final pH of the gels was about 4.8.

5.3.3 Large deformation experiments

Uni-axial compression tests were performed on gel pieces of 25 mm height using an Instron universal testing machine (Model 5543, Instron International Ldt., Edegem, Belgium) equipped with a plate-plate geometry. In order to prevent friction between the plates and the samples, the plates were lubricated with a thin layer of paraffin oil. The compression was up to a strain of 80% at different constant deformation speeds: 0.05, 0.1, 0.5, 1, 2 and 4 mm/s. The true strain ($\epsilon_{\rm H}$), i.e. the absolute deformation of the specimen, and the true stress ($\sigma_{\rm t}$), i.e. the overall stress acting on the sample during deformation, were calculated as follows:

$$\varepsilon_{H} = \int_{H_{0}}^{H} \frac{1}{H} dH = \ln\left(\frac{H}{H_{0}}\right)$$
(5.2)

$$\sigma_{t} = \frac{F}{A} \tag{5.3}$$

where H_0 is the initial height of the specimen, H the actual height after deformation, F the force measured during compression and A the corresponding cross-sectional area of the specimen.

The determination of the recoverable energy (RE) was done by compressing the samples up to a strain of 25% at deformation speeds of 1 and 4 mm/s. The work necessary to compress the samples to the mentioned strain was recorded (W_c), whereby the work was calculated from the area below the stress vs. strain curve directly after reaching a strain of 25%. Hereafter, the compression was removed at the same speed applied during

deformation and the work released by the gel specimen was immediately recorded (W_s). The results were expressed as

$$RE = \frac{W_s}{W_c}$$
(5.4)

5.3.4 Confocal Laser Scanning Microscopy (CLSM)

Samples for microstructural analyses were stained with Rhodamine B (0.2 wt% solution; 10 μ L per mL sample) to visualise the protein phase. Nile Blue was chosen as staining agent of the oil droplets. CLSM-images were recorded on a LEICA TCS SP Confocal Laser Scanning Microscope (Leica Microsystems CMS GmbH., Manheim, Germany), equipped with an inverted microscope (model Leica DM IRBE), used in the single photon mode with an Ar/Kr visible light laser. A Leica objective lens (63x/UV/1.25NA/water immersion/PL APO) was used. The excitation wavelength was set at 568 nm for Rhodamine B and at 488 nm for Nile Blue. Digital image files were acquired in tagged image file format and at 1024x1024 pixel resolution.

5.4 Results

5.4.1 Effect of compression speed on Young's modulus and fracture parameters

For all gels, variations in the compression speed affected at least one of the measured parameters. For the polymer gels (gelatine and κ -carrageenan), no effect of compression speed was observed on the Young's modulus (Figures 5.1A, 5.2A, 5.3A, 5.4A, diamond symbol). However, a clear effect of compression speed was found on fracture stress (Figures 5.1B, 5.2B, 5.3B, 5.4B diamond symbol) and fracture strain (Figures 5.1C, 5.2C, 5.3C, 5.4C, diamond symbol). The effect of speed on fracture stress and fracture strain slightly differed between gelatine and κ -carrageenan gels. For gelatine gels, a gradual and continuous increase of both fracture parameters was observed with compression speeds. For κ -carrageenan gels, an increase was observed up to a speed of 1 mm/s. At higher speed the fracture parameters did not increase further. The effect of compression speed on the large deformation properties of gelatine gels is in agreement with the results published

in literature (van Vliet et al., 1995; Bot, van Amerongen, Groot, Hoekstra & Agterof, 1996b, 1996a).

For particle gels (WPI gels), the effect of compression speed was different from that described for the polymer gels. For WPI gels, the Young's modulus increased with increasing compression speed up to a speed of 1 mm/s, above which the value of the modulus did not increase any further (Figure 5.5A). With increasing compression speed also the fracture stress increased (Figure 5.5B). On the other hand, no effect of compression speed on fracture strain was observed (Figure 5.5C).

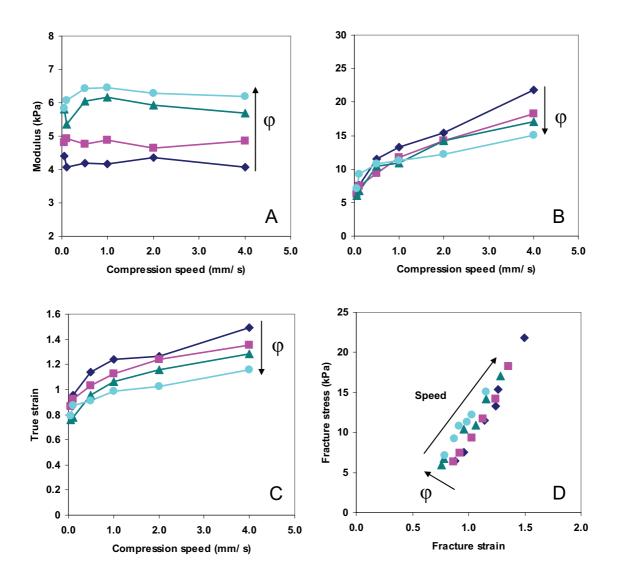


Figure 5.1 – Gelatine bound: effect of compression speed and φ on Young's modulus (A), fracture stress (B), fracture strain (C) and fracture points (D) (\diamond : 0.0 oil; \blacksquare 0.05 oil \blacktriangle : 0.11 oil; \diamond : 0.21 oil). The arrow close to the symbol φ indicates the increase of φ in the samples.

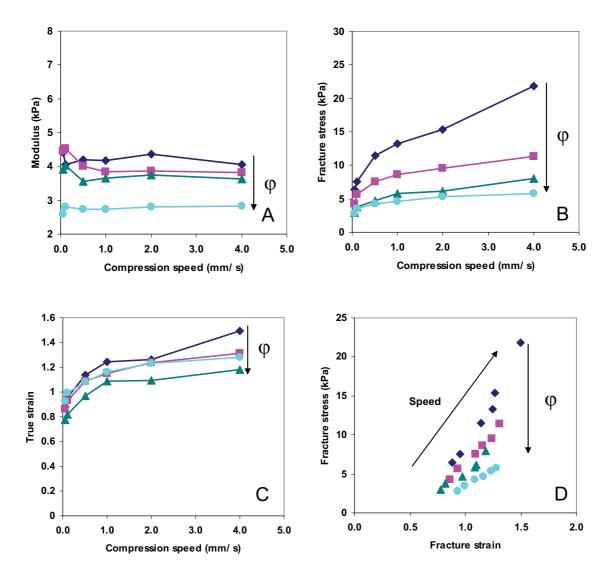


Figure 5.2 – Gelatine unbound: effect of compression speed and φ on Young's modulus (A), fracture stress (B), fracture strain (C) and fracture points (D) (\diamond : 0.0 oil; \blacksquare 0.05 oil \blacktriangle : 0.11 oil; \bullet : 0.21 oil). The arrow close to the symbol φ indicates the increase of φ in the samples.

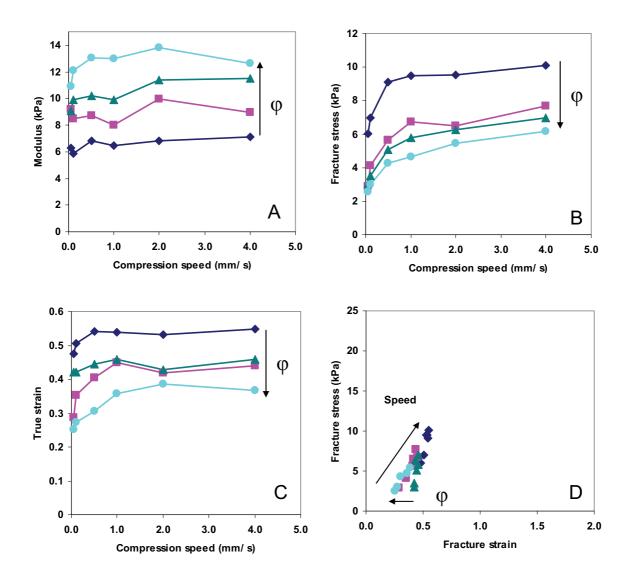


Figure 5.3 - Kappa-carrageenan bound: effect of compression speed and φ on Young's modulus (A), fracture stress (B), fracture strain (C) and fracture points (D) (\diamond : 0.0 oil; \blacksquare 0.05 oil \blacktriangle : 0.11 oil; \bullet : 0.21 oil). The arrow close to the symbol φ indicates the increase of φ in the samples.

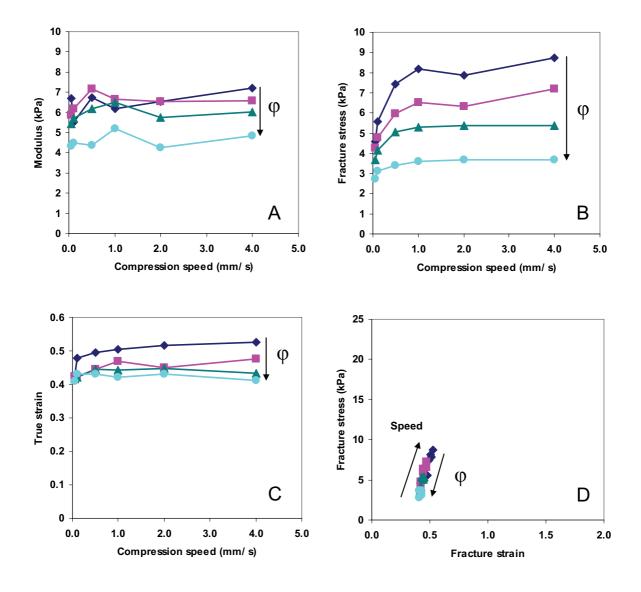


Figure 5.4 - Kappa-carrageenan unbound: effect of compression speed and φ on Young's modulus (A), fracture stress (B), fracture strain (C) (\diamond : 0.0 oil; \blacksquare 0.05 oil \blacktriangle : 0.11 oil; \bullet : 0.21 oil). The arrow close to the symbol φ indicates the increase of φ in the samples.

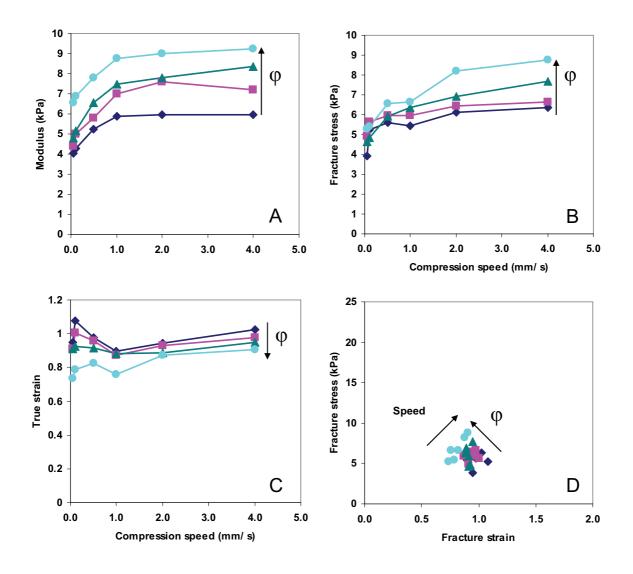


Figure 5.5 – WPI bound: effect of compression speed and φ on Young's modulus (A), fracture stress (B), fracture strain (C) and fracture point (D) (\diamond : 0.0 oil; \blacksquare 0.05 oil \blacktriangle : 0.11 oil; \diamond : 0.21 oil). The arrow close to the symbol φ indicates the increase of φ in the samples.

5.4.2 Droplet-matrix interactions and oil droplet aggregation in emulsion-filled gels

By varying the emulsifying agent used for emulsion preparation, the interactions between oil droplets and gel matrix could be modulated. For the polymer gels studied, samples with bound as well as unbound droplets could be prepared. For the studied particle gels, only samples with bound droplets could be prepared. As previously reported (Sala et al., 2007), the addition of a WPI-stabilised emulsion to gelatine gels resulted in filled gels containing bound droplets, whereas with the same gel matrix a Tween-stabilised emulsion gave filled gels containing unbound droplets. WPI-stabilised emulsion droplets in κ carrageenan gels also behaved as unbound droplets (Sala et al., 2007). For the present work, lactoferrin-stabilised emulsions were added to k-carrageenan in order to obtain filled gels with bound droplets. At the pH of the filled κ -carrageenan gels (7-8), lactoferrin displays a positive net charge, while κ -carrageenan is negatively charged. As a consequence, the interactions between the oil droplets and the gel matrix are expected to be attractive. These interactions indeed manifested themselves by an increase of the Young's modulus with increasing φ in compression measurements (Figure 5.3A). For κ carrageenan samples without oil droplets but containing the same amount of lactoferrin as filled gels with $\varphi = 0.21$, an increase in the Young's modulus by 20% was observed. This increase was comparable to that observed for gels with $\varphi = 0.05$. Furthermore, no effect of lactoferrin was observed on the fracture stress and fracture strain (results not shown). Therefore, the effect of lactoferrin present in the water phase of the added lactoferrinstabilised emulsion on the studied parameters could be neglected. For WPI gels, filled gels with bound droplets were prepared by using a WPI aggregates-stabilised emulsion for sample preparation (Rosa et al., 2006).

The microstructure of the gels studied, with the exception of gelatine gels with unbound droplets and κ -carrageenan gels with bound droplets, has been described previously (Sala et al., 2007; Sala, De Wijk, van de Velde & van Aken, 2008). The procedure chosen for the preparation of gelatine gels with bound droplets resulted in gels with non-aggregated oil droplets. For κ -carrageenan gels containing WPI-stabilised emulsions, extensive aggregation of the oil droplets was observed, whilst the oil droplets embedded in WPI gels were homogeneously distributed. Also for gelatine gels with unbound droplets, the oil droplets were non-aggregated or only slightly aggregated (Figure 5.6A), while the lactoferrin-stabilised oil droplets present in κ -carrageenan gels were extensively aggregated (Figure 5.6B).

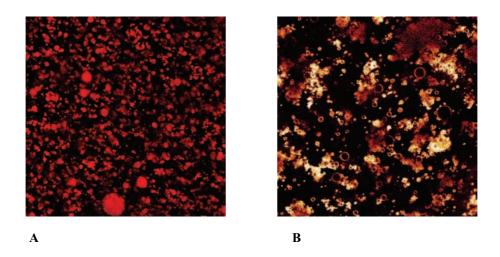


Figure 5.6 - CLSM images of a gelatin gel containing a Tween 20-stabilised emulsion (A; staining agent: Nile blue; bright: fat) and a κ -carrageenan gel containing a lactoferrin-stabilised emulsion (B; staining agent: Rhodamine B; bright: protein) (φ : 0.21; image size 159 X 159 μ m).

In κ -carrageenan gels with lactoferrin-stabilised emulsions, the aggregation of the oil droplets is likely to be driven by electrostatic bridging between the protein adsorbed at the oil-water interface and the polymer present in solution. For the chosen emulsions, the aggregation of the oil droplets in the κ -carrageenan gels could not be prevented. In chapter 3 (Sala et al., 2007) we showed that the aggregation of the oil droplets has mainly an effect on the Young's modulus of the filled gels and does not affect their fracture properties. The aggregation of the oil droplets represents an increase of the effective φ due to the matrix entrapped within the aggregate. In case the stiffness of the aggregates is higher than the Young's modulus of the gel matrix, this results in an increase of the Young's modulus of the filled gels. At the contrary, if the stiffness of the aggregates is lower than the Young's modulus of the gel matrix, the increase in effective φ caused by oil droplet aggregation induces a decrease in the Young's modulus of the filled gel. The effect of aggregation on the Young's modulus can be assumed to be constant with increasing φ . Moreover, droplet aggregation occurred in both gels with bound and unbound dropelts. Therefore, in this work the variations in the large deformation properties of κ -carrageenan gels caused by oil droplet aggregation were not investigated in detail. In chapter 6 more attention will be paid to the effects of aggregation phenomena.

5.4.3 Effect of the oil volume fraction on Young's modulus and fracture parameters

For all gels, the effect of φ on the Young's modulus depended on the interaction between the oil droplets and gel matrix. In accordance with the van der Poel theory, the Young's modulus increased with increasing φ for gels with bound droplets (Figures 5.1A, 5.3A and 5.5A) and decreased for unbound droplets, (Figures 5.2A and 5.4A). The presence of oil droplets did not affect the speed dependency of the Young's modulus of the gels.

Focussing on the effect of oil droplets on fracture parameters, differences were observed between the way gelatine and κ -carrageenan gels react to a variation in compression speed. For gelatine gels with bound droplets, the effect of φ on fracture stress was small for compression speeds up to 1 mm/s. Above this speed, an increase of φ resulted in a decrease of the fracture stress (Figure 5.1B); this effect of φ on fracture stress at higher compression speed was just the reverse of that on the Young's modulus. For gelatine gels with unbound droplets (Figure 5.2B), a clear decrease of fracture stress with increasing φ was also observed, but it started already at compression speed of 0.1 mm/s. Also for k-carrageenan gels the effect of oil content was already visible at compression speeds above 0.05 mm/s both for bound and unbound droplets (Figure 5.3B and 4B). For these gels, a decrease of the fracture stress with increasing φ was observed for both bound and unbound droplets. For both gelatine and κ -carrageenan gels a decrease of the fracture strain with increasing concentration of bound droplets was found (Figure 5.1C, 5.3C). The effect of φ was larger at higher compression speeds, but was already clear at lower speed. A decrease of the fracture strain with increasing φ was also observed for κ -carrageenan gels with unbound droplets (Figure 5.4C). For gelatine gels with unbound droplets (Figure 5.2C), the decrease of fracture strain caused by the presence of the oil droplets was only minor and not systematically related to φ . For WPI gels with increasing φ , the fracture stress slightly increased (Figure 5.5B) and the fracture strain somewhat decreased (Figure 5.5C).

Graphs of the fracture point (defined as the maximum in the stress-strain curve) at different compression speeds and for samples with different φ present the above given information in an efficient way (Figures 5.1-5.5, panels D). These graphs clearly show how the effect of φ on fracture properties depends on the interactions between oil droplets and gel matrix. Furthermore, they demonstrate that the effect of compression speed and φ on fracture parameters is gel-dependent. For gelatine gels with bound droplets (Figure 5.1D), the fracture points of emulsion-filled gels fall above those of the gels without oil.

For gelatine gels with unbound droplets (Figure 5.2D), the fracture points of emulsionfilled gels fall below those of the gels without oil. For gels with unbound droplets, the slope of curves connecting the fracture points of samples with the same φ decreased. This corresponds to a decreasing effect of compression speed on fracture stress with increasing φ . Also for κ -carrageenan gels, the fracture points of emulsion-filled gels with bound droplets fall above those of the gels without oil (Figure 5.3D), whereas the fracture point of gels with unbound droplets fall below those of the gels without oil (Figure 5.4D). However, for these gels the effect of both compression speed and φ on fracture parameters was smaller than for the gelatine gels. The graph obtained for WPI gels was different from those for the polymer gels. For WPI gels, only a limited effect of compression speed was observed (Figure 5.5D).

For gelatine gels, the overall effect of emulsion droplets on fracture stress and strain was similar to that reported for gelatine gels containing whey protein particles (Bot et al., 1996a) although we studied a much larger filler concentration range and performed compression measurements over a larger speed range. The similarity of our results and those of Bot et al. means that the effect of oil droplets on the fracture properties of these gels can be mimicked by whey protein particles.

The strengthening of WPI gels with increasing concentration of oil droplets stabilised by WPI aggregates is in accordance with the results obtained by other authors for heat-induced whey protein gels containing whey protein stabilised emulsions (Langley & Green, 1989; (Xiong, Aguilera & Kinsella, 1991a; Xiong & Kinsella, 1991b); McClements et al., 1993).

5.4.4 Strain-dependency of the Young's modulus

In order to better understand the effect of oil droplets on the structural and functional properties of emulsion-filled gels, an analysis of the effect of both φ and compression speed on the strain-dependency of the modulus of the gels was carried out. The strain-hardening behaviour of the studied gels can be seen from the increase in the slope of the stress vs. strain curves with increasing compressive strain (Figure 5.7). The behaviour of the three gels was remarkably different. Both the polymer gels studied showed strain-hardening, with differences between the two gels related to the different structure of their gel network. For gelatine, two main parts could be recognised in the stress vs. strain curve

(Figure 5.7). At low strain (up to about 0.6), the effect of the strain on the modulus (the slope of the stress vs. strain curve) was relatively limited. At higher strains, the slope of the curve increased and flattened on approaching the fracture point. For κ -carrageenan gels, a sudden increase of the slope of the stress vs. strain curve was observed at strains between 0.1 and 0.2 (Figure 5.7). At higher strain the slope of the curve did not change. In κ -carrageenan gels the polymer chains are less flexible, less random coil-like, more straight and stiff than in gelatine gels, resulting in a fast increase of the modulus with increasing strain. This can explain the difference observed between the two gels. On the other hand, the modulus of WPI gels did not change with increasing strain (Figure 5.7). These gels were not strain-hardening.

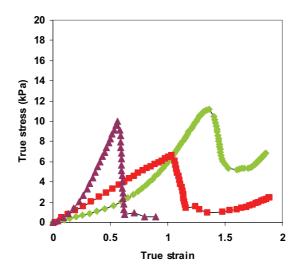


Figure 5.7 – Stress vs. strain curves of gelatine (\blacklozenge), WPI (\blacksquare) and κ -carrageenan gels (\blacktriangle) (compression speed: 4 mm/s).

The effect of φ on strain-hardening behaviour was studied by superimposing the fracture vs. strain curves of gels with different φ and observing possible deviations in the slope of the curves as compared to the curves of gels without oil (Figure 5.8). The curves were superimposed by dividing the stress along the stress vs. strain curve by the Young's modulus. The obtained stress is dimensionless and was called normalised stress. Figure 5.8 shows the results for κ -carrageenan gels (the results for gelatine gels are not shown). For both polymer gels studied, the slope of the normalised stress vs. strain curve was not affected by φ and decreased with increasing φ only as the fracture point was approached (Figure 5.8A). This effect was not affected by the compression speed (compare Figures

5.8A and 5.8B) and was more evident for gels with bound droplets (compare Figures 5.8A and 5.8C). Actually, the observed decrease of the slope of the normalised stress vs. strain curve does not show an effect of the oil droplets on strain-hardening. As the fracture point is approached, small cracks originated at the surface of the oil droplets will propagate and join within the gel structure, resulting in a overall decrease of the measured stress. This effect will increase with increasing φ and is in agreement with the observed effect of φ on fracture stress and fracture strain. For WPI gels, which did not show strain-hardening, no effect of φ and compression speed was observed (results not shown). In conclusion, under the chosen experimental conditions φ and compression speed did not affect the strain-hardening behaviour of the studied gels.

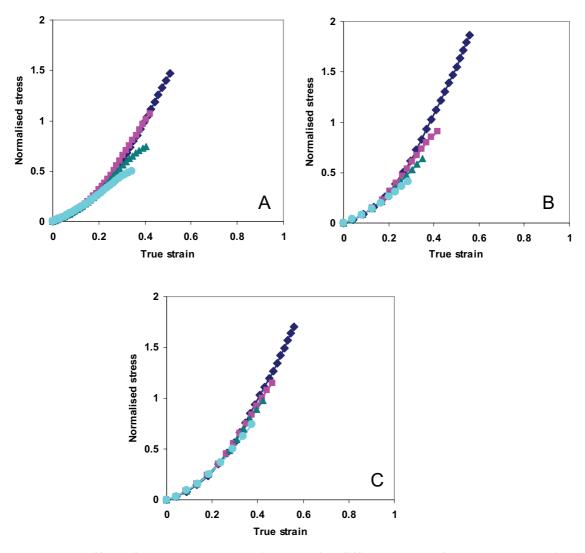


Figure 5.8 - Effect of φ on stress vs. strain curve for different types of κ -carrageenan gels at different deformation speeds. A: bound droplets, 1 mm/s. B: bound droplets, 4 mm/s. C: unbound droplets, 1 mm/s. (\diamond : 0.0 oil; \blacksquare 0.05 oil \blacktriangle : 0.11oil; \diamond : 0.21oil).

5.4.5 Recoverable energy

The energy released by a gel specimen after removing a previously applied deformation gives an indication of the viscoelastic behaviour of the gel. The lower the energy recovered, the more viscous the gels. The effect of φ on recoverable energy differed not only between particle and polymer gels, but also between the different polymer gels. For WPI gels, a gradual decrease of the recoverable energy was observed with increasing φ (Figure 5.9). An increase in φ resulted in less elastic and more viscous gels. For gelatine gels with bound droplets, no effect of φ on recoverable energy was found, independently of the compression speed. However, for gelatine gels with unbound droplets, a clear decrease of the recoverable energy was observed with increasing φ . At higher compression speed this decrease was even larger. Since φ in gelatine gels with unbound droplets did not affect the fracture strain (Figure 5.4C), it can be concluded that an increase of φ in these gels made them less elastic at large deformation. For κ -carrageenan gels, the effect of φ on recoverable energy was relatively small.

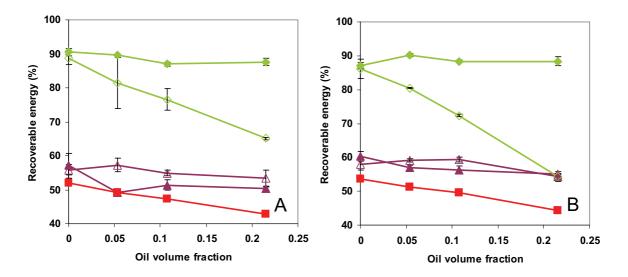


Figure 5.9 - Effect of φ on recoverable energy for different gels. \blacklozenge : gelatine gels with bound droplets; \Diamond : gelatine gels with unbound droplets; \blacktriangle : κ -carrageenan gels with bound droplets; \blacktriangle : κ -carrageenan gels with unbound droplets; \blacksquare WPI gels with bound droplets. (A): compression speed 1 mm/s. (B): compression speed 4 mm/s.

5.5 Discussion

The data currently available in literature on the large deformation and fracture properties of emulsion-filled gels are often inconclusive and are sometimes contradictory. The reason of this lack of coherency is that previous studies have usually focussed on one particular gel system. Moreover, large deformation and fracture measurements have normally been performed only at one deformation speed, whereby the applied deformation speed has almost in all cases been lower than 1 mm/s. In the present study we included different gel systems, covering a representative set of cases with regard to type of gel matrices and interaction between oil droplets and gel matrix. By measuring the effect of φ at different compression speeds, an overview could be obtained of the effect of oil droplets on the large deformation and fracture properties of the gels (Tables 5.5 and 5.6).

Table 5.5 – Summary of the results	s with respect to the effect	of speed.
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-	Compression speed			
Type of gel	$\sigma_{ m f}$	ε _f	$\mathbf{E}_{\mathbf{y}}$	RE
Gelatine bound	+++	+++	0	0
Gelatine unbound	+	+	0	-
к-carrageenan bound	+++	+++	0	0
к-carrageenan unbound	+	+	0	0
WPI bound	++	0	+++	0

 σ_{f} : fracture stress; ϵ_{f} : fracture strain; E_{y} : Young's modulus. + denotes an increase of the parameter with speed. - indicates a decrease of the parameter. More + or – correspond to a stronger effect. 0: no effect.

			φ	
Type of gel -	$\sigma_{\rm f}$	ε _f	Ey	RE
Gelatine bound			+++	0
Gelatine unbound				
к-carrageenan bound			++	-
к-carrageenan unbound				-
WPI bound	++		+++	

Table 5.6 – Summary of the results with respect to the effect of $\boldsymbol{\phi}.$

 σ_f : fracture stress; ϵ_f : fracture strain; E_y : Young's modulus. + denotes an increase of the parameter with ϕ . - indicates a decrease of the parameter. More + or – correspond to a stronger effect. 0: no effect.

Compression measurements over a wide range of deformation speeds provided basic information on the mechanical behaviour of the gel, which was useful for the interpretation of the effect of oil droplets on the mechanical properties of the gels. Measurements at high compression speeds showed large differences between gels with regard to the effect of oil droplets, while these differences were not visible at the low speeds usually applied in literature.

In the following we propose an explanation of the results presented in this work based on the rheological properties of the systems studied and considering the different mechanisms regarding compression speed dependency, stress concentration and energy dissipation upon deformation (Table 5.2 and 5.3).

In Table 5.7 a summary is given of the mechanisms that may explain the observed effects of compression speed on the Young's modulus and fracture properties of the gel matrices studied. For gelatine and κ -carrageenan gels, the Young's modulus was almost independent of the compression speed. These two gels behave almost purely elastically. The compression speed dependency of the Young's modulus of the viscoelastic WPI gels indicates a more viscous behaviour (mechanism A). These findings are in agreement with both the recoverable energy values obtained for gels without oil droplets and the tan δ values reported in literature for these gels. Gelatine gels were the most elastic, WPI gels were the most viscous and κ -carrageenan gels were intermediate. For the polymer gels, the increase of fracture stress and fracture strain with increasing compression speed can be ascribed to increased friction between the structural elements of the gel and, for gelatine, to the unzipping of the physical bond connecting flexible random-coil chains. For WPI gels, which showed a more viscoelastic behavior, the effect of compression speed on fracture properties can be explained on the basis of the viscous flow of the matrix and the presence of inherent defects within the gel network, which induce stress concentration upon deformation.

Type of gel	$\sigma_{ m f}$	ε _f	Ey
Gelatine bound	E, D	E, D	Elastic behaviour
к-carrageenan bound	D	D	Elastic behaviour
WPI bound	B, C, D	B, C, D	А

Table 5.7 – Summary of the mechanisms explaining the effect of the compression speed on fracture properties and Young's modulus of the gels.

 σ_{f} : fracture stress; ϵ_{f} : fracture strain; Ey: Young's modulus.

In Table 5.8 a summary is given of the mechanisms that may explain the effects of the presence of oil droplets in the gel matrix and of their φ on the Young's modulus and fracture properties. In all gels the oil droplets act mainly as stress concentration nuclei, with differences which can be ascribed to the droplet-matrix interactions. The overall effect on fracture properties is a combination of these effects and of the effect of the droplets on the Young's modulus.

Table 5.8 – Summary of the mechanisms explaining the effect of ϕ on fracture properties and Young's modulus of emulsion-filled gels.

Type of gel	$\sigma_{\rm f}$	ε _f	Ey
Gelatine bound	B1, F1	B1	F1
Gelatine unbound	B2, F2	B2	F2
к-carrageenan bound	B1, F1	B1	F1
к-carrageenan unbound	B2, D, F2	B2, D	F2
WPI bound	F1, C, (B1)	C, B1	F1

 σ_{f} : fracture stress; ϵ_{f} : fracture strain; E_{y} : Young's modulus. F1: van der Poel theory for bound droplets; F2: van der Poel theory for unbound droplets.

The presence of oil droplets in the gel matrix modifies also the effect on large deformation properties of changes in compression speed. For all gels, the amount of energy dissipated by friction increases with increasing deformation speed (Table 5.9).

Type of gel	$\sigma_{\rm f}$	ε _f	$\mathbf{E}_{\mathbf{y}}$
Gelatine bound	E, D	E, D	Elastic behaviour
Gelatine unbound	B2, D, E(*)	B2, D, E(*)	Elastic behaviour
к-carrageenan bound	D	D	Elastic behaviour
к-carrageenan unbound	D, B	D, B	Elastic behaviour
WPI bound	C, (D)	C, (D)	А

Table 5.9 – Summary of the mechanisms explaining the interactions of compression speed and φ on fracture properties and Young's modulus of emulsion-filled gels.

 σ_f : fracture stress; ϵ_f : fracture strain; Ey: Young's modulus. *: balance between D and E shifted to D

Nevertheless, the effect of compression speed on the Young's modulus and the fracture parameters as described for the matrices does not qualitatively change as a result of this increase in energy dissipation. Also when oil droplets are present in the gel matrix, the Young's modulus is independent of compression speed for the polymer gels and increases with increasing compression speed for the WPI gels. Furthermore, for both polymer and WPI gels the fracture parameters remain dependent of compression speed. Up to the highest φ studied, the compression speed-dependency of the matrix determines the effect of compression speed on the large deformation and fracture properties of the filled gels. These findings are generally in line with the recoverable energy values obtained for the filled gels. For the polymer gels, the presence of bound droplets did not affect their elastic behaviour. On the other hand, the presence of unbound droplets increased the viscous character of gelatine gels. This implies a higher amount of energy dissipated by friction. With increasing compression speed the amount of energy dissipated by friction increases even more. The effect of φ on the recoverable energy values obtained for gelatine gels with unbound droplets is not enough to show repercussions on the effect of compression speed on the Young's modulus. Also for gelatine gels containing unbound droplets and with $\varphi = 0.21$ no effect of compression speed on the Young's modulus was observed. The measurements of the recoverable energy were performed up to a strain of 0.25. For gelatine gels, this strain is still within the linear region. For both κ -carrageenan and WPI gels a strain of 0.25 falls outside the linear region. For these gels the lower recoverable energy as compared to gelatine is related to the formation of cracks within the gel structure. The formation of cracks will increase with increasing φ . In Table 5.10 the

mechanisms explaining the effects of ϕ and compression speed on recoverable energy are summarised.

Table 5.10 – Summary of the mechanisms explaining the effect of the compression speed on recoverable energy of emulsion-filled gels.

Type of gel	RE			
	Oil droplets	Compression speed		
Gelatine bound	Linear region, small effect	Linear region, small effect		
Gelatine unbound	Energy dissipation for friction (D)	Energy dissipation for friction (D)		
к-carrageenan bound	Outside linear reg., crack formation (*)	No effect		
к-carrageenan unbound	Outside linear reg., crack formation (*)	No effect		
WPI bound	Outside linear reg., crack formation (*)	No effect		

*: Implies energy dissipation.

The strain-hardening behaviour of the polymer gels studied is likely to be related to the straightening of the polymer chains upon deformation (Groot et al., 1996). The strainindependency of the modulus of WPI gels is in agreement with the results of Pouzot et al. (2006) for heat-set β -lactoglobulin gels with a modulus higher than 2 kPa.

The presence of oil droplets within the gel matrix and the compression speed probably do not affect the strain-hardening behaviour of the studied gels. To our opinion, the observed decrease of the slope of the fracture vs. strain curve with increasing φ a higher strains does not represent a change of the strain-hardening behaviour of the gels, but is related to stress concentration phenomena induced by the droplets. This is supported by the effect of φ on fracture stress and strain observed for polymer (strain-hardening) gels. The calculation of strain-hardening parameters (e.g. by dividing the modulus at fracture by the Young's modulus or the modulus in an initial part of the curve (Gwartney, D.K. & Foegeding, 2004) without analysing the stress vs. strain curves would lead to incorrect conclusions. In this particular case it would lead to the conclusions that strainhardening decreases with increasing φ .

5.6 Conclusions

For emulsion-filled gels the compression speed dependency of Young's modulus and fracture behaviour is determined by the gel matrix. The presence of oil droplets embedded in the gel matrix has primarily an affect on the Young's modulus. The effect of the oil droplets on the fracture behaviour of emulsion-filled gels is related to two main mechanisms. Oil droplets act as stress concentration nuclei and increase the energy dissipation by friction. Stress concentration results in a decrease of both fracture stress and fracture strain. Energy dissipation by friction causes an increase of both fracture stress and fracture strain. The first mechanism is more important for bound droplets, the second for unbound droplets. The overall effect of stress concentration and energy dissipation by friction induced by the presence of oil droplets is related to the rheological properties of the gel matrix and to the droplet-matrix interactions. For elastic polymer gels, like gelatine and κ -carrageenan gels, stress concentration is more important than energy dissipation for friction. This also holds for gels with bound droplets as compared to gels with unbound droplets, independently of the type of gel. For particle gels, like WPI gels, friction phenomena will be more relevant. This holds also for gels with unbound droplets as compared to gels with bound droplets, independently of the type of gel. With increasing φ , particle gels and gels containing unbound droplets become less elastic and more viscous. In particle gels, however, energy dissipation by viscous flow also plays an important role.

5.7 References

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Chapter 6

Deformation and fracture of emulsion-filled gels. Effect of gelling agent concentration and oil droplet size.

G. Sala, T. van Vliet, M. A. Cohen Stuart, F. van de Velde, G.A. van Aken, Deformation and fracture of emulsion-filled gels. 2 Effect of gelling agent concentration and oil droplet size, submitted for publication.

Abstract

The large deformation properties of gelatine, κ -carrageenan and whey protein isolate (WPI) gels with varying ratio's between the modulus of the oil droplets and that of the gel matrix (i.e. with varying gelling agent concentration and oil droplet size) were studied as a function of the compression speed. The effect of the gelling agent concentration and the oil droplet size on strain-dependency of the modulus and viscoelastic properties was also studied. An increase in the concentration of gelling agent resulted in denser gels with more bonds between structural elements. This induced an increase of both Young's modulus and fracture stress for all gels. With increasing gelling agent concentration, polymer gels (gelatine and κ -carrageenan) became less strain-hardening and the particle gels (WPI) even became strain-weakening. The effect of a decrease in the oil droplet size on the Young's modulus was generally according to the van der Poel theory, unless when the oil droplets were aggregated. Moreover, a decrease in oil droplet size induced a decrease of the fracture strain in gels with non-aggregated bound droplets. The extent of these changes was shown to depend on the gelling agent concentration. The effect of a decrease of the oil droplet size on other fracture parameters and in other gel systems was minor. With decreasing oil droplet size gelatine gels with unbound droplets and WPI gels became more viscous and less elastic.

6.1 Introduction

In the previous chapter, we studied the effect of compression speed and oil concentration on the large deformation properties of gelatine, κ -carrageenan (polymer gels) and whey protein isolate (WPI, particle gels) emulsion-filled gels (Sala, van Vliet, Cohen Stuart, van Aken & van de Velde, Submitted). The experimental data reported in chapter 5 in question were obtained for systems with constant gelling agent concentration and oil droplet size, i.e. with constant ratio between de modulus of the oil droplets and that of the gel matrix.

For emulsion-filled gels, changes in gelling agent concentration and oil droplet size both result in variations in the ratio M (= G'_f/G'_m) between the modulus of the filler (G'_f) and that of the gel matrix (G'_m). The effect of M on the small deformation properties of emulsion-filled gels was discussed by van Vliet (1988) on the basis of the van der Poel theory (van der Poel, 1958; Smith, 1974, 1975). For bound droplets, the effect of oil volume fraction (φ) on G' (modulus of the filled gel) is directly related to M. For droplets stiffer than the matrix (M >1), the larger the ratio, the larger the increase of G' with increasing φ . For droplets less stiff than the matrix (M <1), the lower the ratio, the larger the decrease of G' with increasing φ . In Figure 6.1 the effect of M on

$$\alpha = \left(\frac{d(G'/G'_m)}{d\varphi}\right)_{\phi \to 0}$$
(6.1)

is shown as derived from the van der Poel theory. For gels with M <1, the minimum value of α is -1.67. This is also the value of G'/ G'_m for gels with unbound droplets as proposed by van Vliet (1988). Alpha increases with increasing M and for M $\rightarrow \infty$ it reaches the asymptotic value of 2.5.

Calculations on the stress conditions under uniaxial compression in an incompressible isotropic gel containing a dilute dispersion of spherical fillers have been based on the theory of elasticity and on the assumption that the interactions between fillers are negligible (Gao, Lelievre & Tang, 1995). The results indicated that the stress concentration around the filler particles depends upon the filler-matrix interactions and on the ratio of the shear moduli of the two system components. For rigid fillers in a soft gel, the stress concentration factor at the interface between a filler and matrix came out at 3 for unbound fillers and at 2.5 for bound fillers. For fillers softer than the matrix, the stress

concentration factor equalled 1.67, independently of the interaction between filler and matrix. The stress concentration decreased with increasing distance from the surface of the filler and became zero at a distance corresponding to three times the radius. The results of Gao et al. (1995) are partially in contrast with the experimental data discussed in chapter 5, where we concluded that the stress concentration effect due to the oil droplets is larger for bound droplets than for unbound droplets.

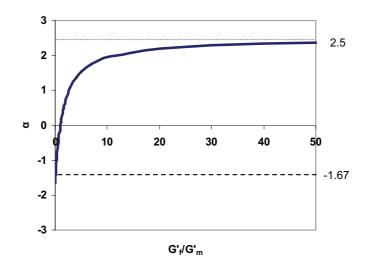


Figure 6.1 – Effect of the ratio between modulus of the filler and that of the matrix on the modulus of the filled gels at $\varphi \rightarrow \infty$ according to the van der Poel theory. G'_m: storage modulus of the gel matrix; G'_f: storage modulus of the filler. The dotted line represent the maximum value for α (2.5), the dashed line the minimum (-1.67). -1.67 is also the value of α for unbound droplets.

In heat-set WPI gels, a decrease of the oil droplet size at constant whey protein concentration (i.e. an increase of the ratio between the modulus of the oil droplet and that of the matrix) resulted in a higher compressive stress for gels containing emulsions stabilised by WPI (i.e. bound droplets) (McClements, Monahan & Kinsella, 1993). For gels containing emulsions stabilised by SDS, Tween 20 and Triton X-100 (i.e. unbound droplets) no effect of the oil droplet size on compressive stress was observed.

In chapter 2 we confirmed the indications of van Vliet regarding the effect of a variation of M on small deformation properties (Rosa, Sala, van Vliet & van de Velde, 2006). In this study the fracture stress and the fracture strain were found to be independent of the droplet size. Compared to the study by the group of McClements (1993), the range of oil droplet size taken into consideration in this study was smaller.

In heat-set soybean protein isolate gels containing oil droplets stabilised by the same protein a decrease in oil droplet size resulted in an increase of the Young's modulus and the fracture stress (Kim et al., 2001). The fracture strain was not affected by either the oil droplet size or the oil content. The oil droplets present in the gels were extensively aggregated.

The effect of oil droplet size and gelling agent concentration on the large deformation properties of agar gels filled with oil droplets stabilised by polyglycerolesters of fatty acids were investigated by compression measurements (Kim, Gohtani, Matsuno & Yamano, 1999). At all agar concentrations the presence of the oil droplets induced a decrease of the fracture stress, which was larger for larger droplets. The presence of the oil droplets and their size did not affect the fracture strain. The oil droplets were extensively aggregated and microscopy observations revealed empty spaces between the gel network and the oil droplets.

Based on the findings reported in literature, the ratio between the modulus of the oil droplet and that of the matrix appears to have a clear effect on the large deformation and fracture properties of emulsion-filled gels. In this chapter the effect was studied of gelling agent concentration, oil droplet size and compression speed on the large deformation properties and visco-elastic behaviour of emulsion-filled gels with varying droplet-matrix interactions. The chosen systems were gelatine, κ -carrageenan and whey protein isolate (WPI) gels containing emulsions made of medium-chain triglycerides oil and stabilised with different emulsifying agents (WPI, Tween 20, lactoferrin and WPI aggregates) to control droplet-matrix interaction.

6.2 Materials and methods

6.2.1 Materials

Porcine skin gelatine PBG 07 (bloom 280, isoelectric point 8-9) was kindly provided by PB gelatines (Vilvoorde, Belgium). Kappa-carrageenan was kindly donated by CP Kelco (Lille Skensved, Denmark). The κ -carrageenan sample consisted of 93% mol κ -units and 7% mol ι -units, as determined by NMR spectrometry (van de Velde, Pereira & Rollema, 2004). Powdered whey protein isolate (WPI, BiproTM) was obtained from Davisco International Inc. (La Sueur, MN, USA). Tween 20 (Polyoxyethylene sorbitan

monolaurate, in the text referred to as Tween) was obtained from Sigma (Sigma-Aldrich Chemie BV, Zwijndrecht, The Netherlands). Lactoferrin were kindly donated by DMV International (Veghel, The Netherlands). Medium Chain Triglycerides (MCT) MIGLYOL 812N oil was purchased from Internatio BN (Mechelen, Belgium). Potassium chloride (p.a.) was obtained from Merck (Darmstadt, Germany). Glucono- δ -lactone (GDL) was kindly donated by Purac (Gorinchem, The Netherlands). All materials were used without further purification. All solutions were prepared with demineralised water.

6.2.2 Sample preparation

6.2.2.1 Emulsions

Emulsions stabilised with different emulsifying agents were used for gel preparation in order to vary the interactions between oil droplet and gel matrix. The procedures for the preparation of the emulsions have been described before (Sala et al., Submitted). In the present study the oil droplet size of the emulsions was varied. The emulsions prepared with each emulsifying agent were homogenised at different pressures in order to obtain the desired droplet size. The droplet size distribution of the emulsions was measured using a Malvern Mastersizer 2000 (Malvern Instruments Ltd., Malvern, UK). The droplet volume-surface average or Sauter diameter ($d_{3,2}$) and other characteristics of the emulsions used for the preparation of the filled gels are reported in Table 6.1.

Emulsifying agent	d _{3,2} (μm)	G' droplet (kPa)	E _y droplet (kPa)	рН
1 wt% WPI	4.25	19	56	7.70
	1.10	73	218	7.44
	0.45	178	533	7.80
3 wt% WPI aggregates	4.90	16	49	7.50
	2.55	31	94	7.58
	0.40	200	600	7.70
2 wt% Lactoferrin	3.75	21	64	5.36
	1.35	59	178	5.32
2 wt% Tween	5.15	4	12	4.24
	0.90	22	67	4.24
	0.45	44	133	4.18

Table 6.1 – Volume-surface average diameter (Sauter diameter) and pH of the emulsions used for the preparation of the filled gels.

The G'of the droplet was calculated by G'= $4\gamma/d$ (van Vliet, 1988) whereby the surface tension γ was taken to be 20 mN/m for protein stabilised droplets and 5 mN/m for Tween stabilised droplets. The Young's modulus (E_y) was E_y = 3G'.

6.2.2.2 Gels

Gelatine (4, 6, 8, 10 wt%) and WPI (3, 5, 7, 9 wt%) gels were prepared in demineralised water. Kappa-carrageenan (0.6, 1.0 1.4, 1.8 wt%) gels were prepared in a 30 mM KCl solution. Samples of filled gels were prepared at two different gelling agent concentrations per gel type (4 and 10 wt% for gelatine, 3 and 6.75 wt% for WPI, 0.6 and 1.8 wt% for κ -carrageenan) with φ of 0.21, corresponding to an oil concentration of 20 wt%. The procedures for the preparation of the gels have been described before in detail (Sala et al., Submitted). In Table 6.2 the ratio's between the Young's modulus of the oil droplets and that of the gel matrix are reported for all combinations studied.

	Emulsifying agent										
		1 wt% V	WPI		wt% \ lggrega			vt% oferrin	2 wt	t% Tw	een
					Ċ	l _{3,2} (μn	1)				
Gel matrix	4.25	1.10	0.45	4.90	2.55	0.40	3.75	1.35	5.15	0.90	0.45
Gelatine											
4 wt% (5 kPa)	11	44	107	-	-	-	-	-	2.3	13	27
10 wt% (25 kPa)	2.3	8.7	21	-	-	-	-	-	0.5	2.7	5.3
к-carrageenan											
0.6 wt% (6.5 kPa)	8.7	34	82	-	-	-	10	27	-	-	-
1.8 wt% (88 kPa)	0.6	2.5	6.1	-	-	-	0.7	2.0	-	-	-
WPI											
3 wt% (6 kPa)	-	-	-	8.2	16	100	-	-	-	-	-
6.7 wt% (40 kPa)	-	-	-	1.2	2.4	15	-	-	-	-	-

Table 6.2 – Ratio E_{f}/E_{m} for the different combinations between emulsions and matrices.

-: combination not studied

The large deformation properties of the gels were determined by uniaxial compression between two flat lubricated plates using different constant deformation speeds. True stress and true strain were calculated as follows:

$$\mathcal{E}_{H} = \int_{H_0}^{H} \frac{1}{H} dH = \ln\left(\frac{H}{H_0}\right)$$
(6.2)

$$\sigma_t = \frac{F}{A} \tag{6.3}$$

For an extensive description of the method we refer to Sala et al. (Submitted). The effect of gelling agent concentration and oil droplet size on strain-hardening behaviour was studied by superimposing the fracture vs. strain curves of gels for which these parameters were varied and observing possible changes in the slope of the curves. The curves were superimposed by dividing the stress along the stress vs. strain curve by the Young's modulus. The obtained stress is dimensionless and was called normalised stress. The microstructure of the samples was studied by Confocal Laser Scanning Microscopy (CLSM) as described in chapter 5. Coalescence phenomena occurring after mixing the emulsions with the gelling agents solutions were studied by analysing the CLSM images of the gels (image size of $39.7 \times 39.7 \mu m$). The diameter of the droplets present in one image was visually estimated. The obtained estimate of the size distribution of the oil droplets present in the gel was compared to the droplet size distribution of the emulsion. Furthermore, CLSM images of different gels containing the same emulsion were compared and increases of the diameter related to coalescence were visually estimated.

6.3 Results

6.3.1 Effect of gelling agent concentration in gels without oil droplet

For all gels, an increase in the gelling agent concentration induced an increase in both the Young's modulus and the fracture stress (Figure 6.2). For WPI gels, also the fracture strain increased with increasing gelling agent concentration, while for polymer gels the effect of the gelling agent concentration on this parameter was minor. The effect of compression speed on the Young's modulus and fracture properties has been discussed before (Sala et al., Submitted). The compression speed remarkably affected the fracture properties of both gelatine and κ -carrageenan gels. This effect of speed increased with increasing gelling agent concentration (Figures 6.2.1B and 2.2B). For WPI gels the dependency of the fracture stress on compression speed increased also with increasing gelling agent concentration, while the effect of the compression speed on the fracture stress on the fracture fracture stress on the fracture stress on the fracture stress and the fracture stress on the fracture stress and the fracture stress on the fracture stress and the fracture stress and the fracture stress on t

With increasing gelling agent concentration, polymer gels became less strainhardening (Figures 6.3.1 and 6.3.2). For κ -carrageenan gels, at the highest concentration tested (1.8 wt%) the stress increased almost linearly with strain, i.e. at the mentioned concentration the gels were not strain-hardening. With increasing gelling agent concentration WPI gels became strain-weakening at intermediate strains (Figure 6.3.3). For all gels, the effect of gelling agent concentration on strain-hardening was not affected by the compression speed (results not shown).

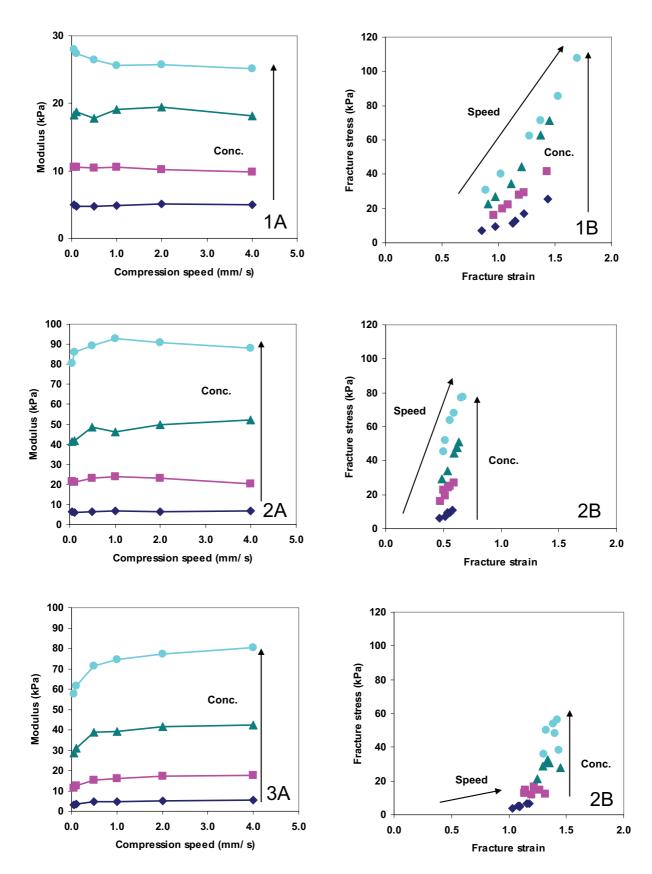


Figure 6.2 - Effect of compression speed on Young's modulus (A) and fracture points (B) of gelatine (1), κ -carrageenan (2) and WPI (3) gels at different concentrations. The concentrations of the different gels are reported in the 'Methods' section.

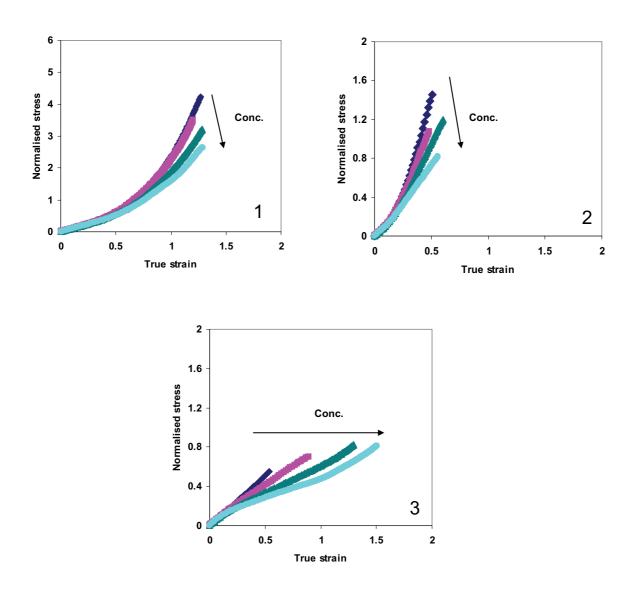


Figure 6.3- Effect of gelling agent concentration on the slope of the stress vs. strain curve for different gels. (1: gelatine; 2: κ -carrageenan; 3: WPI) at a compression speed of 1 mm/s.

The recoverable energy slightly increased with increasing gelling agent concentration for WPI gels, and decreased for κ -carrageenan gels (Figure 6.4). For these gels, the recoverable energy was not affected by the compression speed. For gelatine gels, the recoverable energy was not affected by the gelling agent concentration at low compression speed, and slightly increased at high compression speed (Figure 6.4). In Table 6.3 the effects of the gelling agent concentration on large deformation and fracture properties are summarised. Table 6.4 shows the effects of compression speed on the large deformation and fracture properties of gels with different gelling agent concentrations.

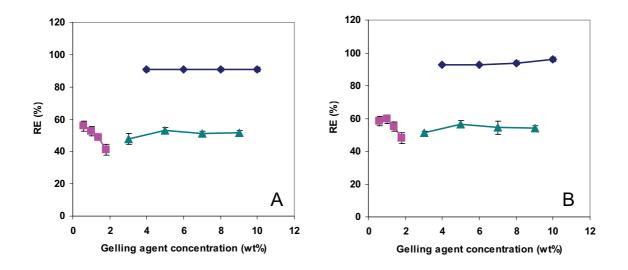


Figure 6.4 - Effect of gelling agent concentration on recoverable energy for different gels: \blacklozenge : gelatine; \blacksquare : κ -carrageenan; \blacktriangle : WPI. (A): compression speed 1 mm/s. (B): compression speed 4 mm/s.

Table 6.3 – Summary of the results obtained for gels without emulsion droplets with respect to thegelling agent concentration.

Type of gel	Gelling agent concentration						
	σ _f	ε _f	Ey	Ef(ε _f)	RE		
Gelatine	+++	++	+++		+		
к-carrageenan	+++	+	+++				
WPI	+++	+++	+++		+		

 σ_{f} : fracture stress; ϵ_{f} : fracture strain; E_{y} : Young's modulus. $Ef(\epsilon_{f})$: modulus as a function of strain. + denotes an increase of the parameter with gelling agent concentration. - indicates a decrease of the parameter. More + or – correspond to a stronger effect. 0: no effect.

Type of gel	Compression speed						
	σ _f	ε _f	Ey	Ef(ε _f)	RE		
Gelatine	+++	+++	0	0	0		
к-carrageenan	+++	++	0	0	0		
WPI	+++	0	+++	0	0		

Table 6.4 – Summary of the results obtained for gels without emulsion droplets with respect to the compression speed.

 σ_{f} : fracture stress; ε_{f} : fracture strain; E_{y} : Young's modulus. $Ef(\varepsilon_{f})$: modulus as a function of strain. + denotes an increase of the parameter with speed. More + correspond to a stronger effect. 0: no effect.

6.3.2 Effect of oil droplet size in gels with different gelling agent concentrations

Variations in the oil droplet size did not remarkably affect the aggregation of the oil droplets embedded in the gel matrix as described in chapters 3 and 5 (Sala, van Aken, Cohen Stuart & van de Velde, 2007; Sala et al., Submitted). In gelatine and WPI gels, the oil droplets were not aggregated, irrespective of the emulsifying agent used for emulsion preparation. In contrast, in k-carrageenan gels both the emulsions stabilised by WPI and those stabilised by lactoferrin were strongly aggregated. A comparison between the CLSM micrographs of gelatine and κ -carrageenan gels containing the same emulsions stabilised by WPI (Figures 6.5A and 6.5B) and with a Sauter diameter of 0.45 µm revealed extensive coalescence in the κ -carrageenan gels in addition to aggregation. This phenomenon was not as evident at larger droplet size and for emulsions stabilised by lactoferrin (results not shown). Furthermore, it was not observed when studying the effect of φ on the large deformation properties of the same gels at constant oil droplet size (d_{3.2} about 1 μ m) (Sala et al., Submitted). Nevertheless, some coalescence of the oil droplets embedded in κ -carrageenan probably occurred also at larger droplet size and for emulsions stabilised by lactoferrin. Coalescence in κ -carrageenan gels was related to the aggregation occurring in the emulsions used for the preparation of the κ -carrageenan upon addition of KCl. KCl addition was needed to adjust the salt concentration to that of the κ -carrageenan solutions. As a result of coalescence, the diameter of oil droplets embedded in kcarrageenan gels was about a factor 2-4 larger than the Sauter diameter measured after preparation of the emulsions. The ratio's between the modulus of the droplet and that of the gel matrix were consequently smaller than those calculated with the original Sauter diameter of the emulsions. Rough estimates of these ratios taking into account the coalescence of the oil droplets are reported in Table 6.5.

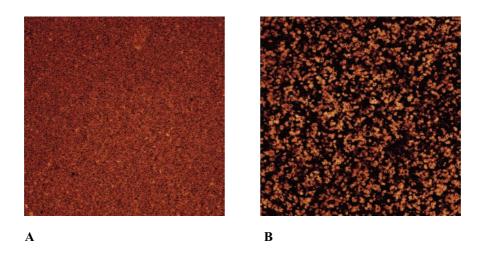


Figure 6.5 - CLSM images of a gelatin gel (A) and a κ -carrageenan gel (B) containing a WPI-stabilised emulsion with an oil droplets size of 0.45 μ m (φ : 0.21; image size 159 X 159 μ m).

Table 6.5 – Ratio E_{f}/E_{m} for the different combinations of emulsions and κ -carrageenan gels after correction for oil droplet coalescence.

			Emulsifying ag	gent	
		1 wt% WP	I	2 wt% Lac	toferrin
			d _{3,2} (μm)		
	8.5-17	2.2-4.4	0.9-1.8	7.5-15	2.7-5.4
0.6 wt% (6.5 kPa)	4.3-2.2	16.8-8.4	41-20.5	4.9-2.5	21.7-10.9
1.8 wt% (88 kPa)	0.3-0.2	1.2-0.6	3-1.5	0.4-0.2	1.6-0.8

The effect of oil droplet size variations depended on droplet-matrix interactions, the microstructure of the gels and M. For non-aggregated bound droplets, like in gelatine gels with WPI-stabilised emulsions (Figure 6.6) and in WPI gels (Figure 6.10), a decrease of the droplet size induced an increase of the Young's modulus and a decrease of the

fracture strain. In agreement with the van der Poel theory, this increase was larger for larger M. For both types of gels, the fracture stress was not affected by a decrease of the oil droplet size. For gelatine gels, the effect on fracture strain was larger at low gelling agent concentration. For WPI gels, this effect was larger at the higher gelling agent concentration.

For gels with bound and aggregated oil droplets (κ -carrageenan gels with lactoferrin-stabilised emulsions), an effect of a decrease in the oil droplet size was observed at low gelling agent concentration (Figure 6.8.1A). At low gelling agent concentration the Young's modulus of the gels increased with decreasing droplet size, while fracture stress and fracture strain slightly increased. At high gelling agent concentration M was about 1 or smaller (Table 6.5). Due to aggregation, the presence of oil droplets in κ -carrageenan gels with high gelling agent concentration caused a decrease in the gel modulus. Probably, the highly deformable droplet aggregates rather than the individual droplets act as the filler particles here, effectively lowering the value of M (Figure 6.8.2A). For gels with unbound droplets (gelatine gels with Tween-stabilised emulsions and κ -carrageenan gels with WPI-stabilised emulsions) variations in the droplet size had no effect on either the Young's modulus or the fracture behaviour (Figures 6.7 and 6.9). For these gels, M is always much smaller than 1, independently of the oil droplet size. For κ -carrageenan gels this can also be ascribed to the aggregation and coalescence of the oil droplets.

For gels with non-aggregated bound droplets, the effect of a reduction of the oil droplets on fracture properties resembled that observed with increasing φ (Sala et al., Submitted). In order to confirm whether in these gels a reduction in oil droplet size could mimic an increase in φ , these parameters were varied at the same time in gelatine gels with a gelling agent concentration of 4 wt% (Figure 6.11). Samples with φ = 0.21 and containing an emulsion with d_{3,2}= 3.1 µm showed comparable Young's modulus and fracture properties as samples with φ = 0.11 and containing an emulsion with d_{3,2}= 0.45 µm.

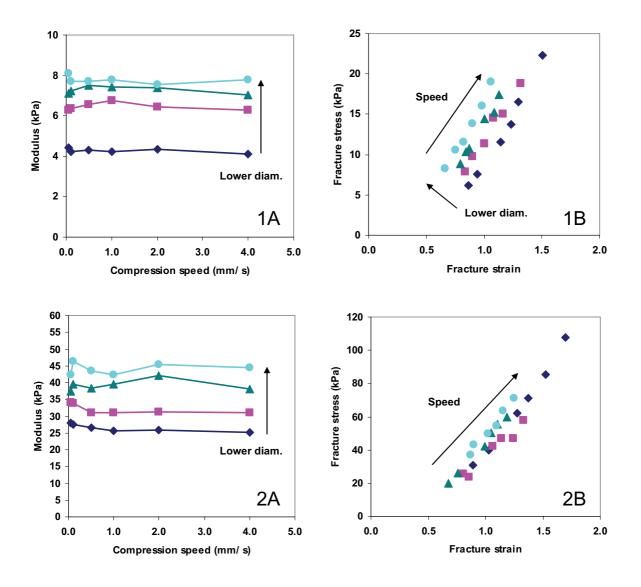


Figure 6.6 – Gelatine bound: effect of compression speed and oil droplet size on Young's modulus (A) and fracture points (B) of gelatine gels with 4 wt% (1) and 10 wt% (2) gelatine (\diamond : no oil; \blacksquare 4.22 µm \blacktriangle : 1.09 µm; \diamond : 0.47 µm).

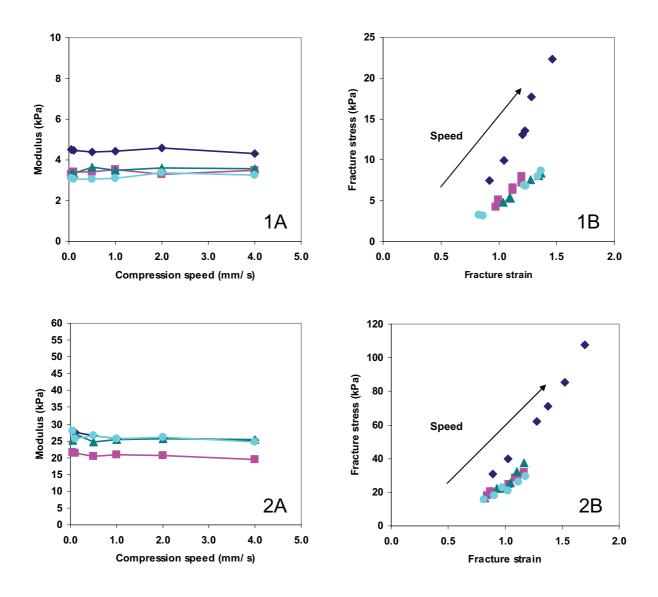


Figure 6.7 – Gelatine unbound: effect of compression speed and oil droplet size on Young's modulus (A) and fracture points (B) of gelatine gels with 4 wt% (1) and 10 wt% (2) gelatine (\diamond : no oil; \blacksquare 5.12 µm \blacktriangle : 0.90 µm; \diamond : 0.45 µm).

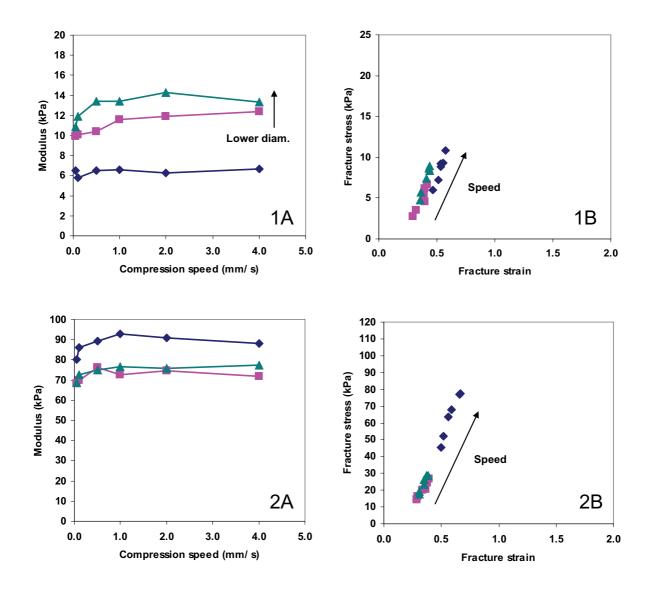


Figure 6.8 – Kappa-carrageenan bound: effect of compression speed and oil droplet size on Young's modulus (A) and fracture points (B) of κ -carrageenan gels with 0.6 wt% (1) and 1.8 wt% (2) κ -carrageenan (\blacklozenge : no oil; \blacksquare 3.17 μ m \blacktriangle : 1.32 μ m).

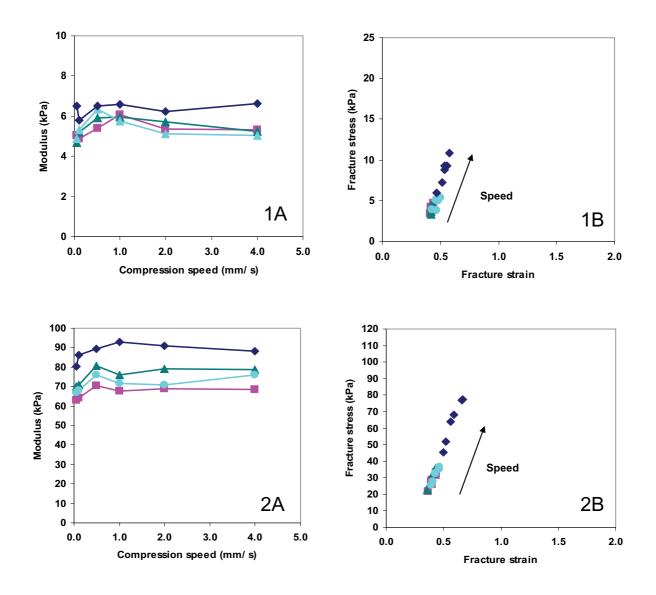


Figure 6.9 - Kappa-carrageenan unbound: effect of compression speed and oil droplet size on Young's modulus (A) and fracture points (B) of κ -carrageenan gels with 0.6 wt% (1) and 1.8 wt% (2) κ -carrageenan (\blacklozenge : no oil; $\blacksquare 4.22 \ \mu m \ \bigstar$: 1.09 μm ; \blacklozenge : 0.47 μm).

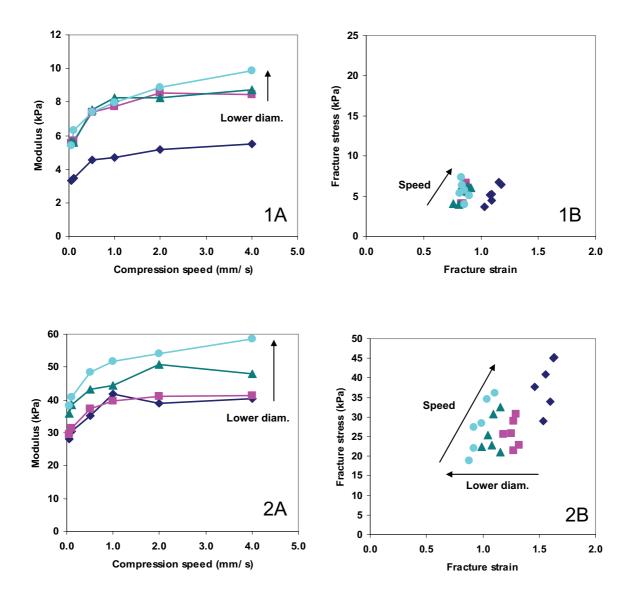


Figure 6.10 – WPI bound: effect of compression speed and oil droplet size on Young's modulus (A) and fracture points (B) of WPI gels with 3.0 wt% (1) and 6.75 wt% WPI (\diamond : no oil; \blacksquare 4.88 µm \blacktriangle : 2.52 µm; \diamond : 0.39 µm).

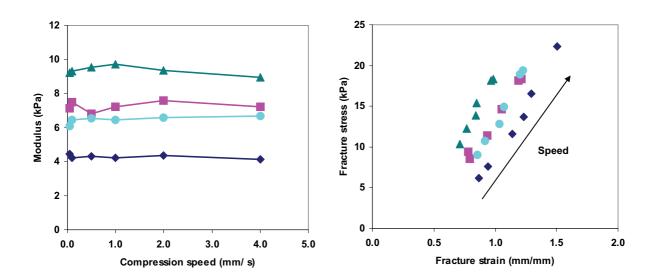


Figure 6.11 – Gelatine bound: Young's modulus vs. compression speed (A) and fracture points (B) of gelatine gels with 4 wt% gelatine and different amounts of WPI-stabilised emulsions with different droplet size (\blacklozenge : no oil; \blacksquare : φ : 0.21; d_{3,2}: 3.1 µm; \bullet : φ : 0.11; d_{3,2}: 0.41 µm; \blacktriangle : φ : 0.21; d_{3,2}: 0.41 µm; \bigstar : φ : 0.41 µm; \Diamond : φ : 0.41 µm;

At the compression speeds tested, the oil droplet size did not significantly affect the strainhardening behaviour of the gels (results not shown). As expected on the basis of the results presented for the effect of the gelling agent concentration (Figure 6.3), the emulsion-filled gels with higher gelling agent concentration were less strain-hardening.

The effect of the oil droplet size on the recoverable energy varied in the different gel systems (Table 6.6). For gelatine gels with bound droplets the recoverable energy slightly increased with decreasing oil droplet size, whereas it strongly decreased in gels with unbound droplets. For κ -carrageenan gels the recoverable energy increased with a decrease of the oil droplet size for both bound and unbound droplets. For WPI gels this parameter decreased with decreasing oil droplet size. In Table 6.7 an overview is given of the effects of the oil droplet size on the large deformation behaviour of the emulsion-filled gels.

					Em	ulsifyir	ng agent		_		
	1 wt% WPI			3 wt% WPI aggregates		2 wt% Lactoferrin		2 wt% Tween		veen	
Gel matrix				RE (%)							
	4.25	1.10	0.45	4.90	2.55	0.40	3.75	1.35	5.15	0.90	0.45
Gelatine											
4 wt% (5 kPa)	89	90	92	-	-	-	-	-	82	66	56
10 wt% (25 kPa)	92	93	93	-	-	-	-	-	96	90	89
к-carrageenan											
0.6 wt% (6.5 kPa)	55	54	59	-	-	-	56	58	-	-	-
1.8 wt% (88 kPa)	49	49	55	-	-	-	48	51	-	-	-
WPI											
3 wt% (6 kPa)	-	-	-	48	43	38	-	-	-	-	-
6.7 wt% (40 kPa)	-	-	-	56	52	45	-	-	-	-	-

Table 6.6 – Effect of droplet size on recoverable energy for the different combinations between emulsions and matrices (compression speed: 4 mm/s).

-: combination not studied; in brackets the Young's modulus of the gels is reported.

Type of gel	Decreasing droplet size							
	$\sigma_{\rm f}$	ε _f	Ey	Ef(_e)	RE			
Gelatine bound								
4 wt%	0		+++	0	++			
10 wt%	+	-	+++	0	++			
Gelatine unbound								
4 wt%	0	0	0	0				
10 wt%	0	0	+	0				
к-carrageenan bound								
0.6 wt%	++	0	+++	0	++			
1.8 wt%	+	0	0	0	++			
к-carrageenan unbound								
0.6 wt%	+	0		0	++			
1.8 wt%	0	0	0	0	++			
WPI bound								
3 wt%	0	0	+	0				
6.7 wt%	++		++	0				

Table 6.7 – Summary of the results obtained for filled gels with respect to the oil droplet size.

 σ_{f} : fracture stress; ϵ_{f} : fracture strain; E_{y} : Young's modulus. $Ef(\epsilon_{f})$: modulus as a function of strain. + denotes an increase of the parameter with decreasing oil droplet size. - indicates a decrease of the parameter. More + or – correspond to a stronger effect. 0: no effect.

6.4 Discussion

The effect of compression speed and presence of oil droplets in the gel matrix on large deformation properties was extensively discussed in chapter 5 (Sala et al., Submitted). In the current chapter we focus our discussion on the effects of gelling agent concentration and oil droplet size, i.e. on the effect of the ratio between the modulus of the filler and that of the matrix.

An increase in gelling agent concentration results in denser gels, with more structural elements and more bonds between them. This can explain the increase in Young's modulus and fracture stress observed for all gels (Table 6.3). In chapter 5 (Sala et al., Submitted), we ascribed part of the effect of the compression speed on the fracture parameters of the gels to friction between structural elements of the gel network. The effect of compression speed on fracture parameters with increasing gelling agent concentration observed in the present work (Table 6.4) can be primarily related to increased friction phenomena. For gelatine gels, an increase in gelling agent concentration will also correspond to a higher density of physical bonds. Upon compression it will then take longer to unzip these bonds in order to fracture the gel. This will result in a higher fracture stress and strain for higher compression speed. A higher density of bonds in gels with a higher gelling agent concentration will also decrease the extensibility of the polymer chains in polymer gels and of the randomly oriented backbones in particle gels. Furthermore, a higher density of bonds in the gel network will reduce strain-induced crystallisation. This can explain the decrease of the strain-hardening behaviour observed for all gels with increasing gelling agent concentration. For WPI gels the strain-weakening behaviour observed with increasing WPI concentration (i.e. with increasing gel modulus) is in accordance with the findings reported by other authors (Pouzot, Nicolai, Benyahia & Durand, 2006). From the results obtained for the recoverable energy (Figure 6.4), we infer that an increase in the gelling agent concentration appears to result for gelatine and WPI gels in a relatively more elastic behaviour and for κ -carrageenan gels in a relatively more viscous behaviour at the applied strains (0.25). The effect observed for gelatine and WPI gels can be readily explained by the shorter length regions over which bonds between different polymer chains interact. A more viscous character of k-carrageenan gels with increasing gelling agent concentration was observed by other authors in the linear region as an increase of the tan δ (Bayarri, Duran & Costell, 2004).

For gels with non-aggregated bound oil droplets, the effect of a decrease in the oil droplet size on the Young's modulus of the filled gels can be explained on the basis of the van der Poel theory (Table 6.8). In these systems, a decrease of the oil droplet size corresponds to a stiffening of the droplets and, therefore, results in larger increases of the Young's modulus as compared to gels with larger droplets and the same φ . The absence of a clear effect of oil droplet size variations on the Young's modulus of gels with unbound droplets supports the approximation by van Vliet (1988) of setting the effective modulus of unbound oil droplets to zero, independently of the size of the droplet aggregation can be twofold. The aggregation of the oil droplets can cause an increase of the effective volume of the fillers, resulting in an increase of the Young's modulus of the filled gels. When the modulus of the aggregates is lower than the Young's modulus of the gel matrix, the effective M is <1 and the effect of oil droplet aggregation can be a decrease of the Young's modulus of the filled gels (Sala et al., 2007). These two effects will undoubtedly depend on the extent of aggregation, but the combined effect is hard to predict.

Type of gel	$\sigma_{ m f}$	ε _f	Ey
Gelatine bound	B1, F1(*)	B1	F1
Gelatine unbound	B2, F2(**)	B2	F2
к-carrageenan bound	B1, F1	B1	F1
к-carrageenan unbound	B2, D, F2(**)	B2, D	F2
WPI bound	F1, C, (B1)	C, B1	F1

Table 6.8 – Summary of the mechanisms explaining the effect of the oil droplet size on fracture properties and Young's modulus.

 σ_{f} : fracture stress; ϵ_{f} : fracture strain; E_{y} : Young's modulus. B: stress concentration; C: induced viscous flow of the matrix; D: friction between structural elements; F: van der Poel theory; 1 refers to the phenomena occurring in gels with bound droplets; 2 refers to phenomena occurring in gels with unbound droplets.*: gives higher σ_{f} at higher compression speed. **: gives lower σ_{f} at higher compression speed.

According to the theory developed by Gao et al. (1995), unbound stiff fillers in a soft gel are expected to induce a larger stress concentration as compared to bound or less stiff fillers. Stress concentration would cause the gels to break at lower fracture strain. Gels containing unbound particles stiffer than the matrix (M >> 1) are therefore expected to break at lower strain. This was not observed in our study. No significant difference was observed in the fracture strain between bound and unbound droplets. In the first part of

this study (Sala et al., Submitted) we even showed that bound droplets are more effective than unbound droplets in decreasing the fracture strains of filled gels. Furthermore, the experimental results obtained for gelatine and WPI gels (i.e. gels in which the oil droplets were not aggregated) show that only for gelatine gels with bound droplets the oil droplets are more effective in decreasing the fracture strain in gels at a higher M (compare Figures 6.7.1B with 6.7.2B, 6.8.1B with 6.8.2B and 6.11.1B with 6.11.2B). For WPI gels, the oil droplets were more effective in decreasing the fracture strain in gels with higher gelling agent concentration, i.e. at lower M (Table 6.2; compare Figures 6.11.1B with 6.11.2B). To study the effect of the stiffness of the oil droplets on stress concentration phenomena, a comparison between gels containing emulsions with different droplet size presents a substantial problem. A decrease of the oil droplet size corresponds in all gels to a remarkable increase in the number of filler particles and to a decreasing distance between droplets. As a consequence, more interference occurs between stress concentration regions. The applicability of the theory Gao et al. (1995) to real gels systems is impaired by several limitations. The assumption made in this theory that there is no filler-filler interaction is valid only at very low filler concentrations. According to Gao et al., the stress concentration decreases with increasing distance from the surface of the filler and becomes zero at a distance corresponding to three times the radius. Already in gels with a φ of 0.05 the distance between neighbouring droplets is smaller than three times the radius. This would result in an overlap of the regions where there is stress concentration coming from different droplets. Furthermore, Gao et al. assumed the absence of frictional stress on the interface between unbound droplets and gel matrix. As shown in chapter 5, for gels containing unbound droplets friction phenomena are extremely relevant at large deformations. Friction (and therefore frictional stress) between the different structural components of filled gels (i.e. also between unbound fillers and gel matrix) increases with increasing deformation speed. The assumption of the absence of frictional stress on the interface between unbound droplets and gel matrix would limit the validity of the theory of Gao et al. to (extremely) low compression speeds.

The decrease of the oil droplet size in gels with a certain gelling concentration corresponds to the stiffening of the droplets and to an increase of their amount. Decreasing the oil droplet diameter by a factor 10 roughly corresponds to an increase of the droplet modulus by the same factor (Table 6.1). At the same time, the number of droplets increases by a factor 1000. The van der Poel theory considers only the stiffness and φ of

the fillers for the prediction of their effect on the modulus of the filled gel (van der Poel, 1958; Smith, 1974, 1975). However, this theory holds in principle only for small deformations. For large deformations, the filler particles should also be considered as defects in the gel matrix which lead to local stress concentration. The stresses near the filler interface may become larger than the strength of the bonds in the gel matrix at smaller deformation. Therefore, the filler particles may act as crack initiators. In this case, the number and the size of filler particles are likely to be important parameters. The size will be primarily important in the sense that this must be larger than the inherent defect length of the gel matrix. For gels with bound non aggregated droplets, a decrease of the droplet size and the related increase in number of droplets has the same effect on Young's modulus and fracture strain as observed for an increase in φ (Figure 6.12; Sala et al., Submitted). For unbound and for aggregated droplets, the increase in the stiffness and the number of droplets as a result of a decrease in oil droplet size does not appear to affect the fracture behaviour of the gels. This supports the observation that unbound droplets are less effective stress concentrating nuclei than bound droplets (Sala et al., Submitted). For gelatine gels with unbound droplets a decrease in oil droplet size and the related increase in the number of droplets results in a remarkable increase of the energy dissipated by friction, as shown by the observed decrease in recoverable energy (Table 6.6). In other words, gelatine gels with small unbound droplets show at large deformation a relatively more viscous character. The same observation holds for WPI gels. Similar effects regarding the recoverable energy were observed for both gels as a result of an increase in φ . The absence of an effect of the stiffness and the number of droplets on the fracture properties of gels with aggregated droplets might be related to their aggregated state.

In chapter 5 we proposed an interpretation of the obtained experimental results on the basis of the different mechanisms regarding compression speed dependency, stress concentration and energy dissipation upon deformation (Sala et al., Submitted). The same mechanisms can also explain the effects of a decrease in oil droplet size on Young's modulus and fracture behaviour (Table 6.8). The overview given in Table 6.8 is the same as that previously proposed for the effect of an increase in φ on the large deformation properties (Sala et al., Submitted), and suggests that, from a phenomenological point of view, a decrease in oil droplet size has the same effects as an increase in φ . For gels with bound, non aggregated droplets, the similarity does not only concern the phenomena occurring, but also the observed effects on large deformation properties. As a consequence, for these gels variations in the oil droplet size represent a tool to engineer gels with different φ but the same fracture behaviour.

6.5 Conclusions

An increase in the gelling agent concentration results in a denser gel structure with a higher number of bonds between the structural elements forming the gel network. This causes an increase of both the Young's modulus and the fracture stress. In particle gels (WPI gels) also the fracture strain increases with increasing gelling agent concentration. This can probably be ascribed to a decrease of the size of the inherent defects present in the gel structure.

By varying the gelling agent concentration and the oil droplet size the ratio between the modulus of the droplets and that of the matrix can be modulated. Variations of this ratio only affect the Young's modulus and fracture properties of gels containing bound, non-aggregated properties. For these gels a decrease in the oil droplet size allows to decrease φ maintaining the same Young's modulus and fracture properties.

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Oil droplet release from emulsion-filled gels in relation to sensory perception

G. Sala, F. van de Velde, M. Cohen Stuart, G.A. van Aken (2007). Oil droplet release from emulsion-filled gels in relation to sensory perception, *Food Hydrocolloids*, 21, 977-985.

Abstract

Oil droplet release upon shearing was studied in emulsion-filled gels containing oil droplets either bound or unbound to the gel matrix. At 20°C no release was observed for gels containing bound droplets. The release measured for gels with unbound droplets related to the fat content and the size of the gel particles obtained after shearing. For gels with bound droplets and melting at the oral processing temperature, increasing the temperature of the determination to 37°C resulted in an almost complete release of the oil droplets. An increase of the oil content induced an increase of the creaminess scores for all gels. These scores were somewhat higher for gels containing unbound droplets and gels melting at oral processing temperature. For these gels, the oil droplet release appears to correlate with creaminess. However, a similar increase in creaminess at increasing oil concentration was also found for gels with oil droplets bound to the matrix. Therefore, it is concluded that the release of oil droplets during oral processing is not the main mechanism causing creaminess perception in emulsion-filled gels.

7.1 Introduction

Knowledge on the relation between sensory perception and rheological, physicochemical and structural properties can facilitate the development of new food products. Rheological properties can often be explained on the basis of the microstructure. Establishing a link between sensory properties and both microstructure and rheological characteristics requires information about the mechanisms relating oral processing and perception of the broken food and its components. However, a correlation between texture perception and instrumental data requires an univocal judgement of texture perception by humans and measurements of the mechanical properties under relevant conditions (van Vliet, 2002). Since this is difficult to achieve and because objective methods to reproduce the eating process are not available (Malone, Appelqvist & Norton, 2003), the link between sensory properties, microstructure and rheological characteristics has remained unclear.

For semi solid foods containing emulsified fats and oils, like custard, mayonnaise and various kinds of sauces, a thorough study on the link between sensory perception and instrumental measurements of rheological and friction properties was carried out (Weenen, Van Gemert, Van Doorn, Dijksterhuis & De Wijk, 2003). For custards, the attribute *creamy* was not satisfactorily correlated to small deformation measurements, such as dynamic stress and frequency sweep, or large deformation measurements, like flow curves and steady shear rate measurements (Jellema, Janssen, Terpstra, de Wijk & Smilde, 2005). With increasing fat content, a decrease in friction was observed for these products, together with an increase in creaminess. Therefore, lubrication was put forward as important factor affecting texture perception in low fat foods (de Wijk & Prinz, 2005). Since amylase-induced starch breakdown also resulted in a decrease of friction, the authors suggested a mechanism for the sensory perception of starch-thickened foods (de Wijk et al., 2005). Starch breakdown would release fat from the starch matrix. The released fat would subsequently migrate to the surface of the bolus, where it would become available for lubrication.

With regard to gelled products, in a study on the sensory properties of stranded and particulate WPI emulsion-filled gels (Gwartney, Larick & Foegeding, 2004) only the firmness sensed at the first bite, the number of chews and the time to swallow were found to correlate to the concentration of emulsified fat. Other sensory attributes correlated only

to the gel structure type. In the systems studied, an increase in oil content induced an increase in gel firmness.

In the study described in chapter 4 (Sala, de Wijk, van de Velde & van Aken, 2008), gels containing emulsion droplets unbound to the gel matrix or with a matrix melting at oral processing temperature resulted in higher scores for the attribute *creamy*, as compared to gels containing droplets bound to the matrix. Therefore, the hypothesis was formulated that the perception of creaminess could be related to the release of oil droplets during mastication.

The aim of this chapter was to study the effect of compositional and experimental parameters on oil droplet release in gels containing emulsion droplets. To do this, a method to quantify the oil droplet release in these systems after shear or breakdown was developed. Gelatine, acid-induced cold-set whey protein isolate (WPI) and κ -carrageenan gels, i.e. gel matrices with a wide variety of parameters concerning elasticity, brittleness and yielding properties, were tested. To these matrices, emulsions stabilized by WPI (or WPI aggregates in the case of acid-induced, cold-set WPI gels) were added. For gelatine, also samples containing emulsions stabilized with Tween 20 were prepared. In order to correlate oil droplet release to sensory perception, gel samples were evaluated by a sensory panel trained according to the principles of Quantitative Descriptive Analysis (QDA) (Stone & Sidel, 1985).

7.2 Materials and methods

7.2.1 Materials

Powdered whey protein isolate (WPI; BiproTM) was obtained from Davisco International Inc. (La Sueur, MN, USA). Kappa-carrageenan was kindly donated by CP Kelco (Lille Skensved, Denmark). The κ -carrageenan sample consisted of 93% mol κ -units and 7% mol ι -units, as determined by NMR spectrometry (van de Velde, Pereira & Rollema, 2004). Gelatine PBG 07 (obtained by acid treatment, isoelectric point 8-9, bloom 270-290) was kindly provided by PB gelatines (Vilvoorde, Belgium). Sunflower oil was purchased from a local retailer. KCl (p.a.) was obtained from Merck (Darmstadt, Germany). Tween 20 (Polyoxyethylene sorbitan monolaurate) was obtained from Sigma (Sigma-Aldrich Chemie BV, Zwijndrecht, The Netherlands). Glucono- δ -lactone (GDL; GluconalTM) was kindly donated by Purac (Gorinchem, The Netherlands). Saccharin was from Acatris Netherlands B.V. (Bunschoten, The Netherlands). Vanilla flavour was donated by Danisco (Grinsted, Denmark). All materials, except Tween 20, were food grade and were used without further purification. All solutions were prepared with demineralised water.

7.2.2 Sample preparation

7.2.2.1 Emulsions

WPI solutions were prepared by adding the protein to the required amount of water. Subsequently, the solutions were gently stirred for 2 hours. Stock emulsions, containing 40 wt% sunflower oil and 1 wt% WPI in the water phase, were prepared by prehomogenising the ingredients using an Ultra Turrax (Polytron, Switzerland) homogeniser. Pre-emulsions were further processed using a laboratory homogenizer (Ariete, Model NS1001L – Panda, Niro Soavi S.p.A, Italy). The volume-surface average or Sauter diameter ($d_{3,2}$) of the droplets of this emulsion was $1.1 \pm 0.05 \mu m$. KCl was added to the emulsion used for the preparation of κ -carrageenan to reach a concentration of 30 mM in the water phase.

Emulsions stabilised with WPI aggregates were prepared as described above, but using a 3 wt% WPI aggregates dispersion as continuous phase. This dispersion was prepared by heating a 9 wt% WPI solution at 68.5° C for 2 hours and subsequent cooling to room temperature with tap water and diluting to 3 wt%. This preparation procedure induces a denaturation of the whey protein >95% (Alting, 2003). The Sauter diameter of the droplets of this emulsion was $1.2 \pm 0.05 \, \mu$ m.

Tween 20 stabilised emulsions were prepared as described for the WPI-stabilised emulsions. The concentration of the emulsifier in this case was 2 wt%. The Sauter diameter of the droplets of this emulsion was $1.0 \pm 0.05 \mu m$. The droplet size distribution of the stock emulsions was measured using a Malvern MasterSizer X (Malvern Instruments, USA). The pH of the emulsions was slightly subneutral (6.6-6.8).

7.2.2.2 Gels

For the study of the oil droplet release, the concentrations of the gelling agents were 4 wt% for gelatine, 3 wt% for WPI and 0.6 wt% for κ -carrageenan. These concentrations lead to approximately the same gel strength. Gelatine and WPI gels were prepared in demineralised water, κ -carrageenan gels in a 30 mM KCl solution.

Samples for sensory analysis were prepared with varying gelling agent concentration in the water phase, in order to obtain comparable moduli (~7kPa) at increasing oil concentration for all samples.

To mask possible off-flavours, 0.012 wt% saccharin and 0.033 wt% vanilla were added to both the emulsions and the gels solutions.

Cold gelation of the WPI gels was induced by addition of a suitable amount of GDL (0.22 wt% for a dispersion with a concentration of 3 wt%) to the WPI dispersion and to the WPI dispersion/emulsion mix and incubation at 25°C for 17 hours, until a pH of 4.5 was reached (Rosa et al., 2006). The WPI dispersion was prepared as described above.

For gelatine and κ -carrageenan gels, the material was allowed to hydrate for 2 hours under gentle stirring at room temperature. The samples were subsequently dissolved by heating at 80°C for 30 minutes and cooled to 25°C for gelatine and to 45°C for κ carrageenan prior to emulsion addition. For κ -carrageenan samples, the emulsions were heated to 45°C. After emulsion addition, the samples were allowed to gel at room temperature. The pH of gelatine gels was in the range 5.3-5.6 (the lower values were observed for gels without emulsion; the higher values for the higher emulsion concentrations). The pH of κ -carrageenan gels was in the range 7.3-8.2 (the higher values were observed for gels without emulsion; the lower values for the higher emulsion concentrations).

The samples for breakdown measurements were allowed to gel in 50 ml plastic syringes (internal diameter 26.4 mm) coated with a thin film of paraffin oil. The samples for oil droplet release were prepared in the same syringes, but without paraffin oil. The samples for the QDA evaluation, prepared under food-grade and sterile conditions, were allowed to gel in lidded plastic cups with a capacity of 50 ml.

7.2.3 Large deformation experiments

Uni-axial compression tests were performed approximately 24 hours after preparation, simultaneously to the QDA evaluation. Gel pieces of about 25 mm height were used for the measurements with an Instron 5543 machine (Instron Corporation, USA) equipped with a plate-plate geometry. The plates were lubricated with a thin layer of paraffin oil. The measurements were performed at room temperature, at a constant deformation speed of 1 mm/s and up to a compression strain of 80%. For gelatine gels, 4 pieces per specimen of 2 specimens were analysed. For the other gels at least 4 pieces per specimen of 1 specimen were used for the measurements.

7.2.4 Quantification of oil droplet release

To quantify the oil droplet release occurring after gel shearing, a highly reproducible method was developed. The shearing treatment consisted of squeezing the gel out of the syringe in which it was prepared by applying on the plunger a constant velocity deformation by means of a Texture Analyser instrument. To this end, the syringe was put on a rack especially build to keep it vertical. The orifice of the used syringes had a diameter of 0.9 mm. For k-carrageenan gels, tests were also carried out after connecting a hypodermic needle to the syringe and after cutting off a part of the original orifice. In the first case the diameter of the orifice was 0.5 mm, in the second case 9 mm. The force needed to squeeze the sample out of the syringe was measured. A known amount of sheared gel (typically 50 g) was collected in a beaker. To this material, an amount of distilled water corresponding to two times that of the gel was added (typically 100 g). The mix gel-water was gently stirred with a magnetic stirrer for 1 minute. The mix was then filtered on a paper filter with large pores (2411 1/2, Schleicher & Schuell, Dassel, Germany). These filters allowed the oil droplets that were released into the liquid phase to pass through the pore. This was confirmed by a complete recovery of the oil from a WPIstabilised emulsion after filtration. The ratio between water and gel was chosen to allow the filtration of the water-gel mix. At lower ratio's the filtration was entirely blocked or became remarkably slow. The oil content of the filtrate was determined by the Röse-Gottlieb method (ISO 1211). This gravimetric method consists in recovering the fat present in an emulsion by extraction with petrol ether and diethylether.

7.2.5 Quantitative Descriptive Analysis

7.2.5.1 Assessors/ sensory attributes

The sensory characteristics of the gels were investigated with the use of a sensory panel trained according to the principles of Quantitative Descriptive Analysis (QDA) (Stone et al., 1985). The panel consisted of nine females aged between 22 and 49 and with aboveaverage scores on all selection tests. These tests included tests of odour identification, odour memory, and verbal creativity, and a series of texture tests in which the ability of the panelist to assess fattiness, roughness, and particle size was measured. All panelists had previously been trained for the assessment of the sensory properties of oil-in-water emulsions. Panelists were seated in sensory booths with appropriate ventilation and lighting. The products were assessed semi-monadically in duplicate on visual analogue scales. The presentation order was randomly assigned per panellist. Acquisition of the panelist's responses was done by computer using FIZZ software (Biosystemes, 1998). In 4 2-hr sessions the panel members were presented and trained with a set of 8 samples of emulsion-filled gels. During these training sessions descriptive attributes were generated that were used to profile 10 emulsion-filled gel samples with 4 reference samples without emulsion. Each gel was served in portions of 40 ml in plastic beakers (volume 50 ml) at an average rate of one sample per 5 minutes. The attributes were generated in Dutch and subsequently translated into English. During profiling, the attributes appeared per category on a monitor placed in front of the panelist with the attributes on the left and a 100-point response scale anchored at the extremes on the right. The panelist used a mouse to indicate the perceived strength of each attribute. Each product was first smelled, after which the odour attributes were rated. Next, the product was taken into the mouth, after which the taste/flavour and mouth feel attributes were rated in the order in which they were perceived. Finally, the product was spat out. The after feel attributes were rated and the panelists rinsed their mouths with acidified water before the next sample.

7.2.5.2 Data analysis

The relationships between sensory attributes and gel samples characteristics were summarized using Principal Component Analysis (PCA) (Unscrambler, Camo Inc., Corvallis, U.S.A). PCA facilitates the identification of attribute synonyms and covariate attributes. Relationships between specific attributes were statistically modeled using 172 Partial Least Squares Regression or PLSR (Unscrambler Vs. 7.5, Camo Inc., Corvallis, U.S.A). The effects of changes in sample properties on individual sensory attributes were analyzed using a factorial ANOVA (SPSS, SPSS Inc, Chicago, U.S.A.), carried out on the raw sensory data. In addition to the three gelling agents, main effects and second order interactions, the ANOVA included a random panelist effect and session effect. Because the ANOVA was carried out on the raw sensory data, it was possible to carry out tests of significance for all effects.

7.3 Results and discussion

7.3.1 Oil droplet release

Emulsion-filled gels with droplets bound to the matrix were obtained for gelatine gels with native WPI-stabilised emulsions and for WPI gels containing WPI aggregates-stabilised emulsions (Sala et al., 2007). In gelatine gels containing a Tween 20-stabilised emulsion, and in κ -carrageenan gels, the oil droplets were not connected to the gel matrix. At 20°C, no oil droplet release could be observed for gels with oil droplets bound to the matrix (Figure 7.1A). For gels containing oil droplets unbound to the matrix, significant amounts of emulsion were released from the matrix after shear treatment (Figure 7.1A). In general, the droplet release was proportional to the oil concentration. For gelatine samples containing a Tween 20-stabilised emulsion, a larger release was observed than for κ -carrageenan gels. Moreover, for these gels an increase of the oil droplet release with increasing oil concentration was observed. This can probably be related to a decrease of modulus and fracture stress at increasing oil concentration observed for these gels in chapter 3 and chapter 5 and to the low value of these parameters as compared to κ -carrageenan. Lower gel strength will result in a more extensive structure breakdown during gel shearing.

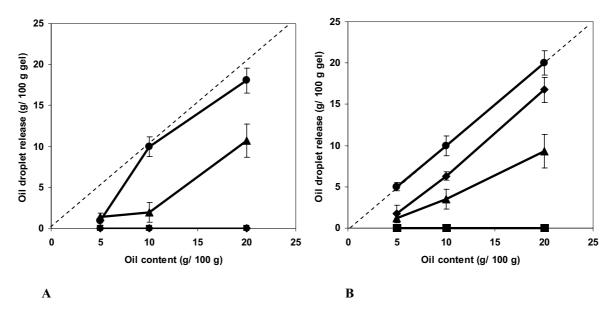


Figure 7.1 - Effect of gel oil content on oil droplet release. A: 20°C; B: 37°C (\blacklozenge : gelatine with WPI-stabilised emulsion; • gelatine with Tween 20-stabilised emulsion; • WPI; \blacktriangle : κ -carrageenan). The dotted line represents total oil droplet release.

The extraction of the emulsion from the gel was also performed at 37° C, in order to mimic the oral processing temperature. Performing the extraction of the oil droplets at this temperature resulted in a substantial release of emulsion droplets also for gelatine gels containing a WPI-stabilised emulsion (Figure 7.1B). As expected, changing the extraction temperature did not affect the oil droplet release for WPI and κ -carrageenan gels. Under the experimental conditions chosen for this determination and at the mentioned temperature gelatine gels melted. Therefore, the differences observed among gel types can be directly related to their melting behaviour. For gelatine samples containing a Tween 20-stabilised emulsion, a slight further increase of the oil droplet release was observed, resulting in a complete release of the emulsion droplets originally entrapped within the gel matrix. The amount of emulsion released after gel shearing appeared to be related to the interactions between oil droplet and gel matrix and to the melting behaviour of the matrix.

For κ -carrageenan gels, i.e. gels containing oil droplets unbound to the gel matrix and not melting at 37°C, an attempt was made to relate the oil droplet release to the extent of structural breakdown of the gel. A variation in structure breakdown was achieved by varying the intensity of the shear treatment. To this end, the gel samples were pressed out of syringes with orifices with different diameter. With decreasing orifice diameter, larger forces had to be applied (data not shown). As a result, at increasing shear intensity, gel particles with decreasing size (i.e. presenting a larger specific surface area) were obtained. The amount of released emulsion increased with decreasing the orifice diameter of the syringe (Figure 7.2). During the set-up of the method, different compression speeds, resulting in different fracture stress values, were applied for sample breakdown (results not shown). This did not significantly affect the oil droplet release. Therefore, the oil droplet release seems to be related only to the specific area of the pieces of the sample obtained after breakdown treatment and not to the applied stress. At increasing oil content, the fraction of extracted emulsion decreased somewhat (Figure 7.2). This decrease appeared most prominent for the most intense shear treatment applied (i.e. for gels pressed out of a hypodermic needle) (Figure 7.2). This is probably due to a lesser separability of the water from the tiny gel particles by filtering, caused by an increased spreadability or softening of the gel particles at the higher oil contents, clogging the filter paper. In reality, the fraction of emulsion droplets released from the gel by shear treatment is probably almost independent of the oil content.

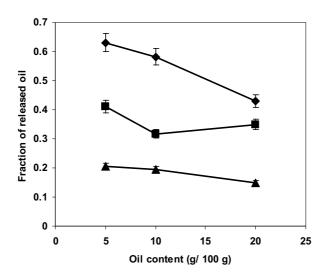


Figure 7.2 - Effect of oil content on fraction of released oil for κ -carrageenan gels pressed out of syringes with orifices with different diameter (\diamond : 0.5 mm; \blacksquare 0.9 mm; \blacktriangle : 9 mm).

For the samples prepared for sensory evaluation, the determination of the oil droplet release was performed at 37°C on four different days. The standard deviation in the resulting data set was smaller than 1% for the samples containing 5 wt% oil. With regard to the samples with 20 wt% oil, the standard deviation was 1.8% for gelatine and 3.4% for κ -carrageenan, respectively. For WPI gels, no oil droplet release was found.

In order to detect possible coalescence phenomena occurring during the shear treatment of the gel, variations of the size distributions of the emulsions droplets extracted from the matrix were studied. This was carried out by light scattering measurements and microscopy observations. A slight increase of the droplet size distribution was observed for the emulsions extracted from gelatine (Figure 7.3A). For κ -carrageenan no variations were observed (Figure 7.3B). The increase observed for gelatine was not due to coalescence, but to the presence in the extract of few, tiny pieces of non-melted gel material in which several droplets were clustered. This was ascertained by microscopic observations (images not shown). The shear treatment applied for the determination of the oil droplet release did not induce coalescence of the oil droplets extracted from the gel matrix.

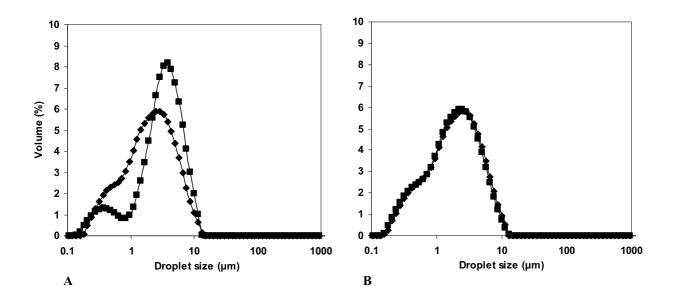


Figure 7.3 – Droplet size density distribution of the bulk emulsion used for sample preparation (\blacklozenge) and of the aqueous extract of the gels with 20% oil (\blacksquare). A: gelatine; B: κ -carrageenan.

7.3.2 Sensory properties

The effects of gel type and oil content on sensory attributes confirmed those reported in chapter 4 (Sala et al., 2008). Also in the present study two main sensory dimensions could be recognised, namely one running from *watery* to *creamy*, and one from *tough* and *crumbly* to *spreadable* and *melting* (Figure 7.4). The first dimension was related to the oil content of the gel, the second to the gel type. In studies on the link between sensory perception and rheological properties of semi-solid foods, such as custard, mayonnaise and sauces, two main sensory dimensions were recognised, one going from *rough* to *creamy* and related to the fat content, and one going from *melting* to *thick* and related to the thickener content (de Wijk, van Gemert, Terpstra & Wilkinson, 2003; Weenen, Jellema & de Wijk, 2005; de Wijk, Prinz & Janssen, 2006). Interestingly, in these studies the attribute *melting* showed a negative contribution to *creamy*, whereas in our work this was not found. In starch-containing semi-solid foods, the attribute *melting* was related to the decrease of thickness induced by starch granules breakdown, resulting in a liquid bolus. In this context, the negative correlation between *creamy* and *melting* appears straightforward. In the present study, the food material was introduced in the oral cavity as a gel and the attribute *melting* was related to the process of gel breakdown, leading to the formation of a semi-solid and spreadable bolus. This bolus was perceived as *creamy* compared to the original gel.

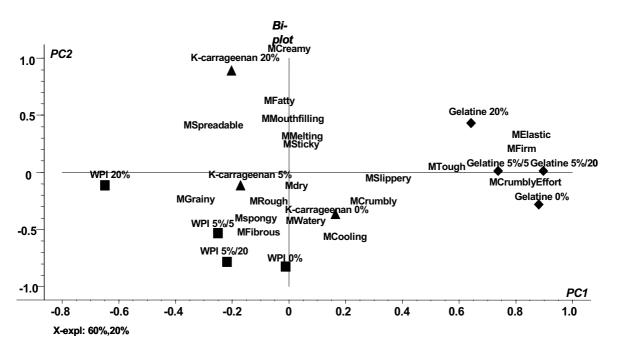


Figure 7.4 – Principal component analysis of sensory data (PC1 explains 60% and PC2 20% of the variance).

Upon increasing oil content, the creaminess of all gels increased (Figure 7.5A). The scores for *creamy* were consistently higher for gelatine and κ -carrageenan gels, although the difference between gelatine and WPI gels was not statistically significant. The scores for the attribute *spreadable* increased at increasing oil concentration for all gels, but the gelatine gels were considerably less *spreadable* than κ -carrageenan and WPI gels (Figure

7.5B). This can be linked to the high fracture stress of the gelatine samples tested in the present study (results not shown). Even though gelatine gels will eventually melt at temperatures around body temperature, the heat transport to the gels particles in the mouth takes some time. Melting is accelerated by the reduction in particle size and the flow in the mouth during mastication. During this oral processing phase the sensory attributes of the gels related to their fracture properties can be appreciated. A high fracture stress was related to high scores for the attributes *tough, firm, crumbly* and *crumbly effort (crumbly* being defined as the presence of small pieces in the mouth and *crumbly effort* as the effort needed to break the sample into pieces) (Table 7.1), which are negatively correlated to *creamy* and *spreadable*.

	Oil Release	Modulus	Fracture	Fracture	Fracture	
			stress	s strain energy		
Oil Release		0,10	0,40	0,43	0,32	
Modulus	0,10	-	0,00	-0,36	-0,14	
Fracture stress	0,40	0,00	-	_0,87	<u>0,96</u>	
Fracture strain	0,43	-0,36	0,87	-	<u>0,90</u>	
Fracture energy	0,32	-0,14	<u>0,96</u>	<u>0,90</u>		
Firm	0,39	-0,29	<u>0,90</u>	<u>0,98</u>		
Elastic	0,42	-0,34	0,87	<u>0,98</u>	<u>0,92</u>	
Tough	0,47	-0,27	0,88	<u>0,96</u>	0,94	
Cooling	-0,40	-0,24	0,27	0,11	0,25	
Slippery	0,44	-0,12	0,69	0,55	0,55	
Fatty	0,27	-0,08	-0,43	-0,17	-0,41	
Spongy	-0,61	0,04	-0,62	-0,57	-0,43	
Crumbly effort	0,42	-0,29	<u>0,91</u>	0,98	0,95	
Crumbly	0,36	0,02	0,72	0,53	0,63	
Fibrous	-0,67	0,11	-0,51	-0,55	-0,34	
Creamy	<u>0,71</u>	-0,12	-0,30	0,02	-0,26	
Spreadable	-0,16	0,23	-0,86	-0,83	-0,89	
Melting	0,50	0,08	-0,49	-0,35	-0,56	
Rough	-0,50	0,18	-0,54	-0,51	-0,37	
Dry	-0,09	0,11	-0,18	-0,09	0,03	
Grainy	-0,53	0,49	<u>-0,78</u>	<u>-0,92</u>	-0,83	
Sticky	-0,07	0,19	-0,10	-0,03	-0,05	
Mouth filling	0,30	0,38	-0,44	-0,38	-0,51	
Watery	-0,47	0,10	-0,36	-0,58	-0,46	

Table 7.1 – Correlations among physicochemical parameters and mouthfeel attributes. Significant correlations ($P \le 0.15$) are underlined.

For gelatine gels, the low scores for the attribute *spreadable* negatively affected the scores for *creamy*. In chapter 4 (Sala et al., 2008), the scores for the attribute *creamy* were

significantly higher for gelatine and κ -carrageenan gels as compared to WPI gels. For the samples described in chapter 4, as a result of a lower gelling agent concentration in the water phase, the fracture stress and the scores for the attribute *spreadable* for gelatine gels were much lower than in the present work.

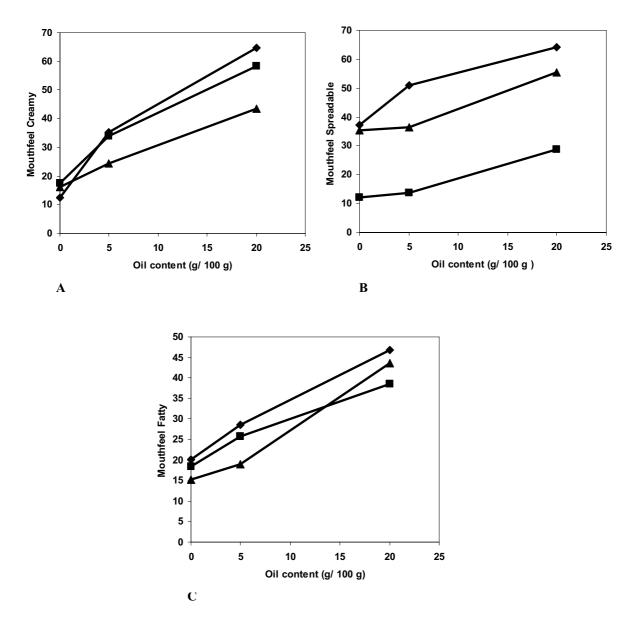


Figure 7.5 - Effect of oil concentration on three different mouthfeel attributes. A: creamy; B: spreadable; C: fatty (\blacklozenge : gelatine; \blacksquare WPI; \blacktriangle : κ -carrageenan).

Whereas in chapter 4 the mouthfeel attribute *fatty* was found to be only affected by the gel type, in the present study this attribute correlated also to the oil content (Figure 7.5C). Increasing the oil concentration from 0 to 20 wt % induced an increase of the scores for *fatty* only by a factor slightly higher than 2. Also in view of the large statistical variation observed for the attribute *fatty* in both studies, we can conclude that in emulsion-filled gels differences in fattiness at increasing oil concentration are not clearly perceived.

Figure 7.6 shows the effect of oil droplets release on both mouthfeel attributes *creamy* and *fatty*. For gels containing unbound oil droplets (κ -carrageenan gels with WPI-stabilised emulsion) and gels melting at the oral processing temperature (gelatine gels) the oil droplet release is highly correlated with both sensory attributes. However, since a similar increase in creaminess and fattiness is also observed upon increasing oil concentration for gels with oil droplets bound to the matrix and non-melting (WPI gels), we can conclude that the perception of creaminess in emulsion-filled gels is not primarily related to the release of oil droplets during structure breakdown. Therefore, the correlation between oil droplet release and the attributes *creamy* and *fatty* for gels containing unbound oil droplets and gels melting at the oral processing temperature appears to be due to the linear relationship between gel oil content and oil droplet release, in combination with a direct relation between the fat content and the mentioned sensory attributes. Clearly, the sensory perception of *creamy* and *fatty* for emulsion-filled gels must have a different cause.

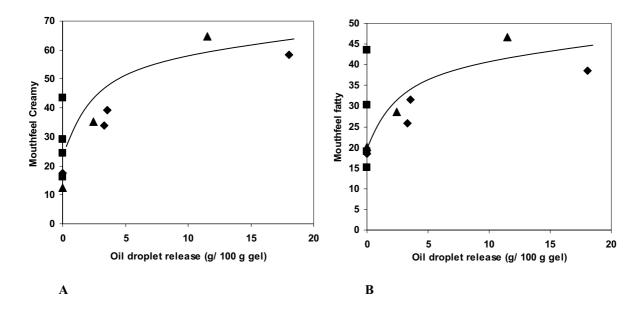


Figure 7.6 - Effect of oil droplet release on two different mouthfeel attributes. A: creamy; B: fatty; (\blacklozenge : gelatine; \blacksquare WPI; \blacktriangle : κ -carrageenan; the curves are drawn to guide the eye).

7.4 Conclusions

The droplet-matrix interactions and the melting behaviour of the gelling agents control the release of oil droplets upon shearing in emulsion-filled gels. Shearing induces the release of unbound droplets, whereas bound droplets are not released. Unbound oil droplets are released in amounts related to the size of the particles in which the gel is broken. For gels that melt at the oral processing temperature, also bound droplets are released after gel melting.

For gels containing unbound droplets or melting during oral processing, the oil droplet release correlates with the attributes *creamy* and *fatty*. Nevertheless, the increase of the scores for these two sensory attributes observed at increasing oil concentration also for gels with oil droplets bound to the matrix shows that the release of oil droplets is not the main mechanism affecting creaminess perception.

7.5 Acknowledgements

Eefjan Timmerman and Jerry van Maanen (WCFS, TNO) are acknowledged for assistance during samples preparation and Roelie Holleman (NIZO food research) for carrying out the Röse-Gottlieb determinations. Hetty Kroese and Jos Mojet (Centre for Innovative Consumer Studies) are acknowledged for the execution of the QDA tests and René de Wijk (WCFS, CICS) for the evaluation of the results.

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Chapter 8

Effect of droplet-matrix interactions on the lubrication properties of sheared emulsion-filled gels

A. Chojnicka & G. Sala, K. de Kruif, F. van de Velde, The interactions between oil droplets and gel matrix affect the lubrication properties of sheared emulsion-filled gels, to be submitted.

Abstract

In this chapter the lubrication behaviour of different emulsions-filled gels is related to their composition and structure. When considering the emulsions used for gel preparation, increasing the oil concentration resulted in a decrease of the friction coefficient. Emulsions with 40 wt% oil showed the same friction coefficient as the pure oil. The lubrication properties of the gels strongly depended on the molecular properties of the gelling agent and on the breakdown behaviour of the gel matrix. For each individual type of emulsion-filled gel, the lubrication behaviour was affected by the droplet-matrix interactions. For gels containing oil droplets bound to the matrix, the friction coefficient gradually decreased with increasing oil concentration. For gels containing oil droplets not bound to the matrix, the friction coefficient of the filled gels was lower than that of the same gel matrix without oil. However, no effect of the oil concentration on friction was observed. The different effects of the oil concentration on the lubrication behaviour of the different gels were explained by the relation between droplet-matrix interactions and 'apparent viscosity' of the broken gels. For gels with bound droplets increasing the oil concentration resulted in an increase of the 'apparent viscosity' of the broken gel. For gels with unbound droplets, the oil concentration did not affect the 'apparent viscosity'. Confocal Laser Scanning Microscopy (CLSM) observations of both emulsions and filled gels did not reveal coalescence of the oil droplets as a result of the shear treatment related to friction measurements.

8.1 Introduction

During oral processing, food products are confined to very thin films between the oral tissues. Tribology studies the mechanics of friction, lubrication and wear of interacting surfaces that are in relative motion. Tribology and thin-film rheology allow to mimic inmouth conditions (forces and surfaces) and are used to study the lubrication properties of food. Oral friction is influenced by: (i) the type of food consumed and its lubrication properties, (ii) the interactions between the lubricants and the surfaces, (iii) the properties of the oral tissues and (iv) physical parameters like the sliding to rolling motion between the tongue and palate as well as the force applied during food consumption. Thin-film rheological properties of foods have been related to the sensory perceptions of mouthfeel, texture and taste (de Vicente, Spikes & Stokes, 2006).

The behaviour of a lubricant between two rubbing surfaces is represented in the form of a Stribeck curve. In this curve the friction coefficient, defined as:

$$\mu = F_{\rm frie}/W \tag{8.1}$$

(where F_{fric} and W are the friction force and the normal load, respectively), is given as a function of the entrainment speed. The friction behaviour can be classified into three separate regimes, that are distinguishable within the Stribeck curve. The boundary lubrication regime is present at very low speeds, where the friction is affected by both the surface-surface interaction dominated by the asperities and ability of the lubricant to form a boundary interfacial film. In the hydrodynamic regime present at very high speeds, the surfaces are fully separated and the lubrication is governed by bulk rheological properties of the lubricant. Between those two regimes a mixed regime can be recognised, where the pressure of the fluid carries only a part of the load, while the other part is sustained by the surface asperities. In this case, the two surfaces are not fully separated (Cassin, Heinrich & Spikes, 2001; de Vicente et al., 2006). The pattern of the Stribeck curves strongly depends on the properties of lubricant and rotating materials, as well as on the experimental conditions applied during measurement.

For semi-solid foods containing emulsified fats and oils, an attempt was made to correlate the sensory attributes generated by a panel with rheological and friction properties (Weenen, H., Terpstra, M., Janssen, A., Jellema, R. H., De Wijk, R., Prinz, J., De Jongh, H. & Van der Linden, 2003a; Weenen, Van Gemert, Van Doorn, Dijksterhuis & De Wijk, 2003b; Jellema, Janssen, Terpstra, de Wijk & Smilde, 2005). For custards, the

mouthfeel attribute *creamy* was not correlated to small deformation measurements (dynamic stress and frequency sweep) or large deformation properties (flow curves and steady shear rate behaviour). The oral perception of these foods was reported to be related to their lubrication properties (de Wijk & Prinz, 2005) measured with a friction tester with a metal-rubber configuration. Increasing the fat content resulted in a decrease of the friction coefficient as well as in an increase of the product's creaminess. The decrease of friction observed as a result of the structure breakdown by amylase in starch containing products was explained with a surfacing mechanism of the oil droplets released from the starch matrix. The presence of particles causes on the other hand astringent sensations and higher friction. Similar results were found by Malone et al. for polymer solutions, emulsions and different types of milk (Malone, Appelqvist & Norton, 2003).

The lubrication properties of gels have not been studied extensively and those of sheared gels have not been reported. Chen et al. (Chen, Moschakis & Nelson, 2004) measured the surface friction of WPI gels and studied the relation between speed and friction, as well as the influence of the surface roughness of the gel on the surface friction.

The rheological properties and the breakdown behaviour of gels filled with emulsions droplets can be varied by changing the interactions between oil droplets and gel matrix, the oil content and the oil droplet size (Aguilera & Kinsella, 1991; Kim, Gohtani & Yamano, 1996; Kim, 2001; Sala, van Aken, Cohen Stuart & van de Velde, 2007; Sala, van Vliet, Cohen Stuart, van Aken & van de Velde, Submitted-a; Sala, van Vliet, Cohen Stuart, van de Velde & van Aken, Submitted-b). In previous studies we showed that the interactions between the oil droplets and the gel matrix in gelatine, κ -carrageenan and cold-set acid-induced whey protein isolates (WPI) gels could be varied by changing the emulsifying agent used for emulsion preparation. The oil droplets were bound to the matrix in gelatine gels containing emulsions stabilised by WPI, in *k*-carrageenan containing emulsions stabilised by lactoferrin and in WPI gels containing emulsions stabilised by WPI aggregates. This resulted for all gels in an increase of the gel modulus and a decrease of the fracture strain. In gelatine and k-carrageenan gels with bound droplets the fracture stress decreased, whereas in WPI gels it increased. The oil droplets were not bound to the matrix in gelatine gels containing Tween 20-stabilised emulsions and in κ -carrageenan containing emulsions stabilised by WPI. This gave a decrease in gel modulus and fracture stress. The fracture strain also decreased, but less than in gel with bound droplets.

In the study described in chapter 4, gels with unbound droplets or melting in the mouth were evaluated as more creamy (Sala, De Wijk, van de Velde & van Aken, 2008). It was hypothesised that for emulsion-filled gels the perception of mouthfeel attributes related to the presence of oil droplets could be mediated by the release of the droplets from the gel matrix upon oral processing. The study described in chapter 7 revealed that the release of the oil droplets is not the only mechanism explaining the perception of creaminess and fattiness in emulsion-filled gels (Sala, van de Velde, Cohen Stuart & van Aken, 2007). Therefore, we hypothesised that the lubrication behaviour of emulsion-filled gels might be another possible factor involved in their sensory perception mechanism. In this chapter we investigate the effect of the individual components of emulsion-filled gels on their lubrication properties by using a tribometer modified to obtain a low contact pressure. Our simulated environment mimics in that respect oral conditions. The effect of saliva on friction is also studied. The chosen systems are gelatine, κ-carrageenan and cold-set, acid-induced WPI gels, containing both bound and unbound oil droplets.

8.2 Materials and methods

8.2.1 Materials

Porcine skin gelatine PBG 07 (bloom 280, isoelectric point 8-9) was kindly provided by PB gelatines (Vilvoorde, Belgium). Kappa-carrageenan was kindly donated by CP Kelco (Lille Skensved, Denmark). The κ -carrageenan sample consisted of 93% mol κ -units and 7% mol ι -units, as determined by NMR spectrometry (van de Velde, Pereira & Rollema, 2004). Powdered whey protein isolate (WPI, BiproTM) was obtained from Davisco International Inc. (La Sueur, MN, USA). Tween 20 (Polyoxyethylene sorbitan monolaurate, in the text referred to as Tween) was obtained from Sigma (Sigma-Aldrich Chemie BV, Zwijndrecht, The Netherlands). Lactoferrin were kindly donated by DMV International, (Veghel, The Netherlands). Medium Chain Triglycerides (MCT) MIGLYOL 812N oil was purchased from Internatio BN (Mechelen, Belgium). Potassium chloride (p.a.) was obtained from Merck (Darmstadt, Germany). Glucono- δ -lactone (GDL) was kindly donated by Purac (Gorinchem, The Netherlands). All materials were used without further purification. All solutions were prepared with demineralised water.

8.2.2 Sample preparation

8.2.2.1 Emulsions

WPI solutions were prepared by adding the protein to the required amount of demineralised water. Subsequently, the solutions were gently stirred for 2 hours. Stock emulsions, consisting of 40 wt% MCT oil and 60 wt% aqueous phase containing 1 wt% WPI, were prepared by pre-homogenising the ingredients using an Ultra Turrax (Polytron, Kinematica AG, Lucerne, Switzerland) homogeniser. Pre-emulsions were further processed using a laboratory homogeniser (Ariete, Model NS1001L 2K – Panda 2K, Niro Soavi S.p.A, Parma, Italy). The same procedure was used for the preparation of the emulsions stabilised with Tween and lactoferrin, except that the emulsifying agent concentration in the aqueous phase was 2 wt%. WPI-stabilised emulsions were used for the preparation of filled gelatine gels and lactoferrin-stabilised emulsions for the preparation of filled κ -carrageenan gels. KCl was added to the emulsions used for the preparation of the preparation of so mM in the aqueous phase.

Emulsions stabilised with WPI aggregates were prepared as described above, but using a 3 wt% WPI aggregates dispersion as continuous phase. This dispersion was prepared by heating a 9 wt% WPI solution at 68.5°C for 2 hours and subsequent cooling to room temperature with tap water and subsequent dilution to 3 wt% with demineralised water. WPI aggregates-stabilised emulsions were used for the preparation of filled WPI gels.

The droplet size distribution of the obtained emulsions was measured using a Malvern Mastersizer 2000 (Malvern Instruments Ltd., Malvern, UK). The droplet volume-surface average or Sauter diameter $(d_{3,2})$ and other characteristics of the emulsions used for the preparation of the filled gels are reported in Table 8.1.

Emulsifier in the water phase	d _{3,2} (μm)	рН
1 wt% WPI	1.15	7.06
2 wt% Tween	0.10	4.30
2 wt% Lactoferrin	1.85	5.10
3 wt% WPI aggregates	1.45	6.64

Table 8.1 - Volume-surface average diameter (Sauter diameter) and pH of the emulsions used for the preparation of the filled gels.

8.2.2.2 Gels

Gelatine (4 wt%) and WPI (3 wt%) gels were prepared in demineralised water. Kappacarrageenan (0.6 wt%) gels were prepared in a 30 mM KCl solution. Samples were prepared without emulsion and with different oil concentrations (5, 10 and 20 wt%). In all samples the concentration of the gelling agent in the aqueous phase was kept constant.

To obtain efficient dissolution of κ -carrageenan and gelatine, the gelling agent was first allowed to hydrate for 2 hours under gentle stirring at room temperature. The samples were subsequently dissolved by heating at 80°C for 30 minutes and cooled to 45°C. For κ -carrageenan gels, prior to emulsion addition the emulsion was heated to 45°C before mixing. For gelatine gels, the gelling agent solution was allowed to cool to 20°C prior to mixing with the emulsion. This procedure was applied to prevent depletion flocculation of the emulsion droplets before gel formation (Sala et al., 2007). After mixing, the samples were allowed to gel at room temperatures in 60 ml plastic syringes (internal diameter 26.4 mm).

Gelation of the WPI gels was induced by addition of GDL (0.22 wt% in the case of WPI aggregates dispersion with a concentration of 3 wt%) to the WPI dispersion and to the WPI dispersion/emulsion mix and incubation at 25°C for 17 hours. The final pH of the gels was about 4.8. The WPI dispersion was prepared as described above.

8.2.3 Friction measurements

The lubrication properties of emulsifier solutions, emulsions and sheared gels were measured between two rotating surfaces in a Mini Traction Machine (MTM, PCS Instruments, London). A low contact pressure was assured by the selection of deformable materials: a neoprene ring and a silicone disk (Chojnicka, Visschers & de Kruif, Submitted). Figure 8.1 shows a schematic representation of the MTM tribometer.

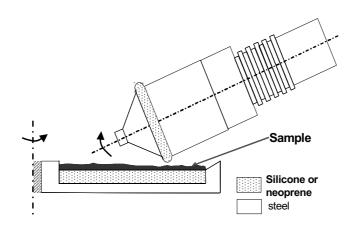


Figure 8.1 - Experimental setup for the friction measurements consisting of two essential parts: a neoprene ring and steel disk with a silicone sheet on the top. The dotted area represents the rubber surfaces in contact with each other. These surfaces are the source of friction.

Relevant physical parameters for friction measurements are the normal load (the force pressing the rubber ring against the disk), the temperature of the system, the tangential (entrainment) speed of the two rotating surfaces at the contact point and the slide to roll ratio, defined as

$$SRR = \frac{U_{disk} - U_{ring}}{U}$$
(8.2)

where the U_{disk} is the mean tangential speed of the disk, U_{ring} that of the ring and U the mean tangential speed at the contact between the surfaces. These physical parameters can be varied in the MTM tribometer.

The friction force was then measured as a function of the applied entrainment speed. In order to mimic oral relevant conditions, the mean speed of the ring and the disc was kept in a range between 10 and 100mm/s. As commonly used in literature, the SRR of 50 % was applied, which corresponds to a mixed rolling-sliding contact. This type of contact was chosen to minimize possible wear damage to the soft surfaces. The temperature was set to $37^{\circ}C$ ($\pm 1^{\circ}C$) degrees, as present in the human mouth, while the normal load was chosen to be 3 and 5N. Since only a part of the Stribeck curve was recorded, the results will be referred to as friction curves. For gelatine gels friction measurements were also

carried out at 20°C. Before each experiment all the rubbers were cleaned with an ethanol, demineralised water and dried with compressed air.

For all systems studied the tribometer reservoir was filled to assure that the lubricant was present between the rotating surfaces. Measurements were carried out in triplicate.

8.2.4 Rheological measurements

The 'apparent viscosity' of the gels broken by forcing them out of the syringe in which they were prepared was measured at 37° C using a standard rheometer (AR 2000, TA Instruments, Leatherhead, UK) with a vane geometry. For gelatine gels also measurements at 20°C were carried out. The vane had four blades, a diameter of 28 mm, a height of 42 mm and was used in combination with a cylindrical shaped cup with a diameter of 70 mm. After lowering the vane into the broken gel, rotating movements were applied. The 'apparent viscosity' was measured at steady shear rate as a function of time. The experiments were done with two steps. First, a step at a shear rate of 10 s⁻¹ was applied during 2 minutes. Then a step at a of shear rate 100 s⁻¹ followed during 5 minutes. The data collected at a shear rate of 100 s⁻¹ were used for analysis.

8.2.5 Confocal Laser Scanning Microscopy (CLSM)

The microstructure of the emulsion-filled gels was visualised with Confocal Laser Scanning Microscopy. Observations were made on the gels before and after friction measurements as well as on the silicone rubber used. To visualise the protein phase the unbroken gels were stained with Rhodamine B (0.2 wt% solution; 10 µL per mL sample). With this staining agent the oil droplets are visualised as holes within the protein matrix. After the friction measurements a combination of Fluorescein isothiocyanate with Nile Red (FITC/NR) was used to stain the protein and oil phases, respectively. Nile Blue was chosen as a staining agent of the oil droplets in order to specifically reveal possible coalescence or aggregation. CLSM-images were recorded on a LEICA TCS SP Confocal Laser Scanning Microscope (Leica Microsystems CMS GmbH., Manheim, Germany), equipped with an inverted microscope (model Leica DM IRBE), used in the single photon mode with an Ar/Kr visible light laser. A Leica objective lens (63x/UV/1.25NA/water immersion/PL APO) was used. The excitation wavelength was set at 568 nm for Rhodamine B and Nile Red, and at 488 nm for FITC and Nile Blue. Digital image files were acquired in tagged image file format and at 1024x1024 pixel resolution.

8.3 Results

The aim of the work was to establish the link between the lubrication properties of emulsion-filled gels and their composition and structure. To achieve this goal, the contribution of all components of the gel systems to the lubrication properties of the filled gels had to be studied. Therefore, lubrication measurements were carried out on the individual components of the gel. For both the emulsions and the gels the effect of the oil concentration on lubrication properties was studied. Furthermore, in order to simulate oral conditions the role of saliva in the lubrication behavior of all systems was studied.

8.3.1 Lubrication properties of the emulsions

Figure 8.2 shows the friction coefficient as a function of the entrainment speed for the WPI stabilized emulsion and its components. Clear differences between friction coefficients of the different systems were observed. A mixed lubrication regime was observed for water, the WPI solution and the 10 wt% emulsions for the whole range of the speeds measured. The friction coefficient of the solution of the emulsifying agent was about 0.2 lower than that of water. Ten wt% oil in the emulsion remarkably improved the lubrication properties compared to the emulsifying agent. At oil concentrations above 10 wt% friction weakly depended on oil concentration and an increase of the oil concentration up to 40 wt% led to only a slight decrease of the friction coefficient. At this oil concentration the hydrodynamic regime appeared to dominate over the whole range of speeds. In the hydrodynamic regime the lubrication properties are determined by the oil droplets entering the contact zone. When MCT oil was used as a lubricant the lubrication behaviour was about the same as that measured for the emulsion with 40 wt% oil. This suggests that this oil concentration is sufficient to achieve the same lubrication properties of MCT oil. For the other emulsifying agents the friction curves of their solutions and of the emulsions were comparable to those shown in Figure 8.2 (results not shown).

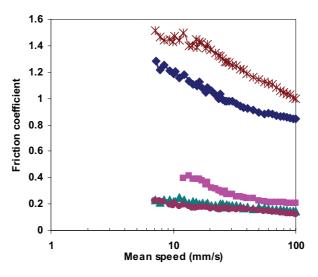


Figure 8.2 – Friction curves of the components of WPI stabilised emulsions (X: water; \bigstar : solution 1 wt% WPI; \blacksquare emulsion with 10 wt% oil \blacktriangle : emulsion with 40 wt% oil; \blacklozenge : MCT oil; Load: 3 N).

In Figures 8.3.A and 8.3.B the friction coefficients for the different emulsions are plotted as a function of the oil concentration at the entrainment speeds of 10 and 100 mm/s, respectively. For all emulsions the emulsifying agent solutions had higher friction coefficients compared with the emulsions in which they were used. For the protein solutions (WPI, WPI aggregates and lactoferrin), the friction coefficient at an entrainment speed of 10 mm/s was 1.2, while that of the solution of 2 wt% Tween 20, which is a synthetic surfactant, was 0.4. For almost all the emulsions with an oil content of 10 wt%, a large decrease of the friction coefficient (to ~ 0.4) compared to the emulsifying agent solutions was observed. The emulsion stabilised by 3 wt% WPI aggregates showed higher friction (~ 0.8) than the emulsions stabilised by the other emulsifying agents. For all types of emulsion, an increase of the oil concentrations up to 40 wt% yielded lower values of the friction coefficient, comparable to that obtained for MCT oil. The lubrication properties of the emulsion at low oil concentration appear to be determined by both the emulsifying agent and the oil droplets concentration. On the other hand, at high oil concentration these properties appear to be only affected by the oil droplets. For both speeds a similar behaviour was observed. However, friction was lower at higher velocity as is expected for a mixed lubrication regime.

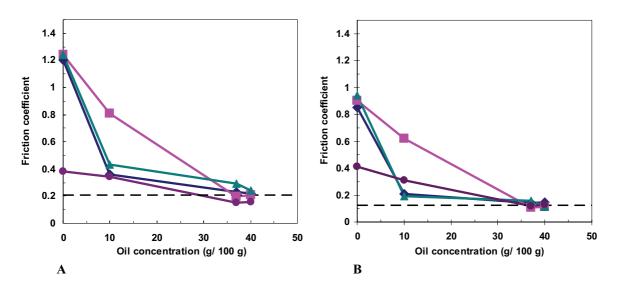


Figure 8.3 – Friction coefficient vs. oil concentration for emulsions stabilised by different emulsifying agents and for MCT oil (\diamond : 1 wt% WPI; \blacksquare 3 wt% WPI aggregates; \blacktriangle : 1 wt% lactoferrin; \bullet : 2 wt% Tween 20. The dashed line represents the friction coefficient of pure MCT oil. Load: 3 N. A: Entrainment speed= 10 mm/s; B: Entrainment speed= 100 mm/s).

Table 8.2 shows the effect of the saliva on the friction coefficient of the four different emulsions with 40 wt% oil, stabilized by different emulsifying agents at 10 and 100mm/s. Differences in friction coefficient between the emulsions could be only observed at low speed. No significant differences were observed between the systems with 7 wt% water and those with the same amount of saliva. It seems evident that saliva does not affect friction. An exception was the lactoferrin-stabilised emulsion, for which the friction coefficient with saliva was 30% lower compared to that for the emulsions with added water. In this case complexation between lactoferrin, which is positively charged at the pH of the emulsion, and the negatively charged mucins present in saliva might occur. This can lead to aggregation of emulsion droplets caused by saliva addition, as reported by Silletti et al. (2007). Aggregation of oil droplets could decrease friction by two different mechanisms. It could either result in an increase of the effective viscosity of the emulsion or facilitate the entrance of the oil droplets into the contact zone between disk and ring.

Emulsifying agent	Entrainment speed					
	10	mm/s	100 mm/s			
	7 wt% water	7 wt% saliva	7 wt% water	7 wt% saliva		
1% WPI	0.23	0.25	0.14	0.15		
3% WPI	0.20	0.21	0.11	0.12		
1%lactoferrin	0.29	0.19	0.16	0.10		
2% Tween	0.15	0.19	0.12	0.16		

Table 8.2 – Effect of water and saliva on friction coefficient in emulsions with 40 wt% oil and stabilised by different emulsifying agents (entrainment speeds: 10 and 100 mm/s).

8.3.2 Lubrication properties of the gels without oil

In a preliminary phase of the study, the gels were allowed to gel on top of the silicon disc used in the MTM tribometer for friction measurements. Following this procedure only 5 ml of the sample could be used for measurement. In this case the gelled samples were destroyed by the rotating surfaces within a few seconds from the beginning of the measurements. The destruction of the gels was uncontrolled and part of the samples fell off the disc. As a consequence, the rotating surfaces were not constantly in contact with the lubricant. Therefore, a technique to break the gel in a controlled way was optimised. The gels were prepared in syringes with a capacity of 60 ml. Prior to friction measurement, the emulsion-filled gels systems were destroyed by pushing them out of the syringe in which they were prepared. The destroyed gels consisted of thick, viscous, pourable fluids. The homogeneity of these fluids was only visually evaluated and varied with the type of gel matrix. Before starting the friction measurements a quantified amount of destroyed gel was spread on the top of the silicone disc placed in the tribometer.

The friction curves of the three gel matrices without oil droplets are shown in Figure 8.4. The friction curve of gelatine was lower than those of κ -carrageenan and WPI. The temperature of 37°C was applied during these measurements to mimic oral conditions. Since at this temperature gelatine gels were melted, for these gels friction measurements were carried out also at 20°C, at which they were not melted. For gelatine gels the friction coefficient measured at 20°C was only slightly lower that that measured at 37°C. At 20°C gelatine gels broke down into a highly homogeneous material. Consequently, the

lubrication behaviour of gelatine gels without oil droplets is only partially related to their physical state (melted/ gelled).

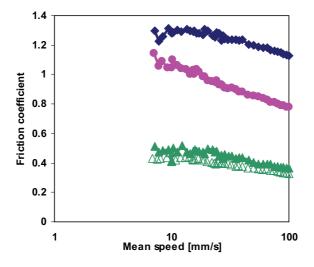


Figure 8.4 – Friction curves of the three gel matrices studied (\diamond :WPI; \blacktriangle : gelatine 37°C; Δ : gelatine 20°C; \bullet κ -carrageenan; Load: 3 N).

Broken κ -carrageenan and WPI gels were visually less homogenous, resulting in a large variation in the distribution of the gel particles. The latter sample (WPI) broke down into relatively large pieces and serum was released. In this sample, the lubrication properties were probably dominated by the exuded water phase with small pieces of broken down gel, whereas large gel particles were not entering the contact zone between the two rotating parts. As a result, WPI gels had the highest friction coefficient compared to the two other systems. Compared to WPI, the κ -carrageenan gels broke down into more defined and homogenous structures, which may explain the lower friction coefficient.

8.3.3 Lubrication properties of the filled gels

The presence of oil droplets in the gel matrix remarkably affected the lubrication behaviour of the gels. For gelatine gels, the effect of the oil droplets on lubrication properties was temperature-dependent. For gels containing oil droplets, the friction coefficient as measured at 100 mm/s and at 37°C was lower than that of gels without oil only in systems containing the emulsion stabilised by Tween 20, i.e. gels with unbound droplets (Figure 8.5). For these gels the friction coefficient decreased to 0.15 at 5 wt% oil

and remained approximately constant with a further increase of the oil content. No effect of the presence of oil droplets was observed for the gelatine gels containing the 1 wt% WPI-stabilised emulsion (gels with bound droplets); a friction coefficient of 0.4 was found for all gels. During the measurement, gelatine gels both with bound and unbound droplets were melted, resulting in a homogenous, emulsions-like fluids. The observed results suggest that under these conditions the gelatine matrix determines the lubrication. The melted gelatine, due to its very sticky properties, may form a film between the surface of the disk and that of the ring, masking the effect of the emulsion droplets. No effect on the friction of the water or saliva was observed for the gelatine gels. Friction measurements performed at 20°C showed a gradual decrease of the friction coefficient of gelatine gels containing the WPI-stabilised emulsion (unbound droplets, Figure 8.6). For gelatine gels containing the Tween-stabilised emulsion (unbound droplets) no effect of temperature on friction was observed (Figure 8.6).

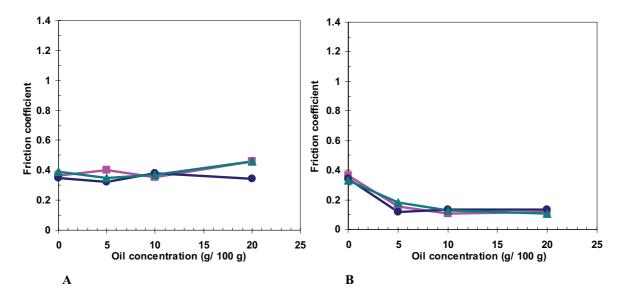


Figure 8.5 – Friction coefficient vs. oil concentration for gelatine gels (\blacksquare) with either bound (A) or unbound (B) droplets and for the same gels after addition of either 7 wt% water (\bullet) or 7 wt% saliva (\blacktriangle). Measurements temperature: 37°C. (Entrainment speed: 100 mm/s; Load: 3 N).

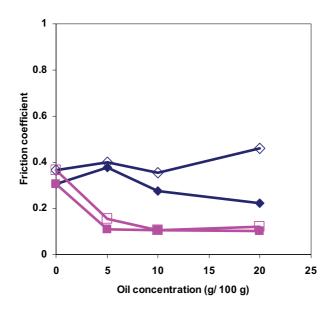


Figure 8.6 – Friction coefficient vs. oil concentration for gelatine gels with either bound (\blacklozenge) or unbound (\blacksquare) droplets and at two different temperatures. (Open symbol: 37°C; filled symbol: 20°C) (Entrainment speed: 100 mm/s; Load: 3 N).

For κ -carrageenan gels, a significant decrease of the friction coefficient to 0.2 was observed already at 5 wt% oil (Figure 8.7). Further increase of the oil concentration did not affect the friction coefficient. For both gels with bound and unbound droplets no effect on friction was observed of dilution with 7 wt% water or saliva. Both the emulsions stabilised by lactoferrin and 1 wt% WPI showed a friction coefficient of about 0.2 already at 10 wt% oil (Figure 8.3). This value of the friction coefficient is comparable to that of the κ -carrageenan filled gels. Figure 8.7 shows that for κ -carrageenan the interactions between droplets and matrix do not have an effect on lubrication.

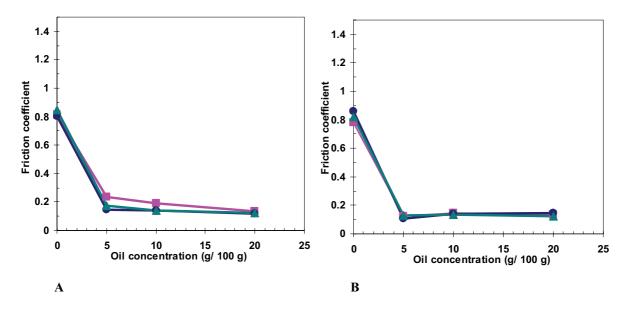


Figure 8.7 – Friction coefficient vs. oil concentration for κ -carrageenan gels (**a**) with either bound (A) or unbound (B) droplets and for the same gels after addition of either 7 wt% water (•) or 7 wt% saliva (**A**). (Entrainment speed: 100 mm/s; Load: 3 N).

Figure 8.8 shows the effect of the oil concentration on the friction coefficient of WPI gels. These gels contain emulsions stabilized by 3 wt% WPI aggregates, which lead to oil droplets bound to the matrix. A small amount of oil (5 wt%) present in the gel did not improve the lubrication properties significantly with respect to the gel matrix without the oil (~ 1.1). However, at oil concentrations above 5 wt% a gradual decrease of the friction coefficient was observed. At 20 wt% oil a friction coefficient of 0.2 was reached. For the emulsion stabilised by 3 wt% WPI aggregates this value of the friction coefficient was obtained at 40 wt% of oil concentration (Figure 8.3). This suggests that a synergy between gel matrix and emulsion droplets may exist, lowering the lubrication properties of these gels with increasing oil concentration. As compared to gelatine and κ -carrageenan gels, the friction coefficient observed for WPI gels at any oil concentration below 20 wt% is higher.

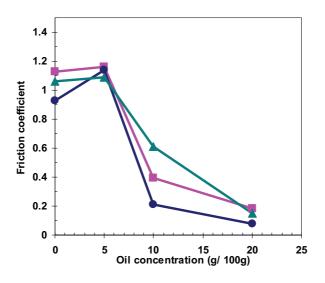


Figure 8.8 – Friction coefficient vs. oil concentration for WPI gels with bound droplets (\blacksquare) and for the same gels after addition of either 7 wt% water (\bullet) or 7 wt% saliva (\blacktriangle) (Entrainment speed: 100 mm/s; Load: 3 N).

8.3.4 Rheological properties of the broken gels

The behaviour of lubricants in the mixed and hydrodynamic regime are known to be related to their viscosity. Higher viscosity values usually correspond to lower friction coefficients. In order to ascertain whether this holds also for broken emulsion-filled gels, the 'apparent viscosity' of the broken gels was measured with a rheometer using a vane geometry. Figure 8.9 shows the 'apparent viscosity' of κ -carrageenan gels with different oil concentrations at fixed shear rate. A slight decrease of the 'apparent viscosity' in time was observed in this case as well as for all the other gels. This was attributed to the breakdown of the gel structure during measurement. To standardise the results, the 'apparent viscosity' values at a shear rate of 100/s were more reproducible than at lower shear rate. The relative differences in 'apparent viscosity' observed at 100 seconds between samples with different oil content remained constant in time.

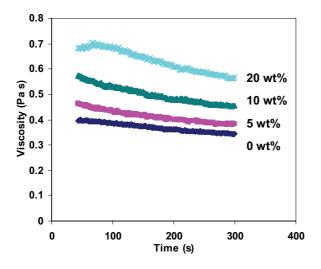


Figure 8.9 – 'Apparent viscosity' of broken κ -carrageenan gels with bound droplets at different oil concentrations (\diamond : 0 wt% oil; \blacksquare : 5 wt% oil; \blacktriangle : 10 wt% oil **x**: 20 wt% oil) (Shear rate 100/s).

The effect of the oil concentration on the 'apparent viscosity' of the broken gel depended on the interactions between oil droplets and gel matrix. For k-carrageenan and WPI gels with bound droplets, an increase of the 'apparent viscosity' was observed with increasing oil concentration (Figure 8.10A). For gelatine gels, the effect of the oil concentration was temperature dependent. When the 'apparent viscosity' was measured at 37°C gelatine gels were melted. Under these experimental conditions very low viscosities and no effect of the oil concentration were observed (Figure 8.10 B). When the measurements were performed at 20°C, the 'apparent viscosity' of broken gelatine gels with bound droplets increased with increasing oil concentration (Figure 8.10B). For gels with unbound droplets increasing the oil concentration above 5 wt% did not affect 'apparent viscosity' (Figure 8.10). For κ -carrageenan gels with unbound droplets, the 'apparent viscosity' of the filled gels was higher than that of the gel without oil droplets (Figure 8.10A). For gelatine gels with unbound droplets, the 'apparent viscosity' of the filled gels was lower than that of the gel without oil droplets (Figure 8.10B). For these gels, only a slight decrease was observed with increasing the oil concentration from 10 to 20 wt%. This is possibly related to an increasing concentration of Tween in the gel. This emulsifier is likely to perform a lubricating action between the gel particles present in the mass of the broken gel, decreasing the adhesion and cohesion forces.

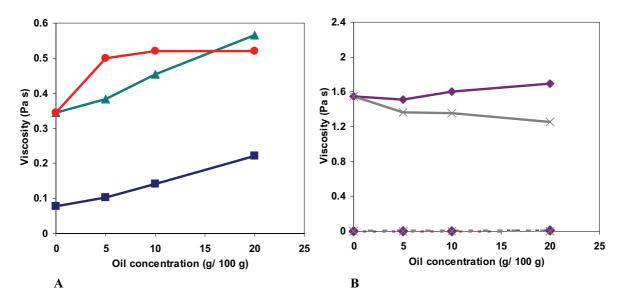
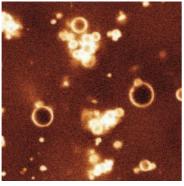


Figure 8.10 – 'Apparent viscosity' of the broken gels vs. oil concentration. A: WPI gels with bound droplets (\blacksquare) and κ -carrageenan gels with bound (\blacktriangle) and unbound (\bullet) droplets. B: gelatine gels with bound (\bullet) and unbound (\bigstar) and unbound (\bigstar) droplets; measurements performed at 37°C (dotted line) and 20°C (solid line) (Shear rate 100/s).

8.3.5 Effect of shearing on microstructure of filled gels

The microstructure of the gels studied in this work has already been described in the previous chapters (Sala et al., 2007; Sala et al., Submitted-a). In gelatine and WPI gels the oil droplets were non-aggregated, whereas in κ -carrageenan gels, independently on the droplet-matrix interaction, the oil droplets were aggregated.

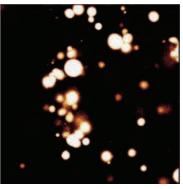
Possible changes in the microstructure of the gels as a result of the friction measurements, with particular attention to the coalescence of the oil droplets, were studied by CLSM microscopy. CLSM images were taken for each gel before and after friction measurements. Furthermore, the silicon discs used in the friction measurements were searched for traces of free oil, which could results from coalescence of the oil droplets during measurements. Migration of the oil droplets within the broken down gels was observed for gels with unbound droplets (Figure 8.11). Nevertheless, by CLSM microscopy no coalescence could be observed (Figure 8.11).



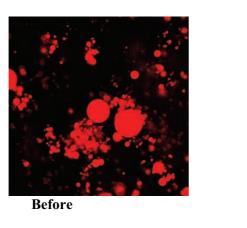
Before

A

B



After





After

Figure 8.11 - CLSM images of k-carrageenan gels with either bound (A) or unbound (B) droplets, before and after friction measurement (5 wt% oil; image size $39.7 \times 39.7 \mu$ m).

8.4 Discussion

The lubrication properties of the oil in water emulsions used in this study are in agreement with the results of Vicente et al. (2006) for oil in water (O/W) emulsions. Vicente et al. (2006) studied the lubrication properties of oil-in-water emulsions in a steel-soft elastomer contact. They found that lubrication is determined by the ratio of the viscosities of the two phases. If the viscosity of the oil is at least 4 times larger than the viscosity of the dispersion medium, the oil droplets enter the contact zone and dominate the lubrication properties. Otherwise the friction is controlled by the aqueous phase. The viscosity of MCT oil is about 5 mPa s, i.e. about 5 times the viscosity of the water phase of the emulsions. The large decrease of the friction coefficient observed in this study already at

an oil concentration of 10 wt% shows that also in the systems studied here the oil droplets enter the contact zone between the silicone disc and the neoprene ring, affecting the lubrication behaviour of the emulsions. The agreement between our results and those of Vicente et al. (2006) holds, in spite of the difference in experimental conditions. In our study a silicone-neoprene contact was chosen, while Vicente et al. worked with a steel-soft elastomer contact.

The limited decrease of friction coefficient with increasing oil concentration above 10 wt% is in agreement with the results reported also by de Hoog et al. (de Hoog, Prinz, Huntjens, Dresselhuis & van Aken, 2006). In this study a custom-made friction apparatus was used with materials with different surface properties like glass, rubber, pig's tongue surfaces. The authors showed that when mucosal surfaces were used and in the range of oil concentration between 10 and 40 wt% the friction coefficient of emulsions stabilised by WPI did not depend on the oil concentration. Furthermore, the surface characteristics were shown to have a large effect on friction.

The different emulsifying agents showed different lubrication behaviours. As compared to proteins, the friction coefficient of the 2 wt% Tween solution and of emulsions stabilised by this surfactant were in general lower (Figure 8.3). Tween 20 is more active in decreasing the surface tensions of systems in which it is contained and might interact with the rubber surfaces and modify them through adsorption. Furthermore, Tween 20 forms micelles already at concentrations above 0.007 wt% (Malik & Jhamb, 1970). Therefore, at the concentration used in our work this surfactant is present as micelles. This could effectively lower friction for all Tween-stabilised emulsions within the whole range of speeds.

The lubrication properties of different gel matrices without oil droplets are likely to be governed by several factors, like the molecular properties of the gelling agent and the homogeneity of the broken gel. For WPI gels (Figure 8.4), which show relevant water phase exudation, the friction is high and is described by two different lubrication regimes. Up to a speed of 25 mm/s no effect of the speed on the friction coefficient is visible. This by definition implies that friction is in the boundary regime. At higher speed the friction coefficient starts to decrease with increasing speed, indicating the beginning of the mixed regime. For κ -carrageenan gels, which break down to a more homogeneous material, a continuous decrease of the friction coefficient with increasing speed is observed, indicating a mixed regime over the whole range of speeds. The shape of the friction curve of gelatine gels, as measured at 20°C, indicates two lubrication regimes in the speed range studied, as described for WPI gels. The lower friction coefficient observed for gelatine gels as compared to WPI gels is probably due to the higher homogeneity, the fluid-like behaviour and the adhesiveness of broken gelatine gels.

For all gel matrices, the mixed regime of lubrication was observed. Therefore, the bulk rheological properties of the lubricant will partly affect friction. For this reason, the relation between friction coefficient and 'apparent viscosity' of the broken gels was studied. When comparing the results for the different matrices, it is clear that the 'apparent viscosity' of the broken gel is not the only factor determining the lubrication properties (Figure 8.11). The 'apparent viscosity' of broken gelatine gels is several times higher than that of WPI gels. Nevertheless, for gels with 20 wt% oil similar friction coefficients are observed.

When considering the effect of the oil concentration for each individual types of gels, the effect of 'apparent viscosity' on friction and the dependence of this effect on the interaction between oil droplet and gel matrix can be clearly observed (Figure 8.12). For gels with bound droplets, the 'apparent viscosity' increases with increasing oil concentration and the friction coefficient decreases with increasing 'apparent viscosity'. For these gels, the observed increase in 'apparent viscosity' with increasing oil concentration is related to the increase in gel modulus (i.e. lower deformability of the particles) (Sala et al, 2007; Sala et al., Submitted-a) and to a different breakdown pattern. With increasing oil concentration, the increase in modulus results in particles of the broken gels with higher stiffness. Furthermore, with increasing oil concentration gels with bound droplets become more brittle and break down in smaller pieces, resulting in a more homogenous mass. For gels with unbound droplets, no effect of the oil concentration above 5 wt% on 'apparent viscosity' was observed (Figure 8.10). Furthermore, for these gels no relationship was observed between friction coefficient and 'apparent viscosity' (Figure 8.12). This is likely related to the effect of oil concentration on gel modulus and breakdown properties. For these gels, increasing the oil concentration results in a decrease of the gel modulus and has only a minor effect on gel brittleness. Therefore, increasing oil concentration is likely to only slightly affect the homogeneity of the broken mass.

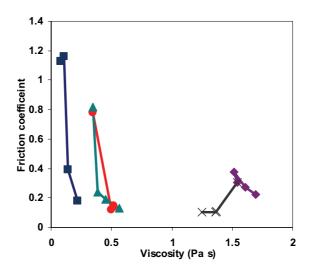


Figure 8.12 – Friction coefficient vs. 'apparent viscosity' of the broken gels (\blacklozenge : gelatine gels with bound droplets; X: gelatine gels with unbound droplets; \blacktriangle : κ -carrageenan gels with bound droplets; \blacklozenge : κ -carrageenan gels with unbound droplets; \blacksquare : WPI gels with bound droplets. For gelatine gels both 'apparent viscosity' and friction coefficient were measured at 20°C, whereas for κ -carrageenan and WPI gels these measurements were carried out at 37°C. (Entrainment speed 100 mm/s; Load: 3 N; Shear rate 100/s).

The effect of the oil concentration on 'apparent viscosity' is not the only factor explaining the large decrease in friction coefficient observed for gels containing oil droplets, as compared to the gels without oil. For gels with bound droplets, oil droplets present in the smallest gel pieces will affect friction like it happens for emulsions. For gels with unbound droplets, also free droplets will be present in the mass of broken gel (Sala et al., 2007). These droplets can affect friction directly. The lubrication properties of gels with unbound droplets are likely to be determined by the individual contribution of gel matrix and released oil droplets. The overall effect of the oil droplets on friction does not appear different between gels with bound droplets and gels with unbound droplets. The lower friction coefficient of gelatine gels with unbound droplets as compared to gelatine gels with bound droplets is likely to be related to the effect of Tween 20.

In chapters 4 and chapter 7 we showed that the scores for mouthfeel attributes related to the presence of oil droplets in the gel matrix (e.g. *creamy* and *fatty*) increase with increasing oil concentration for gels with both bound and unbound droplets. The similarity of the lubrication properties of gels with bound and unbound droplets is in agreement with these findings. A relationship between the lubrication properties of broken gels and the perception of sensory attributes related to the presence of oil droplets in the gel matrix can be hypothesised.

8.5 Conclusions

The lubrication behaviour of gels is largely determined by the molecular and functional properties of the gelling agent. The inclusion of oil droplets in the gel matrix remarkably changes the lubrication properties of the gels. These changes depend on the droplet-matrix interactions. The changes observed for gels with bound droplets are related to the increase in 'apparent viscosity' of the broken gel mass. For gels with unbound droplets the decrease of the friction coefficient is likely to be the result of the individual contribution of gel matrix and released oil droplets. In spite of the two different mechanisms, the overall effect of the oil droplets on friction does not remarkably differ between gels with bound droplets and gels with unbound droplets, which is in agreement with findings of sensory studies on this type of systems described in chapter 7.

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Summary and conclusive remarks

This thesis reports studies on the large deformation and lubrication properties of emulsionfilled gels, and the way these properties are related to the sensory perception of the gels. Understanding sensory perception mechanisms related to the presence of emulsion droplets in the gel matrix is of basic importance to produce foods with reduced fat but unchanged sensory properties.

Many dispersions or solutions of gelling agents containing oil droplets show phase separation phenomena caused by different physicochemical mechanisms and the preparation of stable, homogenous systems is often difficult. **Chapter 2** reports the optimisation of the preparation of WPI emulsion-filled gels. For emulsions stabilised by native WPI, creaming was observed upon mixing of the emulsion with a suspension of WPI aggregates, likely as a result of depletion flocculation induced by the differences in size between the droplets and aggregates. These systems resulted in non-homogeneous gels. Stable and homogeneous emulsion-filled gels were prepared by cold gelation of emulsions stabilised by a suspension of heat denatured WPI. This chapter describes also the rheological properties of these gels at small and large deformation obtained in a first explorative investigation.

After developing a set of suitable model gels, the chosen approach was to firstly investigate the effect of the oil droplets on the large deformation properties of the gels at constant and relatively low deformation speed, as usually reported in literature. The selected gels were gelatine, κ -carrageenan and WPI gels containing emulsion droplets stabilised by various emulsifying agents, i.e. with varying interactions with the gel matrix. Chapter 3 deals with the large deformation properties of these gels. For gelatine gels, depending on the emulsifying agent used for emulsion stabilisation, the Young's modulus either increased or decreased. It was concluded that in the first case the oil droplets were bound to the gel matrix and that in the latter case the oil droplets were unbound. For WPI gels, only filled gels with bound droplets could be obtained. The variations of the Young's modulus observed for κcarrageenan gels were mainly related to interactions between k-carrageenan and the emulsifying agent present in the aqueous phase. Theories based on the effect of the oil content on modulus satisfactorily fitted the trend of the experimental results, both for bound and unbound droplets. The fracture strain decreased with increasing oil content for bound droplets and remained constant for unbound droplets, while the fracture stress was unaffected by bound droplets and decreased in the case of unbound droplets. Theories describing the effect of filler content on fracture strain and stress failed to predict the experimental results.

The role of gel matrix and oil content in the sensory perception of the model gels was also studied. **Chapter 4** reports the results of an explorative sensory study in which the

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selected model gels and κ/ι -carrageenan gels were characterised. The emulsion droplets were homogeneously distributed in WPI gels, slightly aggregated in mixed κ/ι -carrageenan and extensively aggregated in κ -carrageenan gels. For gelatine, gels with either non-aggregated or aggregated emulsion droplets could be prepared by modifying the processing conditions. The sensory properties of the gels were mainly controlled by the matrix. At increasing oil content the perceived creaminess and spreadability of the samples increased. For gelatine, κ carrageenan and mixed κ/ι -carrageenan gels, i.e. for gels melting at the oral processing temperature or containing unbound oil droplets, the creaminess scores were consistently higher than for WPI gels, which were perceived as more rough. For gelatine gels, the aggregation of the oil droplets had no effect on sensory perception. No relevant correlations were found between the large deformation properties of the gels determined at constant deformation speed and the sensory attributes.

In a successive phase of the work the effect of the deformation speed on the large deformation properties of the gels was studied. The motivation of this choice was twofold: to acquire a better knowledge on the effect of the oil droplets on the rheological properties of the gels and to determine the large deformation properties of the gels at deformation speeds similar to those observed during oral processing. Chapter 5 deals with the effect of deformation speed on the large deformation and viscoelastic properties of the selected model gels. The gelling agent concentration and the oil droplet size were kept constant. The rheological properties of the gel matrices controlled the compression speed dependency of the gels containing oil droplets. Polymer gels (gelatine and k-carrageenan gels) showed a predominantly elastic behaviour. Their Young's modulus was not affected by the compression speed. The increase of fracture stress and strain observed with increasing compression speed was related to friction between the structural elements of the gels and, for gelatine, to the unzipping of physical bonds. Particle gels (WPI gels) showed a more viscoelastic behavior. Their Young's modulus and fracture stress increased with compression speed. This was attributed to the viscous flow of the matrix and friction phenomena between structural elements of the gel. The effect of an increase in the oil volume fraction on the Young's modulus was for all gels according to the van der Poel theory. Oil droplets embedded in the gel matrix acted as stress concentration nuclei and increased friction. The relative impact of these two effects was related to the viscoelastic properties of the gels and to droplet-matrix interaction. For polymer gels and gels with bound droplets stress concentration phenomena played a relatively larger role. For viscoelastic gels and gels with unbound droplets friction

phenomena were relatively more important, increasing the viscoelastic character of the gels. As a result, an increase in oil volume fraction resulted in a decrease of both fracture stress and fracture strain for polymer gels and in an increase of the fracture stress for WPI gels.

Chapter 6 deals with the large deformation and viscoelastic properties of model gels with constant oil content, but varying gelling agent concentration and oil droplet size. An increase in the concentration of gelling agent resulted in denser gels with more bonds between structural elements. This induced an increase of both Young's modulus and fracture stress for all gels. With increasing gelling agent concentration, polymer gels (gelatine and κ -carrageenan) became less strain-hardening and the particle gels (WPI) even became strainweakening. The effect of a decrease in the oil droplet size on the Young's modulus was generally according to the van der Poel theory, unless when the oil droplets were aggregated. Moreover, a decrease in oil droplet size induced a decrease of the fracture strain in gels with non-aggregated bound droplets. The extent of these changes depended on the gelling agent concentration. The effect of a decrease of the oil droplet size on other fracture parameters and in other gel systems was minor. For gels with non-aggregated bound droplets, the effect of a reduction of the oil droplets size on fracture properties resembled that observed with increasing oil volume fraction. For these gels, a reduction in oil droplet size could mimic an increase in oil volume fraction.

The droplet-matrix interactions were assumed to have an effect on the release of the oil droplets from the gel matrix during oral processing. Therefore, a method to determine the oil droplets release upon gel shearing was optimised and the behaviour of the oil droplets in the different model gels was characterised. The role of oil droplet release on sensory perception was investigated. These aspects are described in **chapter 7** for the selected model gels. At 20°C no release was observed for gels containing droplets bound to the matrix, whereas the release measured for gels with unbound droplets related to the fat content and the size of the gel particles obtained after shearing. For gels with bound droplets and melting at the oral processing temperature, increasing the temperature of the determination to 37°C resulted in an almost complete release of the oil droplets. An increase of the oil content induced an increase of the creaminess scores for all gels. These scores were somewhat higher for gels containing unbound droplets and gels melting at oral processing temperature. For these gels, the oil droplet release appeared to correlate with creaminess. However, because a similar increase in creaminess at increasing oil content was also found for gels with oil droplets bound to the matrix, it was concluded that the release of oil droplets during oral processing is not the main mechanism causing creaminess perception in emulsion-filled gels.

After ascertaining the limited role of the release of oil droplets in sensory perception, it was decided to study the lubrication properties of filled gels and the role played in these properties by individual gel components and saliva. The results of this part of the work are discussed in chapter 8. In this study the gels were sheared so as to resemble a broken gel resulting from oral processing. When considering the emulsions used for gel preparation, increasing the oil content resulted in a decrease of the friction coefficient. Emulsions with 40 wt% oil showed the same friction coefficient as the pure oil. The lubrication properties of the gels strongly depended on the molecular properties of the gelling agent and on the breakdown behaviour of the gel matrix. For each individual type of emulsion-filled gel, the lubrication behaviour was affected by the droplet-matrix interactions between oil droplet and matrix. For gels containing oil bound droplets, the friction coefficient gradually decreased with increasing oil content. For gels containing unbound droplets, the friction coefficient of the filled gels was lower than that of the same gel matrix without oil. However, no effect of the oil content on friction was observed. The different effects of the oil content on the lubrication behaviour of the different gels were explained with the relation between droplet-matrix interactions and 'apparent viscosity' of the broken gels. For gels with bound droplets increasing the oil content resulted in an increase of the 'apparent viscosity' of the broken gel. For gels with unbound droplets, the oil content did not affect viscosity. Confocal Laser Scanning Microscopy (CLSM) observations of both emulsions and filled gels did not reveal coalescence of the oil droplets as a result of the shear treatment during friction measurements.

The study of the large deformation properties of emulsion-filled gels described in this thesis focused on the first fracture event occurring upon compression. The effect of the droplet-matrix interactions on the 'apparent viscosity' of broken gels, observed when studying the lubrication properties of these systems, indicates the relevance of the successive fracture events for the properties of gels processed in the mouth. Gels with the same matrix and oil content, but with different droplet-matrix interactions are broken down in the mouth into systems with different rheological properties. The findings obtained in this thesis allow to propose a mechanism relating the effect of the oil droplets on the first fracture event and the properties of an extensively broken gel. With increasing oil content, gels with bound droplets become more brittle and are likely broken down in smaller pieces, resulting in a more homogenous mass, without visible large particles. Furthermore, with increasing oil content, the increase in Young's modulus gives particles of the broken gels with a higher 'apparent

viscosity'. For gels with unbound droplets, increasing the oil content causes a decrease of the gel modulus and has only a minor effect on gel brittleness. Therefore, these gels are broken down into less homogenous systems, containing larger, less stiff particles and with a lower 'apparent viscosity'. Compared to gels without oil, gels containing both bound and unbound droplets are fragmented in more homogeneous systems.

The sensory perception of emulsion-filled gels appears to be dominated by the properties of the gel matrix and by the oil content. Polymer gels are perceived as more melting, particle gels as more rough. With increasing oil content both types of gels become more creamy and spreadable. These sensory attributes are positively correlated with each other. The release of oil droplets during oral processing does not completely explain the perception of oil-related sensory attributes. As a matter of fact, the sensory score for the attribute creamy (and in certain cases fatty) also increases with increasing oil content when no release of the oil droplets occurs. Since the friction coefficient of broken gels decreases with increasing oil content for gels with both bound and unbound droplets, it can be concluded that a part of the perception of these attributes is mediated by the lubrication properties of the broken gel. The increase in spreadability, and therefore also a part of the increase in creaminess, observed with increasing oil concentration can be explained by the mechanism described above to relate the first fracture event of filled gels to the properties of extensively fragmented gels. The increase in brittleness resulting from the presence of oil droplets in the gel matrix yields upon oral processing more homogeneous fragmented gels compared to gels without oil. Thus, the most important effect of the oil droplets embedded in the gel matrix is the breakdown of the gel network, which in turn determines the sensory perception.

Concluding, the droplet-matrix interaction affects the fracture behaviour of the filled gels, which determines their spreadability, and the 'apparent viscosity' of the broken gels. The 'apparent viscosity' partially controls the lubrication properties of these systems and thereby the perception of creaminess and fattiness. In Figure 9.1 a summarising scheme is shown of the links between the physicochemical mechanisms affecting the sensory perception of emulsion-filled gels and the respective sensory attributes. To completely unveil the sensory perception mechanism of emulsion-filled gels, future research should focus on the phenomena relating the large deformation properties to the rheological properties of the broken gel, with particular regard to fracture events following the first event, and to the effect of the size and stiffness of the particles of the broken gel on 'apparent viscosity'. The precise mechanism relating the lubrication properties of the broken gels to sensory perception is not known yet. Therefore, future research should also focus on this item.

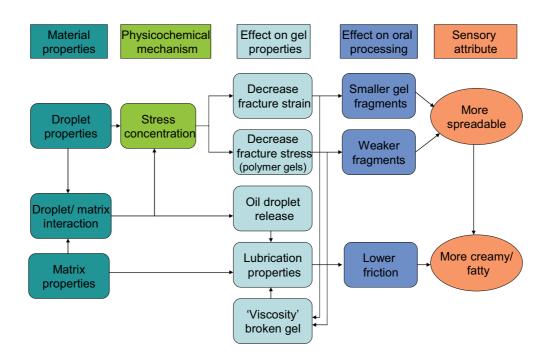


Figure 9.1 – Links between gels properties affecting the sensory perception of emulsion-filled gels and the respective sensory attributes.

Samenvatting en slotopmerkingen

Dit proefschrift beschrijft een serie studies naar de mechanische eigenschappen onder grote vervorming en de lubricatie-eigenschappen van emulsiegevulde gelen. Verder beschrijft dit proefschrift de manier waarop deze eigenschappen gerelateerd zijn aan de sensorische perceptie van de gelen. Kennis over het mechanisme van de sensorische perceptie van emulsiegevulde gelen is van groot belang voor de productie van levensmiddelen met een gereduceerd vetgehalte maar met onverminderde sensorische kwaliteiten.

In dispersies en oplossingen van geleringsmiddelen die oliedruppels bevatten treedt vaak fasescheiding op, veroorzaakt door verschillende fysisch-chemische mechanismen. De bereiding van stabiele, homogeen gevulde gelen is daarom niet eenvoudig. **Hoofdstuk 2** beschrijft de optimalisatie van de bereiding van emulsiegevulde wei-eiwitgelen. Oliedruppels gestabiliseerd door natief wei-eiwit gaven fasescheiding in suspensies van wei-eiwitaggregaten, waarschijnlijk als gevolg van depletie-vlokking. Dit resulteerde in heterogene gelen. Stabiele en homogene emulsiegevulde gelen werden bereid door verzuring van emulsies gestabiliseerd door een suspensie van wei-eiwitaggregaten. In dit hoofdstuk worden ook de rheologische eigenschappen van deze gelen beschreven bij zowel kleine als grote vervorming.

Na de ontwikkeling van een set geschikte modelgelen werd deze onderworpen aan grote vervorming teneinde het effect van de oliedruppels op de mechanische eigenschappen te bestuderen. In navolging van gepubliceerde studies werd dit bij constante en relatief lage vervormingsnelheid gedaan. De geselecteerde gelen waren gelatine, ĸ-carrageen and weieiwitgelen met oliedruppels waarvan de interacties met de matrix gevarieerd werden door de keuze van de emulgator. In Hoofdstuk 3 worden de mechanische eigenschappen onder grote vervorming van deze gelen beschreven. Voor gelatinegelen nam de Young's modulus soms toe en soms af, al naar gelang de gebruikte emulgator. Een toename van de Young's modulus duidt op oliedruppels die gebonden zijn aan de gelmatrix. Uiteraard duidt een afname van de Young's modulus dan op oliedruppels niet gebonden aan de gelmatrix. Voor wei-eiwitgelen konden alleen monsters met gebonden druppels worden bereid. De veranderingen in Young's modulus voor k-carrageengelen waren voornamelijk gerelateerd aan interacties tussen kcarrageen en de emulgatoren in de waterfase. Verschillende theorieën gaven een correcte voorspelling van het effect van de volumefractie olie op de Young's modulus, voor zowel gebonden als ongebonden druppels. Met een toename van het oliegehalte nam de vervorming bij breuk af voor gebonden oliedruppels, maar bleef ongewijzigd voor ongebonden oliedruppels. De spanning bij breuk werd niet beïnvloed door gebonden druppels en nam af voor ongebonden druppels. Theorieën over het effect van deeltjes op vervorming en spanning bij breuk bleken niet geschikt om deze experimentele resultaten te voorspellen.

De rol van gelmatrix en oliegehalte op de sensorische perceptie van de modelgelen werd ook onderzocht. **Hoofdstuk 4** beschrijft de resultaten van een studie naar de sensorische eigenschappen van de bovengenoemde geselecteerde gelen en van kappa/iota (κ/ι)carrageengelen. De oliedruppels waren gelijkmatig verdeeld in wei-eiwitgelen, licht geaggregeerd in κ/ι -carrageengelen, en sterk geaggregeerd in κ -carrageengelen. Door aanpassingen van de bereidingswijze werden gelatinegelen bereid waarin de oliedruppels nietgeaggregeerd dan wel geaggregeerd waren. De gelmatrix bepaalde grotendeels de sensorische eigenschappen van de gelen. Met een toename van het oliegehalte namen de romigheid en smeerbaarheid toe. Voor gelatine-, κ -carrageen- en κ/ι -carrageengelen (met andere woorden, voor gelen die bij lichaamstemperatuur smelten en/ of met ongebonden oliedruppels) waren de scores voor romigheid consequent hoger dan voor wei-eiwitgelen, die als ruwer werden waargenomen. Voor gelatinegelen had de aggregatie van oliedruppels geen effect op de sensorische eigenschappen. Er werden geen relevante correlaties gevonden tussen sensorische attributen enerzijds en mechanische eigenschappen onder grote vervorming bepaald bij constante vervormingsnelheid anderzijds.

In het vervolg van het onderzoek werd het effect van de vervormingsnelheid op de mechanische eigenschappen bestudeerd. Twee motieven bepaalden deze keuze. Ten eerste, wilden we betere kennis te verwerven over het effect van oliedruppels op de rheologische eigenschappen van de gelen. Ten tweede, wilden we de mechanische eigenschappen onder grote vervorming bepalen, bij een vervormingsnelheid vergelijkbaar met die in de mond. Hoofdstuk 5 bespreekt het effect van de vervormingsnelheid op de mechanische en viscoelastische eigenschappen van de geselecteerde modelgelen. De concentratie van de geleringsmiddelen en de grootte van de oliedruppel van de bestudeerde monsters werden constant gehouden. De rheologische eigenschappen van de gelmatrix bepaalden hier het effect van de vervormingsnelheid op de mechanische eigenschappen onder grote vervorming. Polymeer gelen (gelatine- and κ -carrageengelen) vertoonden een elastisch gedrag. De Young's modulus werd niet beïnvloed door de vervormingsnelheid. De toename van de spanning en de vervorming bij breuk bij een toename van de vervormingsnelheid konden worden toegeschreven aan frictie tussen structurele elementen van de gelen. Voor gelatinegelen kwam dit door de locale breuk van fysische bindingen. Deeltjesgelen (weieiwitgelen) vertoonden een visco-elastisch gedrag. De Young's modulus en de vervorming bij breuk namen toe met de vervormingsnelheid. Dit werd toegekend aan de viskeuze stroming in

de matrix en aan frictie tussen structurele elementen van de gel. Het effect van een toename van de volumefractie olie op de Young's modulus kwam voor alle gelen overeen met de Van der Poel-theorie. Oliedruppels in een gelmatrix (i) werken als stress-concentratiekernen en (ii) verhogen frictie. Het relatieve belang van deze twee effecten was afhankelijk van de viscoelastische eigenschapen van de matrix, en van de druppel-matrixinteractie. Voor polymeergelen en gelen met gebonden druppels speelden stress-concentratieverschijnselen een grotere rol. Voor visco-elastische gelen en gelen met ongebonden druppels was frictie meer van belang, met als gevolg een toename van het visco-elastische karakter van de gelen. Een toename van de volumefractie olie veroorzaakte vervolgens een afname van zowel spanning als vervorming bij breuk voor polymeergelen en een toename van de spanning bij breuk voor deeltjesgelen.

Hoofdstuk 6 bespreekt de mechanische en visco-elastische eigenschappen van modelgelen met een constant oliegehalte, maar verschillende concentraties geleringsmiddelen en groottes van de oliedruppels. Een toename van de concentratie geleringsmiddel resulteerde in dichtere gelen met meer bindingen tussen structurele elementen. Dit veroorzaakte een toename van zowel de Young's modulus als de spanning bij breuk voor alle gelen. Met een toename van de concentratie van geleringsmiddel werden polymeergelen minder 'strainhardening' en deeltjesgelen zelfs 'strain-weakening'. Het effect van een afname van de grootte van de oliedruppels was in het algemeen in overeenstemming met de Van der Poeltheorie, tenzij de oliedruppels geaggregeerd waren. Een afname van de grootte van de oliedruppel (bij gelijk oliegehalte) veroorzaakte verder een afname van de vervorming bij breuk in gelen met niet-geaggregeerde gebonden druppels. De mate waarin dit effect optrad was afhankelijk van de concentratie van het geleringsmiddel. Het effect van een afname van de grootte van de oliedruppels op andere breukparameters en in andere systemen was gering. Voor gelen met niet-geaggregeerde gebonden druppels leek het effect van een afname van de grootte van de oliedruppels (bij gelijk oliegehalte) op dat van een toename van het oliegehalte (bij contante druppelgrootte). Voor deze gelen kan een afname van de grootte van de oliedruppels een toename van het oliegehalte nabootsen. Deze vinding is van groot belang voor de ontwikkeling van nieuwe producten met verlaagd vetgehalte.

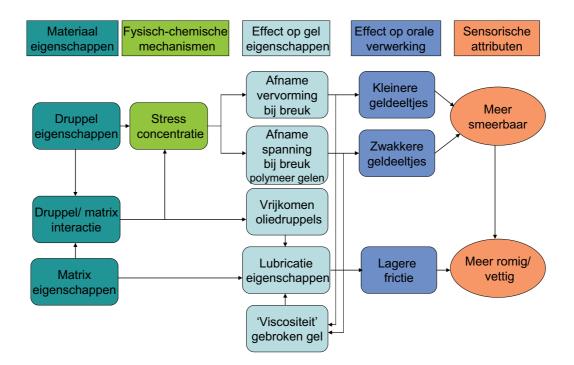
Eerste hypothesen over het mechanisme van de perceptie van emulsiegevulde gelen gingen uit van een effect van de druppel-matrixinteracties op het vrijkomen van de oliedruppels uit de gelen tijdens consumptie. Om dit te onderzoeken werd een methode ontwikkeld om het vrijkomen van oliedruppels als gevolg van het vermalen van de gel te kwantificeren. De rol van het vrijkomen van oliedruppels op de perceptie van de gelen werd ook bestudeerd. Deze aspecten zijn in **hoofdstuk 7** beschreven voor de geselecteerde modelgelen. Bij 20°C werd er geen vrijkomen van oliedruppels waargenomen voor gelen met gebonden oliedruppels. Het vrijkomen van oliedruppels uit gelen met ongebonden druppels was gerelateerd aan het oliegehalte en de grootte van de geldeeltjes na vermaling. Gelatinegelen smelten bij lichaamstemperatuur. Als de analyse bij deze temperatuur werd uitgevoerd, kwamen de oliedruppels ook vrij uit gelen met gebonden druppels. Een toename van het oliegehalte gaf een toename van de romigheid voor alle gelen. De romigheid was hoger voor gelen met ongebonden druppels, en voor gelen die smelten bij lichaamstemperatuur. Voor deze gelen correleerde de hoeveelheid vrijgekomen olie met de romigheid. Echter, ook voor niet smeltende gelen met gebonden druppels werd een vergelijkbaar effect van het oliegehalte op de romigheid gevonden. De bovengenoemde hypothese over de relatie tussen druppel-matrixinteracties en het vrijkomen van de oliedruppels uit de gelen tijdens consumptie werd dus bevestigd. Toch bleek het vrijkomen van oliedruppels niet het voornaamste mechanisme waarmee de perceptie van de romigheid van emulsie-gevulde gelen kan worden verklaard.

In het vervolg van het onderzoek werden de lubricatie-eigenschappen bestudeerd van emulsiegevulde gelen, van de afzonderlijke componenten ervan en van speeksel. De resultaten van dit onderzoek worden in hoofdstuk 8 besproken. In deze studie werden de gelen vermalen, zodat ze op gelen leken na orale verwerking. De emulsies die gebruikt werden voor de bereiding van de emulsiegevulde gelen vertoonden een afname van de frictiecoëfficiënt bij een toename van het oliegehalte. Emulsies met 40% olie (op gewichtsbasis) hadden dezelfde frictiecoëfficiënt als de olie. De lubricatie-eigenschappen van de emulsiegevulde gelen hingen voornamelijk af van de moleculaire eigenschappen en het breukgedrag van de matrix en van de druppel-matrixinteracties. Voor gelen met gebonden druppels nam de frictiecoëfficiënt geleidelijk af bij een toename van het oliegehalte. Voor gelen met ongebonden druppels was de frictiecoëfficiënt lager dan die van de matrix zonder oliedruppels. Toch werd er voor deze gelen geen effect van het oliegehalte op de frictiecoëfficiënt waargenomen. De verschillende effecten van het oliegehalte op het lubricatiegedrag van de verschillende gelen werden verklaard door de relatie tussen druppel-matrixinteracties en de 'schijnbare viscositeit' van de vermalen gelen. Voor gelen met gebonden druppels resulteerde een toename van het oliegehalte in een toename van de 'schijnbare viscositeit' van de gemalen gelen. Voor gelen met ongebonden druppels had het oliegehalte geen effect op de 'schijnbare viscositeit'. Confocale Scanning Laser Microscopie (CSLM) opnamen van zowel de emulsies als de emulsiegevulde gelen lieten geen coalescentie zien van de oliedruppels als gevolg van de frictiemetingen.

De studie van de mechanische eigenschappen van emulsiegevulde gelen zoals beschreven in dit proefschrift was aanvankelijk gericht op het optreden van de eerste breuk onder compressie. Het effect van de druppel-matrixinteracties op de 'schijnbare viscositeit' van de gemalen gelen wijst echter op de relevantie van de opvolgende afbraak. Gelen met dezelfde matrix en hetzelfde oliegehalte, maar met verschillende interacties tussen oliedruppels en gelmatrix, worden in de mond verbroken tot systemen met verschillende rheologische eigenschappen. De vindingen beschreven in dit proefschrift maken het mogelijk om een mechanisme voor te stellen voor de relaties tussen de eerste breuk en de eigenschappen van een gemalen gel. Met een toename van het oliegehalte worden gelen met gebonden druppels brosser. Daardoor worden ze gebroken in kleinere deeltjes, resulterend in een homogene massa zonder grote, met het blote oog zichtbare deeltjes. Bovendien leidt de toename van de Young's modulus bij de toename van het oliegehalte tot stijvere gelbrokjes. Als resultaat worden gelen met gebonden druppels gebroken tot systemen met een hogere 'schijnbare viscositeit'. Voor gelen met ongebonden druppels daarentegen veroorzaakt een toename van het oliegehalte een afname van de gel modulus, met geringe effecten op de gelbrosheid. Deze gelen worden gebroken tot minder homogene systemen, met grotere, mindere stijve deeltjes en met een lagere 'schijnbare viscositeit'. Vergeleken met gelen zonder olie worden emulsiegevulde gelen met zowel gebonden als ongebonden druppels gefragmenteerd tot homogenere systemen.

De sensorische perceptie van emulsiegevulde gelen wordt gedomineerd door de eigenschappen van de gel matrix en het oliegehalte. Polymeergelen worden waargenomen als meer smeltend, deeltjesgelen als meer ruw. Met een toename van het oliegehalte worden beide gelsoorten meer romig en smeerbaar. Deze sensorische attributen zijn met elkaar gecorreleerd. Het vrijkomen van oliedruppels tijdens consumptie kan de perceptie van vetgerelateerde attributen niet volledig verklaren: de score voor het sensorische attribuut 'romig' (en in sommige gevallen 'vettig') neemt met een toename van het oliegehalte ook toe voor gelen waarbij geen oliedruppels vrijkomen. Aangezien de frictiecoëfficiënt van alle gebroken emulsiegevulde gelen afneemt met een toename van het oliegehalte, kan er geconcludeerd worden dat de perceptie van deze attributen wordt beïnvloed door de lubricatie-eigenschappen van de gebroken gelen. Het effect van het oliegehalte op de smeerbaarheid (en vervolgens ook op een deel van de toename in romigheid) kan worden verklaard aan de hand van de relatie tussen de eerste breuk van gevulde gelen en de eigenschappen van gebroken gelen. De toename in brosheid als gevolg van de aanwezigheid van oliedruppels in de gelmatrix resulteert tijdens consumptie in meer homogene gebroken gelen vergeleken met gelen zonder oliedruppels. Het belangrijkste effect van de oliedruppels in de gelmatrix is dan ook hun rol bij het afbreken van het gelnetwerk. Het is dit gebroken netwerk dat op zijn beurt de sensorische perceptie bepaalt.

Concluderend, de druppel-matrixinteractie beïnvloedt het breukgedrag van de emulsiegevulde gelen, dat vervolgens gerelateerd is aan de sensorische smeerbaarheid, en de 'schijnbare viscositeit' van de gebroken gelen. De 'schijnbare viscositeit' controleert gedeeltelijk de lubricatie-eigenschappen van deze systemen en vervolgens de perceptie van romigheid en vettigheid. Figuur 9.1 geeft een samenvattend schema van de verbanden tussen fysisch-chemische mechanismen van emulsiegevulde gelen en de bijhorende sensorische attributen. Het mechanisme van de sensorische perceptie van emulsiegevulde gelen is nog niet volledig onthuld. Om dit te kunnen bereiken zou toekomstig onderzoek gericht moeten zijn op het vinden van verbanden tussen mechanische eigenschappen onder grote vervorming enerzijds, en rheologische eigenschappen van de gebroken gelen anderzijds. Bijzondere aandacht zou besteed moeten worden aan de afbraak na de eerste breuk, en aan het effect van de grootte en de stijfheid van gelbrokjes op 'schijnbare viscositeit'. Ook het mechanisme dat de lubricatie-eigenschappen van de gebroken gelen verbindt met de sensorische perceptie van de gelen is nog niet bekend. Toekomstig onderzoek zou hierop gericht moeten worden.



Figuur 9.1 – Verbanden tussen geleigenschappen met een effect op de sensorische waarneming van emulsiegevulde gelen en de bijhorende sensorische attributen.

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- G. Sala, T. van Vliet, M. A. Cohen Stuart, G.A. van Aken, F. van de Velde, Deformation and fracture of emulsion-filled gels. 1 Effect of oil content and deformation speed, submitted for publication.

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- A. Chojnicka & G. Sala, K. de Kruif, F. van de Velde, The interactions between oil droplets and gel matrix affect the lubrication properties of sheared emulsion-filled gels, to be submitted.

Curriculum vitae

Guido Sala werd geboren op 28 augustus 1967 te Vimercate, een klein stadje 15 km ten noorden van Milaan. In 1986 behaalde hij zijn gymnasium diploma aan de Liceo Classico B. Zucchi, te Monza. In datzelfde jaar begon hij zijn studie Landbouw Wetenschappen aan de Universiteit van Milaan. In 1992 studeerde hij af bij de leerstoelgroep Levensmiddelentechnologie en microbiologie. Per november 1992 werd hij aangesteld als tijdelijk wetenschappelijk onderzoeker bij bovengenoemde leerstoelgroep, waar hij zich met studies naar de strembaarheid van melk bezig hield. In oktober 1995 begon zijn Nederlands avontuur als gastmedewerker bij de afdeling Analytische Chemie van het toenmalige Nederlands Instituut voor Zuivelonderzoek te Ede. Hier werkte hij aan de toepasbaarheid van "Multi-Angle Laser Light Scattering" (MALLS) detectie in de HPLC-analyse van polysacchariden en melkeiwitten. Per september 1996 werd hij aangesteld als productontwikkelaar bij de afdeling Research & Development van de zuivelconcern Baars Dairy te Schoonrewoerd. Een jaar later kreeg hij een functie als wetenschappelijke onderzoeker bij het toenmalige Instituut voor Agrotechnologisch Onderzoek (ATO-DLO, later Agrotechnology and Food Innovations, tegenwoordig Agrotechnology & Food Sciences Group, AFSG) te Wageningen. Zijn onderzoeksveld was de toepassing van membraantechnologie in de zuivelindustrie. Tussen januari 2000 en augustus 2001 werkte hij als procestechnoloog bij de afdeling Research & Development van de Kaasdivisie van Campina, te Tilburg. In september 2001 keerde hij terug naar ATO-DLO om te werken aan een project over de bereiding van eiwitgestabiliseerde emulsies met behulp van membraanemulgering. Gedetacheerd bij Wageningen Centre for Food Science begon hij in juli 2004 een promotieonderzoek bij het Laboratorium van Fysische Chemie en Kolloïdkunde van de Wageningen Universiteit. De resultaten van dit onderzoek worden in dit proefschrift beschreven. Sinds juli 2007 is hij wederom werkzaam als onderzoeker bij AFSG, binnen de Centre for Innovative Consumer Studies.

Educational activities

Discipline specific activities

VLAG courses

- Food rheology, 1999, Wageningen, The Netherlands
- Sport & nutrition, 2004, Arnhem and Zeist, The Netherlands
- Industrial proteins, 2006, Wageningen, The Netherlands
- Reaction kinetics, 2006, Wageningen, The Netherlands

Courses and conferences

- Lecture series on coacervates, 2005, Utrecht University, Utrecht, The Netherlands
- Basics of rheology, 2005, Anton Paar, Waalwijk, The Netherlands
- Seminar on rheo-optics, 2005, Leuven University, Leuven, Belgium
- Dutch Polymer Days, 2006, National Dutch Graduate School of Polymer Science and Technology, Lunteren, The Netherlands

Meetings

- PhD students work group, 2004-2007, Laboratory of Physical Chemistry and Colloids Science, Wageningen University, Wageningen, The Netherlands
- Colloquia, 2004-2007, Wageningen University, Wageningen, The Netherlands
- Work meetings project 'Engineered texture of emulsions and foams', Wageningen Centre for Food Science (WCFS), 2004-2007, Wageningen, The Netherlands
- Work meetings project 'Dynamics of biopolymer networks and textures', WCFS, 2004-2007, Wageningen, The Netherlands
- Program meetings 'Structure and Functionality', WCFS, 2004-2007, Wageningen, The Netherlands
- Discussion group 'Fracture mechanics', WCFS, 2004-2007, Wageningen, The Netherlands

General courses

- Scientific English, 2005, Language Centre, Wageningen University, Wageningen, The Netherlands